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FORMATION AT TEMPERATURES LOWER THAN  $1000^\circ\text{C}$ .

# Nb<sub>3</sub>Al FORMATION AT TEMPERATURES LOWER THAN 1000°C

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## Abstract.

A study has been made of the possibility of making Nb<sub>3</sub>Al wires by interdiffusion between Al and Nb at relatively low temperatures (lower than 1000°C). This method should allow the fabrication of a copper stabilized wire by coworking Nb and Al composites in a copper matrix before the diffusion treatment. Results concerning the diffusion temperature and time dependence of  $J_c$  and  $T_c$  are presented. While  $J_c(64 \text{ kG})$  is quite high, of the order of  $1.5 \times 10^5 \text{ A/cm}^2$ ,  $T_c$  is 15.56 °K, lower than the usually reported value. X-ray measurements of the lattice parameter are also reported and correlated with the measured value of  $T_c$ .

## Introduction.

It is well known that the superconducting properties of the intermetallic compound Nb<sub>3</sub>Al are such as to make it a possible candidate for large scale applications where high critical fields and high critical currents densities are required. Since Nb<sub>3</sub>Al is an A15 compound like the well studied Nb<sub>3</sub>Sn, it is logical to ask whether the fabrication methods of the latter can be extended to Nb<sub>3</sub>Al. Actually it is reported that the temperatures required for the formation of this compound<sup>1,2</sup> (is high, ranging around 1400°C); this gives rise to a number of technical problems; e.g. the partial vapor pressure of aluminum at 1400°C is 10 mm Hg and strong evaporation of aluminum takes place. Furthermore, at these temperatures the recrystallisation of niobium is almost complete; this can lower the density of pinning centers and consequently the critical current.

In the present work we describe a fabrication process in which, by a suitable choice of experimental parameters, a stabilized single core cable of Nb<sub>3</sub>Al can be obtained at temperatures lower than 1000°C. Experimental results on the most important superconducting properties will be presented and discussed.

## Fabrication Method and Results.

Two thin foils of niobium (thickness  $t_{\text{Nb}}$ ) and aluminum (thickness  $t_{\text{Al}}$ ) were superimposed and then tightly wound round a small copper cylinder. The composite was inserted into a hollow copper cylinder and this specimen was rod rolled and drawn to a final diameter of 0.2 mm. The wire was then reacted at different temperatures and for several different times.

The reaction temperatures ranged from 750°C to 950°C and the reaction times varied from 30

minutes to 16 hours.

The experimental results are presented in Fig. 1 which shows the dependence of critical current  $J_c$  at 64 kG on the reaction time for different temperatures. In Fig. 2,  $J_c$  measured at 4.2°K, is plotted against the applied magnetic field. The data refer to the samples reacted at 850°C and the various curves correspond to different diffusion times. The field dependence of  $J_c$  is similar to that reported for other type II materials. The same behaviour has been found for samples reacted at 750°C and 950°C. The estimated maximum cross section of Nb<sub>3</sub>Al<sub>2</sub> is about  $5 \times 10^{-5} \text{ cm}^2$  which gives a  $J_c(64 \text{ kG}) = 1.8 \times 10^5 \text{ A/cm}$  for the sample diffused 6 hours at 850°C.

X-ray analysis were performed on some of the samples reacted at 850°C and showed that all the aluminum initially present was reacted and that only the A15 Nb<sub>3</sub>Al phase together with unreacted niobium was present. The mean value of the lattice parameter  $a$  was found to be 5.20 Å.

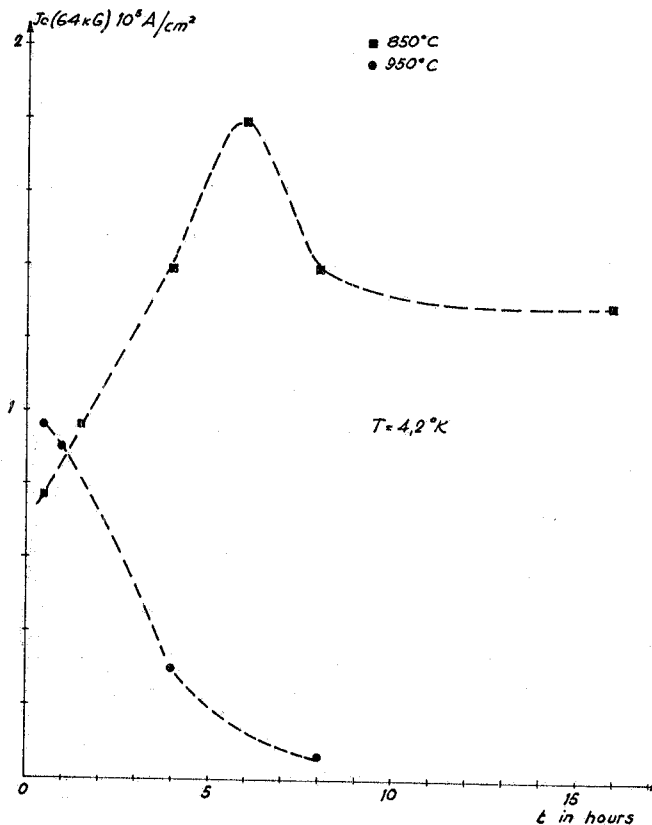


FIG. 1 - Critical current density  $J_c$  of Nb<sub>3</sub>Al wires vs. time  $t$ , for two different reaction temperatures.

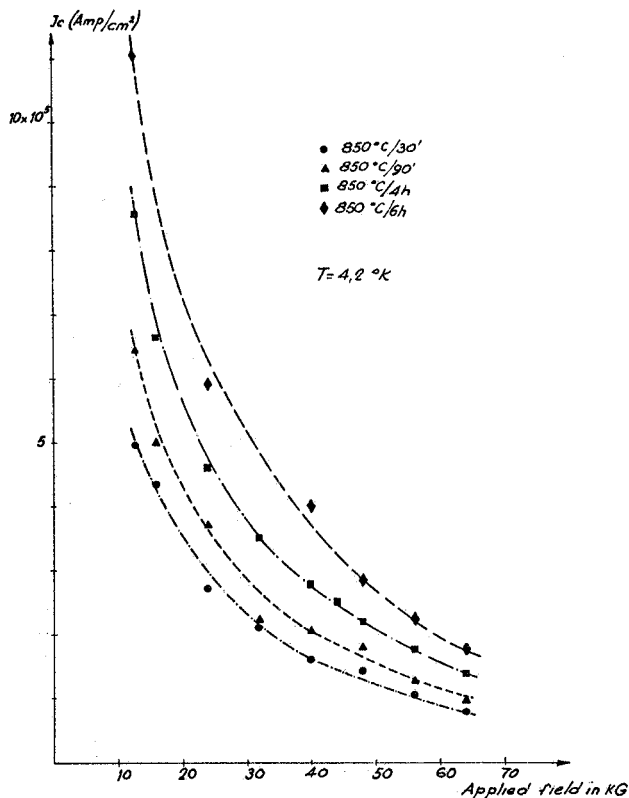


FIG. 2 - Critical current density  $J_c$   $Nb_3Al$  wires vs applied magnetic field for samples reacted at  $850^\circ C$  for different times.

We have also measured the critical temperatures for all the samples reacted at  $850^\circ C$ , but no significant dependence of  $T_c$  on the reaction time has been found:  $T_c$  ranges from  $15.48^\circ K$  to  $15.62^\circ K$ .

The Al critical current density showed a strong dependence on the thickness  $t_{Al}$ . The data shown in Figs. 1 and 2 refer to samples for which  $t_{Al}$  was 0,2  $\mu$  and the average alloy composition of the diffusion couple was Nb-Al 14 at %. Higher values of the thickness  $t_{Al}$  gave lower critical current densities.

#### Discussion.

First, our measurements show that  $Nb_3Al$  is formed at relatively low temperatures provided the thickness in the diffusion couple is extremely low. The interest in this result lies in the fact that normally for diffusion experiments at such low temperatures only non superconducting phases richer in aluminum have been observed. A possible explanation of this result is the following. In the usual diffusion experiments in binary systems, the thickness of both components is much larger than that of the diffusion region i. d. one is concerned with semi-infinite diffusion couples. Under these conditions it is possible that one or more intermetallic phases do not form even if one would expect them on the basis of the phase diagram<sup>3</sup>. This happens e. g. when the kinetic constant for the growth of a particular phase is much smaller than those of other phases. So in the Nb-Al system, at low temperatures ( $800^\circ C$ - $900^\circ C$ ) only the  $NbAl_3$  phase is practi-

cally found as its kinetic constant is the highest ref.(4). In our case the aluminum thickness  $t_{Al}$  is of the same order as the size of the diffusion region. When Al has completely reacted into  $NbAl_3$ ,  $Nb_2Al$  will start to form at expenses of  $NbAl_3$  and then  $Nb_3Al$  at expenses of  $Nb_2Al$ . A confirmation comes from the fact that by increasing the thickness  $t_{Al}$  the critical current density strongly decreases. as other non superconducting phases are present.

Second, no direct measurements of the upper critical field  $H_{c2}$  has been made. However from the ratio between the measured value of  $T_c$  and the usually reported value of  $18^\circ K$  (ref. 5), using the relation  $H_{c2}(0) \approx N\gamma T_c$ , we can deduce a value for  $H_{c2}(0)$  of about 260 kG. This large value of  $H_{c2}$  accounts for the very high critical current density at 64 kG. We also plotted the mean pinning force per unit volume  $F_p = J_c \times H$  versus the applied magnetic field;  $F_p$ , at least up to the field value of 64 kG, is quite independent of the applied field, showing a behaviour very similar to that reported for other high field A15 compounds (ref. 5) (e. g.  $Nb_3Sn$  diffused ribbon).

The dependence of  $J_c$  (64 kG) on the heat treatment time is rather complicated. The samples reacted at  $850^\circ C$  exhibit a maximum in  $J_c$  when  $t \approx 6$  hours; the maximum relative to the samples reacted at  $950^\circ C$  corresponds to  $t$  less than 30 minutes, while for those diffused at  $750^\circ C$  the presumed maximum arises for  $t$  larger than 16 hours. The existence of such a maximum can be explained on the basis of two competitive processes which are likely to occur by increasing the diffusion time: ordering of the superconducting phase and reduction in the density and/or in the efficiency of pinning; of course the first mechanism enhances  $J_c$  the second depresses it.

It is possible to correlate the measured value of the lattice parameter  $a$  with the observed value of  $T_c$ . Fig. 3 shows the dependence of  $T_c$  on  $a$  for

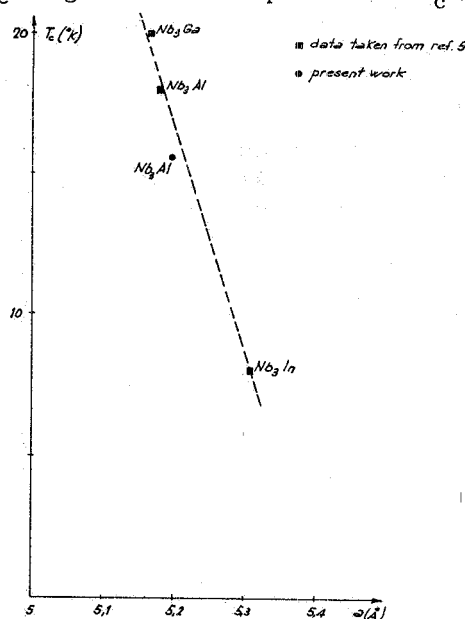


FIG. 3 - Critical temperature  $T_c$  of A15 compounds characterized by the same value of  $e/a = 4.5$  vs. lattice parameter  $a$ .

the three A15 compounds  $Nb_3Ga$ ,  $Nb_3Al$  and  $Nb_3In$ ; all these materials have the same value of the electron concentration  $e/a$ , corresponding to the value  $e/a=4.5$  electrons per atom. The correlation between  $T_c$  and  $a$ , as reported by J. M. Leger (ref. 7), is made by grouping the various A15 superconducting compounds in different series, each of which corresponds to a given value of  $e/a$ . The good agreement between our measured values of  $T_c$  and  $a$  and the curve reported in ref. 7 based on experimental data relative to materials obtained by quite different methods, confirms the validity of the analysis reported there. In this context it is likely that the reduction of  $T_c$  we observe is due to a slight mistif in the stoichiometry of the compound. Systematic measurements are in progress to investigate a possible correlation between the lattice parameter and the heat treatment time.

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Some preliminary measurements of the dependence of the critical current density on the radius of curvature have been taken and results are shown in Fig. 4. No reduction of  $J_c$  is found for radii of curvature larger than 7.5 cm; for smaller radii no conclusions can be drawn and further measurements are needed.

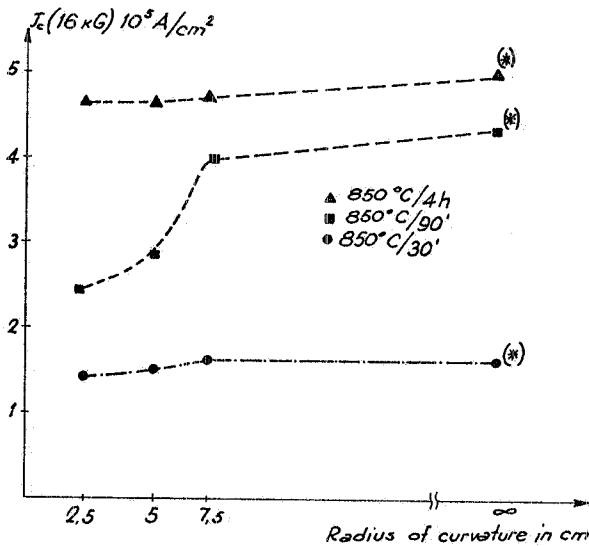


FIG. 4 - Critical current density  $J_c$  of some  $Nb_3Al$  wires as a function of radius of curvature. Data with (x) are relative to samples as received.

We can conclude that our method allows the fabrication of a copper stabilized  $Nb_3Al$  wire that promises to be a new tool for high field applications.