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L. Lovitch and S. Rosati : THE TWO-NUCLEON SCHRODINGER EQUATION WITH TENSOR FORCES. A FORTRAN PROGRAM FOR THE $J=1^+$ BOUND AND ZERO ENERGY EIGENSOLUTION.

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L. Lovitch^(x) and S. Rosati: THE TWO-NUCLEON SCHRODINGER EQUATION WITH TENSOR FORCES. A FORTRAN PROGRAM FOR THE $J = 1^+$ BOUND AND ZERO ENERGY EIGENSOLUTIONS⁽⁺⁾.

ABSTRACT. -

A Fortran program is presented for determining the bound state and zero energy eigensolutions, and associated properties, of the neutron--proton $J=1^+$ system when the interaction between the particles is described by a given combination of central, tensor and spin-orbit potentials.

1. INTRODUCTION. -

The solution of the deuteron Schrödinger equation in the presence of tensor forces, that is to say, the calculation of the eigenvalue, wave functions and associated properties, in correspondence to some given potential, does not lend itself in any case to an analytic solution in closed form. A perturbation solution when the tensor force is not small is not practical, while the use of trial wave functions accompanied by a standard variational calculation of energy suffers the usual difficulties, especially when a repulsive core is present.

(x) - Department of Physics, Columbia University, New York, N.Y.

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The variation-iteration procedure developed by Feshbach and Schwinger⁽¹⁾ has been used quite extensively in recent years, especially following the coding by Kalos and Blatt⁽²⁾ originally devised for the Illinois computer. Apart form being and indirect method, it does not always, of itself, converge rapidly and when modified accordingly results in quite extensive computations. A less essential criticism is that the latter code is written in the symbolic language of the ILLIAC and so is neither readily understood nor easily adapted for other electronic computers.

This report describes a computer program written by us in FOR-TRAN, which, when the neutron-proton potential is assigned, evaluates:

a) - for the bound state, the eigenvalue, the associated wave functions, the percentage of the D component, the quadrupole moment and the deuteron effective range,

b) - for zero energy, the corresponding wave functions, the scat tering length, the effective range, and the first two shape-dependent para meters.

The method adopted, described in refs. 3) and 4), is a direct numerical integration of the equations employing middle-point matching conditions which for the zero energy case determines the solutions uniquely, while for the bound-state deuteron equations it yields a corrector formula to a trial eigenvalue giving quadratic convergence when used iteratively.

The program is composed of three subprograms. The main subprogram includes the input and output instructions and the principle calculations involved. It calls on two subprograms: the first of these is a short program which calculates the potentials at the set of net-points of the integration (allowing four possible combinations of potential shape), while the second solves the set of simultaneous linear equations that result when the continuity conditions for the inward and outward solutions are imposed at the matching-point.

2. MATHEMATICAL FORMULATION. -

Throughout, we choose 1 MeV, 1 fm and π as the units of energy, length and action. In terms of these the velocity of light is 197.32 MeV fm π^{-1} , and M, which is twice the reduced neutron-proton mass, is 0.024114 MeV- 1 fm⁻² π^{2} .

The neutron-proton potential is taken to be of the form

$$V(\vec{r}) = V_{C}(r) + V_{T}(r) S_{12} + V_{LS}(r) \vec{L} \vec{S}$$
, (1)

2.

where

$$S_{12} = 3(\vec{e}_1 \cdot \vec{r})(\vec{e}_2 \cdot \vec{r}) / r^2 - \vec{e}_1 \cdot \vec{e}_2.$$

The J = 1^+ wave function is

$$\Psi = {}^{3}S_{1} + {}^{3}D_{1} = r^{-1} \{ u(r) \mathcal{Y}_{L=0,S=1}^{J=1} + w(r) \mathcal{Y}_{L=2,S=1}^{J=1} \},$$
(2)

where the angular momentum functions

$$\mathcal{Y}_{L,S}^{J} = \sum_{M_{L},M_{S}} (LSM_{L}M_{S}/JM) Y_{L,M_{L}}(\theta, \phi) \chi_{S,M_{S}}$$

are proper combinations of spherical harmonics and spin functions, and in the case of the bound state, the radial functions satisfy the normalisation condition

$$\int_{0}^{\infty} dr \left\{ u^{2}(r) + w^{2}(r) \right\} = 1 \quad . \tag{3}$$

The Schrödinger equation gives rise to the following coupled equations for u(r) and w(r):

$$\frac{d^{2}u}{dr^{2}} = \left\{ -\xi + f_{1}(r) \right\} u + f_{2}(r) w ,$$

$$\frac{d^{2}w}{dr^{2}} = f_{2}(r) u + \left\{ -\xi + \frac{b}{r^{2}} + f_{3}(r) \right\} w ,$$
(4)

where

$$\mathcal{E} = ME$$
, (5a)

and

$$f_{1}(r) = MV_{C}(r), \qquad f_{2}(r) = 8^{1/2} MV_{T}(r),$$

$$f_{3}(r) = M \left[V_{C}(r) - 2V_{T}(r) - 3V_{LS}(r) \right].$$
(5b)

The boundary conditions for the solutions are that u = w = 0 for r = 0, or at the edge of a hard core, and that $u, w \rightarrow 0$ as $r \rightarrow \infty$ for the bound state, while, for the zero-energy \leq -solution, the coefficient of the r^3 term in w is null, i.e. $w_{\propto} \propto 1/r^2$ (we return to this later).

2.1. - The Bound state. -

For any negative value of \leq (see eq. (5a)) the eqs. (4) have two linearly independent solutions $u(\leq)$ and $w(\geq)$ which are regular at the origin, and two linearly independent solutions which have the decaying asymptotic behaviour required of a bound state. From the linear combination of these an infinity of inward and outward solution can be obtained:

$$u_{in}(\varepsilon) = A u_{in}^{(1)}(\varepsilon) + B u_{in}^{(2)}(\varepsilon) ,$$

$$w_{in}(\varepsilon) = A w_{in}^{(1)}(\varepsilon) + B w_{in}^{(2)}(\varepsilon) ,$$
(6)

and

$$u_{out}(\varepsilon) = C u_{out}^{(1)}(\varepsilon) + D u_{out}^{(2)}(\varepsilon) ,$$

$$w_{out}(\varepsilon) = C w_{out}^{(1)}(\varepsilon) + D w_{out}^{(2)}(\varepsilon) .$$
(7)

Therefore, for a given trial energy \mathcal{E} , two independent solutions are integrated inward from large distances and two independent solutions are integrated outward form the origin, or edge of a hard core, until they meet at some intermediate point r=R. At r=R, the inward and outward solutions, and their first derivatives, can be made equal with suitable choice of A, B, C and D if and only if the trial energy value \mathcal{E} coincides with an eigenvalue. In other words, an eigenvalue is given as a zero of the determinant

$$\Delta(\varepsilon) = \begin{vmatrix} u_{in}^{(1)}(\varepsilon) & u_{in}^{(2)}(\varepsilon) & u_{out}^{(1)}(\varepsilon) & u_{out}^{(2)}(\varepsilon) \\ w_{in}^{(1)}(\varepsilon) & w_{in}^{(2)}(\varepsilon) & w_{out}^{(1)}(\varepsilon) & w_{out}^{(2)}(\varepsilon) \\ u_{in}^{(1)'}(\varepsilon) & u_{in}^{(2)'}(\varepsilon) & u_{out}^{(1)'}(\varepsilon) & u_{out}^{(2)'}(\varepsilon) \\ w_{in}^{(1)'}(\varepsilon) & w_{in}^{(2)'}(\varepsilon) & w_{out}^{(1)'}(\varepsilon) & w_{out}^{(2)'}(\varepsilon) \end{vmatrix}$$
(8)

We wish now to explain why we integrate two inward and two out ward solutions rather than limit ourselves to integrating in just one direction. Let us first examine what happens if we integrate outward only. As we proceed toward the asymptotic region the general solution for u and w is of the form

$$u \sim \overline{A} e^{-kr} + \overline{B} e^{kr}, \qquad (9)$$
$$w \sim \overline{C} e^{-kr} \left(1 + \frac{3}{kr} + \frac{3}{k^2 r^2}\right) + \overline{D} e^{kr} \left(1 - \frac{3}{kr} + \frac{3}{k^2 r^2}\right)$$

The boundary conditions impose, however, that \overline{B} and \overline{D} be zero. But round ing off and truncation errors introduce small amounts of the unwanted solution and so sooner or later the outward solution explodes exponentially, in every case, and it is not possible to formulate a criterion which will determine the correct solution unambiguously.

To integrate inward only can be just as inaccurate, since the origin is, in general, a singular point of equs. (4). For example, if the interparticle potentials are constant around the origin, then it can be shown that the general solution for w behaves as $1/r^2$ when $r \rightarrow 0$, while if the potentials are Yukawian then $u \sim 1/r$ and $w \sim 1/r^2$ as $r \rightarrow 0$. It is, therefore, impossible to make u and w vanish at the origin by integrating inward

L.

(11)

only, since rounding off and truncation errors will always introduce part of the unwanted singular solution. Integrating both outward from the origin, or edge of a hard core, and inward from large distances, with the correct boundary conditions imposed in beginning the integrations, until they meet at some intermediate point, avoids such difficulties, since the unwanted solutions decrease in these directions, respectively.

With regard to the inward solutions, these can be started in the "extreme asymptotic" region, i. e. in the region where the nuclear potentials are zero or completely disregardable, so that the eqs. (4) result uncoupled and have the solution

$$u(r) = N_{\rm S} e^{-kr} ,$$

$$w(r) = N_{\rm D} e^{-kr} \left(1 + \frac{3}{kr} + \frac{3}{k^2 r^2}\right) ,$$
(10)

where N_S and N_D are constants of integration and k^2 = - Ł .

The range of integration can, in practice, be halved by the use of a JWKB-type approximation⁽³⁾ so as to start the inward solutions of eqs. (4) in the "medium asymptotic" region, where the nuclear potentials are small but not negligible. If R_{j-1} , R_j are two successive points of the net which we consider in the numerical integration in this region, with the corresponding values (u_{j-1}, w_{j-1}) and (u_j, w_j) for the solutions of eqs. (4), then⁽³⁾

$$\frac{\mathbf{u}_{j-1}}{\mathbf{u}_{j}} = \frac{\left[\overline{\mathbf{u}}_{o}(\mathbf{R}_{j})\right]^{1/2}}{\left[\overline{\mathbf{u}}_{o}(\mathbf{R}_{j-1})\right]^{1/2}} \exp\left[\frac{1}{2}(\mathbf{R}_{j}-\mathbf{R}_{j-1})\left\{\overline{\mathbf{u}}_{o}(\mathbf{R}_{j})+\overline{\mathbf{u}}_{o}(\mathbf{R}_{j-1})\right\}\right],$$

and

$$\frac{\mathbf{w}_{j-1}}{\mathbf{w}_{j}} = \frac{\left[\overline{\mathbf{w}}_{o}(\mathbf{R}_{j})\right]^{1/2}}{\left[\overline{\mathbf{w}}_{o}(\mathbf{R}_{j-1})\right]^{1/2}} \exp\left[\frac{1}{2}\left(\mathbf{R}_{j} - \mathbf{R}_{j-1}\right)\left\{\overline{\mathbf{w}}_{o}(\mathbf{R}_{j}) + \overline{\mathbf{w}}_{o}(\mathbf{R}_{j-1})\right\}\right],$$

where

$$\begin{split} \overline{u}_{0}(\mathbf{r}) &= + \left[- \varepsilon + f_{1}(\mathbf{r}) + f_{2}(\mathbf{r}) \frac{w(\mathbf{r})}{u(\mathbf{r})} \right]^{1/2} , \\ \overline{w}_{0}(\mathbf{r}) &= + \left[- \varepsilon + \frac{6}{r^{2}} + f_{3}(\mathbf{r}) \frac{u(\mathbf{r})}{w(\mathbf{r})} \right]^{1/2} . \end{split}$$
(12)

The right-hand-sides of (11) then involve the ratios w_j/u_j and w_{j-1}/u_{j-1} . It is sufficiently accurate in the "medium asymptotic" region to give an arbitrary value to w_j/u_j and to replace w_{j-1}/u_{j-1} in \overline{u}_0 and \overline{w}_0 by

$$\frac{w_{j-1}}{u_{j-1}} = \frac{w_j}{u_j} \left(1 + \frac{3}{kR_{j-1}} + \frac{3}{k^2R_{j-1}^2}\right) / \left(1 + \frac{3}{kR_j} + \frac{3}{k^2R_j^2}\right), \quad (13)$$

although in principle one could iterate, i. e. insert the resulting ratios gi-

ven by (11) in (12) to obtain new values, and so on until convergence is achieved. This iteration procedure has been tested and been found to be unnecessary, giving the same final results.

As has been already observed, $\Delta(\xi)$ is zero only when ξ is an eigenvalue of the system. Integrating two inward and two outward solutions for an arbitrary negative value of ξ until some matching-point, r = R, is reached, we can choose A, B, C and D so that at r = R,

$$u_{in}(\xi) = u_{out}(\xi) = u_{m},$$

$$w_{in}(\xi) = w_{out}(\xi),$$

$$w'_{in}(\xi) = w'_{out}(\xi),$$
(14)

where u_m is any constant value which is fixed a priori. It can be shown⁽³⁾ that if $\mathcal{L} + \delta \mathcal{E}$ is the exact eigenvalue then we can write a corrector formula

$$\delta \mathcal{E} = \frac{u'_{m} \left[u'_{out}(\mathcal{E}) - u'_{in}(\mathcal{E}) \right]}{\int_{0}^{R} dr \left[u^{2}_{out}(\mathcal{E}) + w^{2}_{out}(\mathcal{E}) \right] + \int_{R}^{\infty} dr \left[u^{2}_{in}(\mathcal{E}) + w^{2}_{in}(\mathcal{E}) \right]} + 0 \left(\delta \mathcal{E}^{2} \right).$$
(15)

Alternatively, we can choose A, B, C and D such that, at r = R,

$$u_{in}(\mathcal{E}) = u_{out}(\mathcal{E}),$$

$$u_{in}'(\mathcal{E}) = u_{out}'(\mathcal{E}),$$

$$w_{in}(\mathcal{E}) = w_{out}'(\mathcal{E}) = w_{m},$$
(16)

where w_m is a constant value fixed a priori; and then $\delta \epsilon$ is given by

$$\delta \mathcal{E} = \frac{w_{m} \left[w_{out}^{\prime}(\varepsilon) - w_{in}^{\prime}(\varepsilon) \right]}{\int_{0}^{R} dr \left[u_{out}^{2}(\varepsilon) + w_{out}^{2}(\varepsilon) \right] + \int_{R}^{\infty} dr \left[u_{in}^{2}(\varepsilon) + w_{in}^{2}(\varepsilon) \right]} + 0 \left(\delta \varepsilon^{2} \right),$$
(17)

It should be noted that the use of eqs. (14) with the corrector formula (15), or eqs. (16) with the corrector formula (17) should and does yield identical results.

If, alternatively, we assume a given value for the bound state energy $\boldsymbol{\xi}$, we can invert the problem, that is to say, it is possible to adjust one of the parameters of the potential so as to reproduce such an energy value. For example, if the variable parameter is a multiplicative factor which is common to the central, tensor and spin-orbit parts of the potential, so that in eqs. (4) we now have the terms λf_1 , λf_2 , λf_3 in pla ce of f_1 , f_2 and f_3 respectively, then the corrector formula for this factor λ is:

$$\delta \lambda = \frac{-u_{m} \left[u_{out}^{\prime}(\varepsilon) - u_{in}^{\prime}(\varepsilon) \right]}{\int_{0}^{R} \left[u_{out}^{2} f_{1} + w_{out}^{2} f_{3} + 2u_{out} w_{out}^{2} \right] + \int_{R}^{\infty} dr \left[u_{in}^{2} f_{1} + w_{in}^{2} f_{3} + 2u_{in} w_{in}^{2} f_{2} \right]},$$
(15a)

for the case that we satisfy the eqs. (14) at the matching-point r = R. This corresponds to eq. (15) for $S \in$. We can also readily deduce the corrector formula for $\delta \lambda$ that may be used in conjuction with eqs. (16):

$$\delta \lambda = \frac{-w_{m} \left[w_{out}^{\prime}(\varepsilon) - w_{in}^{\prime}(\varepsilon) \right]}{\int_{0}^{R} dr \left[u_{out}^{2} f_{1} + w_{out}^{2} f_{3} + 2u_{out} w_{out} f_{2} \right] + \int_{R}^{\infty} dr \left[u_{in}^{2} f_{1} + w_{in}^{2} f_{3} + 2u_{in} w_{in} f_{2} \right]}$$
(17a)

Finally, if $\mathcal{T}^2 = -\mathcal{E}_d$, where \mathcal{E}_d is the eigenvalue of eqs.(4), then as $r \to \infty$ we have the behaviour for the corresponding solution: $u_d \sim N_S e^{-\Im r}$ and $w_d \sim N_d e^{-\Im r}$. The deuteron effective range is defined to be

$$g_{t} = g(E_{d}, E_{d}) = \frac{1}{\mathcal{T}} - \frac{2}{N_{S}^{2} + N_{D}^{2}}$$
 (18)

2.2. - The zero-energy solution. -

Imposing the boundary conditions at the origin, or edge of a hard core, it is clear that there are two linearly independent scattering eigensolutions. These are known as the \checkmark -solution and /3-solution and are mixtures of pure ${}^{3}S_{1}$ and ${}^{3}D_{1}$ states which correspond to pure ${}^{3}S_{1}$ and ${}^{3}D_{1}$ waves respectively in the limit that the tensor force vanishes.

The general solution of eqs. (4), with $\mathcal{E} = 0$, for asymptotic values of r, i.e. where the potentials vanish, is

$$u \sim gr + h$$
, $w \sim g' r^3 + \frac{h'}{r^2}$ (19)

The \prec -solution and \land -solution have the properties⁽⁵⁾ that $g'_{\alpha} = 0$ and $h_{\beta} = 0$ respectively, and at zero and low energies the scattering occurs in the \prec -channel. This may be described in terms of an effective range approximation for such energy values.

Consider the four linearly independent asymptotic solutions (19) of eqs. (4). We can combine these so as to obtain three linearly independent solutions possessing the property that g' = 0. Thus, to solve for the \checkmark -so lution we integrate two linearly independent solutions outward from the origin (or edge of hard core), with the correct zero boundary condition there, and integrate three linearly independent solutions inward from large values of r, until some matching-point r = R is reached, and combine them linearly is reached.

$$\begin{aligned} u_{out} &= A u_{out}^{(1)} + B u_{out}^{(2)} , & u_{in} &= C u_{in}^{(1)} + D u_{in}^{(2)} + E u_{in}^{(3)} , \\ w_{out} &= A w_{out}^{(1)} + B w_{out}^{(2)} , & w_{in} &= C w_{in}^{(1)} + D w_{in}^{(2)} + E w_{in}^{(3)} , \end{aligned}$$

so that the solutions and their derivatives are continuous at r = R,

$$\begin{aligned} u_{out}(R) &= u_{in}(R) , & u'_{out}(R) &= u'_{in}(R) , \\ w_{out}(R) &= w_{in}(R) , & w'_{out}(R) &= w'_{in}(R) . \end{aligned}$$

There are therefore four equations in four unknowns, the relative mixing of the solutions (the fifth unknown may be given an arbitrary non-zero value), which have clearly a unique solution.

From the resulting solution we can derive the scattering length

$$a_t = -\frac{h_{\alpha}}{g_{\alpha}}$$
(20)

and the effective range

$$r_{0t} = 2 \int_{0}^{\infty} dr \left[\left(1 - \frac{r}{a_{t}}\right)^{2} - u_{\varkappa}^{2} - w_{\varkappa}^{2} \right] =$$

$$= 2 \left[r_{f} \left(1 - \frac{r_{f}}{a_{t}} + \frac{r_{f}^{2}}{3a_{t}^{2}}\right) - \int_{r_{c}}^{r_{f}} dr \left\{ u_{\varkappa}^{2} + w_{\varkappa}^{2} \right\} - \frac{r_{f}}{3} \left\{ w_{\varkappa} \left(r_{f}\right) \right\}^{2} \right],$$
(21)

where r_c is the hard core radius, or zero if there is no hard core, and r_f is the distance from the origin of any point in the asymptotic region. It should be mentioned that the final term in expression (21) arises from evaluating directly

 $-2 \int_{r_f}^{\infty} dr w_{x}^2$

The mixed effective range is given by

$$g(0, E) = 2(\vartheta - \frac{1}{a_t}) / \vartheta^2$$
 (22)

Finally, the shape parameters \mathbf{P}_t and \mathbf{Q}_t in the effective range approximation:

$$k \cot \delta_{\alpha} = -\frac{1}{a_t} + \frac{1}{2} r_{0t} k^2 - P_t r_{0t}^3 k^4 + Q_t r_{0t}^5 k^6$$
, (23)

are given by (4):

$$P_{t} = \left\{ 3 \left(\mathcal{T} - \frac{1}{a_{t}} \right) - \mathcal{T}^{2} \left(r_{0t} + \frac{1}{2} \mathcal{S}_{t} \right) \right\} / r_{0t}^{3} \mathcal{T}^{4} = \left\{ \frac{3}{2} \left(0, E_{\chi} \right) - r_{0t} - \frac{1}{2} \mathcal{S}_{t} \right\} / r_{0t}^{3} \mathcal{T}^{2} , \qquad (24)$$

and

(

$$Q_{t} = \left\{ -2\left(\Im - \frac{1}{a_{t}}\right) + \frac{1}{2}\Im^{2}(r_{0t} + \varsigma_{t}) \right\} / r_{0t}^{5}\Im^{6} = \left\{ -\Im\left(0, E_{d}\right) + \frac{1}{2}(r_{0t} + \varsigma_{t}) \right\} / r_{0t}^{5}\Im^{4} .$$
(25)

If, on the other hand, we adopt the effective range approximation (7) (see also eq. (3.2) of ref. (8)):

$$k \cot \delta_{\mathcal{X}} = -\frac{1}{a_t} + \frac{1}{2} r_{0t} k^2 + \frac{C_t}{1 + D_t r_{0t}^2 k^2} ,$$
 (23a)

which may well be applicable over a larger range of values of k than eq. (23), then it may be shown that (4)

$$C_{t} = \frac{\left(\Im - \frac{1}{a_{t}} - \frac{1}{2}r_{0t}\Im^{2}\right)^{2}}{r_{0t}^{3}\Im^{4}\left(\Im - \frac{1}{a_{t}} - \frac{1}{2}\Im_{t}\Im^{2}\right)} = \frac{\left\{\Im\left(0, E_{td}\right) - r_{0t}\right\}^{2}}{2r_{0t}^{3}\Im^{2}\left\{\Im\left(0, E_{td}\right) - \Im_{t}\right\}}, (24a)$$

and

$$D_{t} = \frac{2(\gamma - \frac{1}{a_{t}}) - \frac{1}{2}(r_{0t} + \beta_{t})\gamma^{2}}{r_{0t}^{2}\gamma^{2}(\gamma - \frac{1}{a_{t}} - \frac{1}{2}\beta t\gamma^{2})} = \frac{2\beta(0, E_{d}) - r_{0t} - \beta_{t}}{r_{0t}^{2}\gamma^{2}\{\beta(0, E_{d}) - \beta_{t}\}}.$$
 (25a)

3. PROGRAM DESCRIPTION. -

The program was originally written in FORTRAN II, but at an in termediate stage of the testing it was decided to translate it to FORTRAN IV (due to changes in the computer facilities available to us). We therefore present the FORTRAN IV version of the program, and keeping in mind the fact that FORTRAN II is still being used extensively, we note that the only changes required to obtain a FORTRAN II version are appropriate modifications in the input and output statements and to the names, in call statements, of the subprograms of the system.

The program listing that we present yields double precision operations for all floating-point calculations. To obtain double precision results it is not necessary to perform all these calculations in double precision, but it was felt that the greater simplicity resulting, combined with the very small time difference involved on an IBM 7094 computer, justified our doing so. To change to single precision calculations, all that is then needed is to replace the D-conversion by E-conversion for the floating point constants and in format statements associated with the input and output, and to remove all type statements "Double Precision" that appear towards the beginning of each subprogram.

10.

The entire program consists of a main routine and two subroutines. The main routine executes the bulk of the calculations and the input and output instructions, subroutine POT calculates the potential functions normalised accordingly, and subroutine SYSTEM performs the solution of a set of simultaneous linear equations of arbitrary order (we need to solve a set of three equations prior to evaluating the corrector formula for the bound state, and a set of four equations to match the zero-energy scattering solutions).

We present the listing of the main program and subroutine POT in Appendix A. For subroutine SYSTEM (A, N, B) any standard subprogram that solves the set of N simultaneous linear equations, which we write in matrix form

$$AX = B, \qquad (26)$$

and which, before returning execution to the calling program, replaces the array B by the solution X of the system, may be used. The subprogram used by us was based on a program MATINV existing in the SHARE catalogue available to users of IBM machines. For compatibility with the main program it is necessary that A and B of subroutine SYSTEM be dimensioned as A(4,4) and B(4) respectively.

Subroutine POT yields the central, tensor and spin-orbit potentials at the set of net-points of the integration range combined, and normalised, in a form suitable for direct insertion in the differential equations. The well shapes of the potentials calculated may be

Square well	:	V(r)	=	$ \begin{cases} V_{0}, & r < r_{0}, \\ 0, & r > r_{0}, \end{cases} $	
Exponential w	ell:	V(r)	=	$V_0 e^{-\mu r}$,	(27)
Yukawa well	:	V(r)	Ξ	$\frac{v_0 e^{-\mu r}}{\mu r}$,	
Gauss well	:	V(r)	=	$v_0 e^{-\alpha r^2}$,	

and there may or may not be a hard core associated with the two-particle interaction. The information necessary to define the potentials is transmitted to the subroutine from the main program, after being specified by the input data.

3.1. - Main Subprogram. -

The most important part of this program for the causal user consists of the input statements, so that once a set of input data is specified the machine effects the calculations requested by the data. There are three such input statements: they are preceded by the external formula numbers 2, 4 and 6 and are associated respectively with the format state ments having external formula numbers 500, 504 and 516.

Since, in general, the nuclear potentials are short ranged and vary strongly near the origin, it is necessary, when solving the differential equations, to use small integration step-lengths in this region; while on the other hand, when we reach a region where the potentials become small, it may be sufficient to use much larger step-lengths to obtain a particular accuracy and, indeed, it would be extremely wasteful of machi ne-time to use the same step-length over the whole range of integration besides requiring a corresponding increase in the capacity of the memory of the computer. We have therefore allowed for the possibility of using dif ferent integration step-lengths, dividing up the total range of integration of the equations into blocks, each of which is subdivided into a certain number of intervals of equal length. Clearly, the actual step-lengths to be used for a particular problem depends essentially on the accuracy desired for the results; nevertheless we feel it worthwhile stating, as an illustration, that, to obtain very accurate results with some potentials, step-lengths of about 0.001 fm had to be used near the origin, whereas at about 2 fm away from it step-lengths of 0.2 fm were already quite adequate.

The first input statement:

2 READ (5,500) CØRE, H(1), JØUT, JTØT, (N(L), X(L), L=1, JTØT)

associates the numbers on the first few data cards with respectively, the hard core radius, the step-length to be used nearest the origin, the number of blocks to be used in the outward integration, the total number of blocks to be used over the entire integration range, followed by the number of step-lengths to be used in the first block (i. e. the one nearest the origin), the step-length scale factor in going from the first to second block, the number of step-lengths to be used in the second block, the step-length scale le factor in going from the second to the third integration block, and so on until the number of step-lengths in the final block is read.

The machine then proceeds to calculate the distance from the origin of each of the integration net-points and the appropriate factors that should be associated with them in the numerical integration of simple quadratures, such as is required later to normalise the wave functions. The numerical integration formula used for these quadratures is the three-point SIMPSON rule.

In the second input statement of the program :

4 READ (5,504) IV, VC, RC, VT, RT, VL, RL

the first quantity is the one which decides whether square wells, exponen-

tials wells, Yukawa wells or Gauss wells are to be used for the central, tensor and spin-orbit potentials of the nuclear force interaction. This is followed successively by the depth and range of each of these three poten tials. The depths should in all cases be presented in MeV, positive for a repulsive potential and negative for an attractive potential, whereas the ranges for a square well, exponential well, Yukawa well, Gauss well should be given in fm, fm⁻¹, fm⁻¹, fm⁻² respectively. It should be noted that if a calculation is to be made with a neutron-proton potential having no spinorbit term and using Yukawa potentials for the central and tensor parts, then a non-zero value should be assigned to the range of the spin-orbit term.

The third and final input statement of the program :

6 READ (5,516) EO, EPS, IC, IR, IPR, M, KCH, MAXIT

reads a trial energy for the bound state (this should be negative), and the minimum significance to be accorded to the successive corrections to the energy value in MeV. Thus, if a correction is less than the latter quantity in absolute value (it may be given as zero), then the energy search is termi nated. As has been already mentioned, however, the accuracy is limited rather by the step-lengths used in the integration formula. Therefore, if we require a value of the energy accurate to 0.001 MeV for the potentials of Appendix B, say, then we may obtain such an accuracy with single precision calculations dividing the range of integration into step-lengths of 0.01 fm for 0 < r < 0.2, 0.02 fm for 0.2 < r < 0.8, 0.04 fm for 0.8 < r < 0.8< 2.0 and 0.4 fm for 2.0 < r < 12.0. Putting the next number (IC) equal to 1, 2 or 3 instructs the machine to calculate the solution to the bound sta te problem only, the solutions to the bound state and scattering at zero energy, or the zero-energy scattering solution only respectively. The suc ceeding numbers stipulate the re-entry point at the end of a given calculation; which wave functions (if any) are desired in the output; whether, in solving the bound state problem, we wish to use eqs. (14) and (15) or eqs. (16) and (17) (we have already pointed out that these will give the same final results); whether to use the "extreme asymptotic" solution given by eqs. (10) or the JWKB solution of eqs. (11), (12) and (13) for starting the inward integrations, in the case of the bound state problem; and, finally, the maximum number of iterations to be used in solving the bound state problem.

With regard to the re-entry point, we have allowed for a re-entry at any one of the three input statements. Hence, for example, if we wish to change the potential without altering the net-points over the range of the integration we can make the re-entry at the second input statement. For starting the inward integrations in the case of the bound state problem, clearly the "extreme asymptotic" solution is the more indicated for square-well potentials since these are exactly zero further than a certain distance from the origin. In all other cases, the JWKB solution makes it possible to reduce the total range of integration by about a factor of two as compared with the "extreme asymptotic" solution, in obtaining the same accuracy. For example, to obtain more than five figure accuracy for the energy

of a bound state, it is necessary to integrate inward from about 27 fm if we use the "extreme asymptotic" solution, whereas with the JWKB solution somewhere between 12 and 17 fm suffices for this purpose. To conclude our comments on the input statements we should mention that we have found that the solution to the bound state problem generally converges in between three and five interations. All further details regarding the input statements are contained in comments at the beginning of the subprograms, listing of which are given in Appendix A. In Appendix B we give a sample set of input data, while in Appendix C we give a sample set of results obtained using the first set of data listed in Appendix B.

In conclusion, we feel that some comments on the numerical in tegration of the differential equations are appropriate. In the program, we have used the NUMEROV recurrence relation⁽⁶⁾ to integrate inside each of the blocks into which the range of integration is divided, and a generalisation of $it^{(3)}$ to continue the solution from one block of a given steplength size to another one.

If we write eqs. (4) in matrix form

$$d^{2}Y/dr^{2} = V(r)Y, \qquad (28)$$

then, if h is the step-length in a given block, writing

$$Z = Y - \frac{1}{12} h^2 Y^{(2)}, \qquad (29)$$

where $\texttt{Y}^{(2)}$ is the second derivative of Y with respect to r, the NUMEROV recurrence relation is

$$Z_{n+1} = 2Z_n - Z_{n-1} + h^2 Y_n^{(2)} = 12Y_n - 10Z_n - Z_{n-1}, \qquad (30)$$

with an error of approximately $-(h^6/240)Y_n^{(6)}$.

To continue the solution from one block of step-lengths to the next let Y_n , Y_{n+k} , Y_{n-1} be, respectively, the values of Y at r_n , r_n +kh, r_n -lh for arbitrary values of k and l, then

$$1\left[Y_{n+k} - \frac{1}{12}h^{2}(k^{2}+kl-l^{2})Y_{n+k}^{(2)}\right] = (l+k)\left[Y_{n} + \frac{1}{12}h^{2}(l^{2}+3lk+k^{2})Y_{n}^{(2)}\right] - k\left[Y_{n-l} - \frac{1}{12}h^{2}(l^{2}+lk-k^{2})Y_{n-l}^{(2)}\right], \qquad (31)$$

with an error $0(h^5)$ when $k \neq 1$, and which reduces to eq. (30) when k = 1.

These are the most accurate three-point formulas that may be used to integrate eqs. (29). More accurate integration formulae involving a larger number of points can be derived, such as for example, the predic tor-corrector formulae of Milne

$$Y_{n+1} = Y_n + Y_{n-2} - Y_{n-3} + \frac{h^2}{4} (5Y_n^{(2)} + 2Y_{n-1}^{(2)} + 5Y_{n-2}^{(2)}) + 0(h^6) ,$$

$$Y_n = 2Y_{n-1} - Y_{n-2} + \frac{h^2}{12} (Y_n^{(2)} + 10Y_{n-1}^{(2)} + Y_{n-2}^{(2)}) + 0(h^6) ,$$
(32)

over five points. The use of more accurate formulae would permit one to use larger integration step-lengths and though they involve a larger number of elementary operations there would probably be a net reduction in the calculation time. More important still is the saving in the memory sto re of the computer which could be extremely important in the inverse problem of searching for a potential, of a given type, to fit the deuteron data and scattering phase shifts over a range of energy values.

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APPENDIX A

PROGRAM LISTING

\$IBFTC DEUD NOLIST DECK C DIRECT NUMERICAL SOLUTION, WITH MIDDLE-POINT MATCHING, OF С C THE DEUTERON EQUATIONS WITH TENSOR FORCES GIVING THE ENERGY EIGENVALUE, PERCENTAGE D-STATE AND QUADRUPOLE MOMENT, AND/OR С THE SCATTERING LENGTH AND EFFECTIVE RANGE TOGETHER WITH THE C C ASSOCIATED WAVE FUNCTIONS. C VARIOUS STEP-LENGTHS CAN BE USED IN INTEGRATING OVER THE С TOTAL RANGE C JTOT = TOTAL NUMBER OF BLOCKS OF DIFFERENT STEP-LENGTHS C C JOUT = NUMBER OF BLOCKS USED IN INTEGRATING OUTWARD RMAX = RANGE OF INTEGRATION FOR LAST ITERATION IN SEARCHING FOR THE EIGENVALUE, OR WHEN CALCULATING THE SCATTERING LENGTH AND C С C EFFECTIVE RANGE C N(L) = NUMBER OF STEP-LENGTHS IN L-TH BLOCK С X(L) = STEP-LENGTH SCALE FACTOR IN GOING FROM L-TH TO (L+1)-TH С BLOCK С CORE = HARD CORE RADIUS OF POTENTIAL VC, RC, VT, RT, VL, RL ARE THE PARAMETERS OF POTENTIAL AND IV DEFINES ITS TYPE - CF. SUBPROGRAM POT FOR FURTHER DETAILS C С С C C EO = TRIAL ENERGY VALUE FOR EIGENVALUE PROBLEM - NEGATIVE С EPS IS ACCURACY REQUIRED FOR EIGENVALUE - THIS CAN BE ZERO C IC = 1 FOR SOLVING THE EIGENPROBLEM ONLY C IC = 2 FOR SOLVING THE EIGENVALUE PROBLEM AND SCATTERING LENGTH C AND EFFECTIVE RANGE C IC = 3 FOR EVALUATING THE SCATTERING LENGTH AND EFFECTIVE RANGE C IR = 1, 2, 3 GIVES REENTRY AT 2, 4, 6 RESPECTIVELY C IPR=1 TO PRINT U1, W1, U2, W2, U, W AT END OF FINAL ITERATION TO PRINT U, W AT END OF FINAL ITERATION C IPR=2 C IPR=3 TO PRINT U1, W1, U2, W2, U, W DURING EACH ITERATION С IPR=4 TO PRINT U. W DURING EACH ITERATION IPR=5 FOR NO SOLUTION PRINT-OUT C C M =1, 2 FOR MATCHING EXACTLY U, W RESPECTIVELY AND, IN CASE OF С EIGENVALUE PROBLEM, THE CORRECTOR FORMULA IS GIVEN IN TERMS OF C THE MISMATCH OF W, U RESPECTIVELY С C KCH = 1,2 FOR EXTREME ASYMPTOTIC, JWKB SOLUTION RESPECTIVELY C FOR INITIATING THE INWARD SOLUTION С RS1, RS2 ARE INITIAL RATIOS OF THE TWO INDEPENDENT D-WAVE/S-WAVE C SOLUTIONS AT THE FIRST STEP LENGTH FROM THE HARD CORE RADIUS c RF1: RF2 ARE INITIAL RATIOS OF THE TWO INDEPENDENT D-WAVE/S-WAVE С SOLUTIONS AT THE FIRST STEP-LENGTH FROM THE END OF INTEGRATION C RANGE G1. G2 ARE THE VALUES OF G FOR THE ZERO-ENERGY ASYMPTOTIC : ALPHA S-WAVE SOLUTIONS, 1.+ G*R С DIMENSION N(10) DIMENSION H(10) + A1(4) + HV(10) + R(300) + SIMP(300) + U1(300) + U2(300) + 1 U(300),W1(300),W2(300),W(300),B(4),A(4,4),X(10),F1(300), 2 F2(300),F3(300),U2S(300),W2S(300),U3(300),W3(300) C

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1ED)

с

EQUIVALENCE (U1, U), (W1, W), (U2, U2S), (W2, W2S) C HTM=0.0241143D0 RAD2=DSQRT(2.DO) RAD3=DSQRT(3.D0) С 2 READ (5, 500) CORE, H(1), JOUT, JTOT, (N(L), X(L), L=1, JTOT) С JIN=JTOT-JOUT X(JTOT)=1.DO X(JOUT)=1.DO H1=H DO 3 L=1,JTOT H(L)=H1 HV(L)=H1*H1/12.D0 3 H1=H1*X(L) c INTEGRATION COEFFICIENTS C 17 K=0 K1 = 1R=CORE+H SIMP=4.D0*H/3.D0 D0 65 L=1,JTOT 21 H1=H(L) K2=N(L) IF(L-1)41,41,29 25 29 IF(L-JOUT-1)37,33,37 33 NT2=K1 NT3=K NT4=K-1 RM=R(K) 37 A=H1/3.D0 SIMP(K)=SIMP(K)+A SIMP(K1)=4+D0*A R(K1) = R(K) + H141 DO 45 1B=2+K2 K=K1 K1=K+1 R(K1)=R(K)+H1 SIMP(K1)=H1+H1-SIMP(K) 45 IF(SIMP(K1)-H1)53,57,57 49 SIMP(K1)=0.5DO*SIMP(K1) 53 GO TO 61 SIMP(K1)=0.375D0*SIMP(K1) 57 SIMP(K)=1.25D0*SIMP(K) 61 K=K1 65 K1 = K1 + 1NT=K NT1=NT-1 H1=1.D0/H(JOUT) С READ (5,504)IV, VC,RC,VT, RT,VL,RL 4 С CALL POT(IV,VC,VT,VL,RC,RT,RL,JTOT,JOUT,N,H,X,HV,R,F1,F2,F3) DE=0.D0 C 6 READ (5,516)E0,EPS,IC,IR,IPR,M,KCH,MAXIT RS1=2.5D0*H RS2=5.D0*H RF1=7.0-2 RF2=1.D-2 G1=-1.D0 G2=-0.5D0 G3=0.1D0 С

```
WRITE (6,522)
      WRITE ( 6,508)CORE,H(1),JTOT,JOUT,(N(L),H(L),X(L), L=1,JOUT)
C
      L1 = JOUT + 1
C
      WRITE ( 6,510)RM,JIN,(N(L),H(L),X(L),L=L1,JTOT)
      WRITE (6,512)IV, VC, RC, VT, RT, VL, RL
      WRITE (6,520)IC,M,KCH,G1,G2,G3,RF1,RF2,RS1,RS2
WRITE (6,522)
C
      GO TO(69,73,73),IC
 69
      ICC=IC
      GO TO 77
 73
      ICC=IC-1
С
 77
      GO TO (81,85),ICC
      EE=HTM*EO
 81
      GO TO 87
 85
      E0=0.D0
      EE=E0
 87
      DE=EE+DE
С
 89
      DO 373 IT=1,MAXIT
 93
      GO TO (97,107), ICC
C
 97
     P=DSQRT(-EE)
C
     P1-P4 ARE CORRECTIONS FOR THE FINAL INTEGRATION COEFFICIENT
с
С
     SIMP(NT) TO TAKE INTO ACCOUNT TAIL OF WAVE FUNCTION
C
     P1=0.5D0/P
     A=1.DO/(P*R(NT))
     B=1.D0/(1.D0+3.D0*A*(1.D0+A))
     P2=P1*B*B*(1.D0+6.D0*A*(1.D0+A*(2.D0+A)))
     P3=P1*B*(1.D0+A*(4.D0+5.D0*A))
     P4=P1*B*B*(1.D0+A*(7.D0+A*(18.5D0+18.D0*A)))
 107
     K=0
С
 109
     DO 117 L=1,JTOT
     ER=DE*HV(L)
     L1 = N(L) - 1
     DO 110 IB=1.L1
     K=K+1
     F1(K) = F1(K) - ER
 110 F3(K)=F3(K)-ER
     IF(L-JOUT) 112,112,111
     ER=ER*X(L)*X(L)
 111
 112
     K = K + 1
     F1(K) = F1(K) - ER
     F3(K)=F3(K)-ER
 117
С
     A=R(NT)
     B=R(NT1)
С
     GO TO (126,125),ICC
 121
C
C
     BOUNDARY VALUES OF ZERO ENERGY FUNCTIONS
С
 125
     U1(NT)=1.D0+A*G1
     U2(NT)=1.D0+A*G2
     U3(NT)=U1(NT)
     W1(NT)=1.DO/(A*A)
     W2(NT) = W1(NT)
```

W3(NT) = G3*W1(NT)U1(NT1)=1.D0+B*G1 U2(NT1)=1.D0+B*G2 U3(NT1) = U1(NT1) $W1(NT1) = 1 \cdot D0/(B*B)$ W2(NT1) = W1(NT1)W3(NT1)=G3*W1(NT1) GO TO 131 c c BOUNDARY VALUES OF FUNCTIONS C 126 U1(NT)=1.D-10 U2(NT)=1.D-10 W1(NT)=U1(NT)*RF1 W2(NT)=U2(NT)*RF2C = A/BC1=P*A C2=P*B C=C*C*(C2*(C2+3.D0)+3.D0)/(C1*(C1+3.D0)+3.D0) C1=RF1*C C2=RF2*C С GO TO (127,128),KCH 127 A1=DEXP(P*H(JTOT)) U1(NT1)=U1(NT)*A1 U2(NT1)=U2(NT)*A1W1(NT1)=W1(NT)*A1*C W2(NT1)=W2(NT)*A1*CGO TO 131 C C JWKB APPROXIMATION C A1=DSQRT(F1(NT)+F2(NT)*RF1)128 A1(2)=DSQRT(F1(NT)+F2(NT)*RF2) A1(3)=DSQRT(F3(NT)+F2(NT)/RF1) A1(4) = DSQRT(F3(NT) + F2(NT)/RF2)B1=DSQRT(F1(NT1)+F2(NT1)*C1) U1(NT1)=U1(NT)*DEXP((A1+B1)* RAD3)*DSQRT(A1/B1) C B1=DSQRT(F1(NT1)+F2(NT1)*C2) U2(NT1)=U2(NT)*DEXP((A1(2)+B1)* RAD3)*DSQRT(A1(2)/B1) C B1=DSQRT(F3(NT1)+F2(NT1)/C1) W1(NT1)=W1(NT)*DEXP((A1(3)+B1)* RAD3)*DSQRT(A1(3)/B1) C B1=DSQRT(F3(NT1)+F2(NT1)/C2) W2(NT1)=W2(NT)*DEXP((A1(4)+B1)* RAD3)*DSQRT(A1(4)/B1) C C START INWARD INTEGRATION C K=NT 131 K1=NT1 L1=JIN L2 = -1C 135 ICL=ICC+L2-1 DO 187 L=1+L1 139 IF(L2)143,143,147

19.

143	JR=JTOT-L+1 XM=1.DO/(X(JR)*X(JR))
145	IF(ICL) 163,145,163 S31=(1.DO-F1(K)*XM)*U3(K)-F2(K)*XM*W3(K) Z31=(1.DO-F3(K)*XM)*W3(K)-F2(K)*XM*U3(K) S32=(1.DO-F1(K1))*U3(K1)-F2(K1)*W3(K1) Z32=(1.DO-F3(K1))*W3(K1)-F2(K1)*U3(K1) G0 T0 163
147 151 155	JR=L IF(L-1) 155,155,159 S11=0.D0 Z11=0.D0 S21=0.D0 Z21=0.D0 G0 T0 167
C C	S AND Z ARE AUXILIARY VARIABLES FOR THE SOLUTIONS
C 163	S11=(1.D0-F1(K)*XM)*U1(K)-F2(K)*XM*W1(K) Z11=(1.D0-F3(K)*XM)*W1(K)-F2(K)*XM*U1(K) S21=(1.D0-F1(K)*XM)*U2(K)-F2(K)*XM*W2(K) Z21=(1.D0-F3(K)*XM)*W2(K)-F2(K)*XM*U2(K)
C 167	S12=(1.D0-F1(K1))*U1(K1)-F2(K1)*W1(K1) Z12=(1.D0-F3(K1))*W1(K1)-F2(K1)*U1(K1) S22=(1.D0-F1(K1))*U2(K1)-F2(K1)*W2(K1) Z22=(1.D0-F3(K1))*W2(K1)-F2(K1)*U2(K1)
C	K=K+L2
	K1=K1+L2 K2=N(JR)
171	D0 175 IB=2,K2 S13=10.D0*(U1(K)-S12)+U1(K)+(U1(K)-S11) Z13=10.D0*(W1(K)-Z12)+W1(K)+(W1(K)-Z11) S23=10.D0*(U2(K)-S22)+U2(K)+(U2(K)-S21) Z23=10.D0*(W2(K)-Z22)+W2(K)+(W2(K)-Z21)
C	A=1.D0/((1.D0-F1(K1))*(1.D0-F3(K1))-F2(K1)*F2(K1))
	U1(K1)=A*(Z13*F2(K1)+S13*(1.DO-F3(K1))) W1(K1)=A*(Z13*(1.DO-F1(K1))+S13*F2(K1)) U2(K1)=A*(Z23*F2(K1)+S23*(1.DO-F3(K1))) W2(K1)=A*(Z23*(1.DO-F1(K1))+S23*F2(K1))
C 173	IF(ICL) 174,173,174 S33=10.D0*(U3(K)-S32)+U3(K)+(U3(K)-S31) Z33=10.D0*(W3(K)-Z32)+W3(K)+(W3(K)-Z31)
174	U3(K1)=A*(Z33*F2(K1)+S33*(1.D0-F3(K1))) W3(K1)=A*(Z33*(1.D0-F1(K1))+S33*F2(K1)) S31=S32 S32=S33 Z31=Z32 Z32=Z33 S11=S12 S12=S13 Z11=Z12 Z12=Z13 S21=S22

S22=S23 Z21=Z22 Z22=Z23 C K=K+L2 175 K1=K1+L2 С C CONTINUING THE SOLUTIONS FROM ONE STEP-LENGTH TO THE NEXT С 177 IF(L2)179,179,181 179 A=X(JR-1)GO TO 183 181 A=1.D0/X(L) C 183 B=1.D0+A*(1.D0-A) A=1.D0/A C3=1.D0+A*(1.D0-A) C=1.D0+A*(3.D0+A) K2=K-L2 С A1=1.D0-B*F1(K1) B1 = -B * F2(K1)A2=B1 B2=1.D0-B*F3(K1) B=1.D0/(A1*B2-B1*A2) C C1=(1*D0+A)*(U1(K)+C*(U1(K)-S12))-A*(U1(K2)-C3*(U1(K2)-S11)) $C2=(1 \cdot D0+A)*(W1(K)+C*(W1(K)-Z12))-A*(W1(K2)-C3*(W1(K2)-Z11))$ U1(K1)=(C1*B2-C2*B1)*B W1(K1)=(C2*A1-C1*A2)*B C C1=(1.D0+A)*(U2(K)+C*(U2(K)-S22))-A*(U2(K2)-C3*(U2(K2)-S21)) C2=(1.D0+A)*(W2(K)+C*(W2(K)-Z22))-A*(W2(K2)-C3*(W2(K2)-Z21)) U2(K1)=(C1*B2-C2*B1)*BW2(K1)=(C2*A1-C1*A2)*B С IF(ICL) 187,185,187 185 $C1=(1 \cdot D0+A)*(U3(K)+C*(U3(K)-S32))-A*(U3(K2)-C3*(U3(K2)-S31))$ $C2=(1 \cdot D0+A)*(W3(K)+C*(W3(K)-Z32))-A*(W3(K2)-C3*(W3(K2)-Z31))$ U3(K1)=(C1*B2-C2*B1)*B W3(K1)=(C2*A1-C1*A2)*B 187 CONTINUE C U10UT=U1(K) W1OUT=W1(K) U2OUT=U2(K)W2OUT=W2(K) C S13=(1.D0-F1(K1))*U1(K1)-F2(K1)*W1(K1) S23=(1.D0-F1(K1))*U2(K1)-F2(K1)*W2(K1) Z13=(1.D0-F3(K1))*W1(K1)-F2(K1)*U1(K1) Z23=(1.D0-F3(K1))*W2(K1)-F2(K1)*U2(K1) C A=-L2 С DU10UT=A*((S11-S13)+0.5D0*(U1(K1)-U1(K2))) *H1 DU20UT=A*((S21-S23)+0.5D0*(U2(K1)-U2(K2))) *H1 DW10UT=A*((Z11-Z13)+0.5D0*(W1(K1)-W1(K2))) *H1 DW2OUT=A*((Z21-Z23)+0.5D0*(W2(K1)-W2(K2))) *H1 IF(ICL) 189,188,189 188 U3IN=U3(K) W3IN=W3(K) S33=(1.D0-F1(K1))*U3(K1)-F2(K1)*W3(K1)

21.

	Z33=(1.00-F3(K1))*W3(K1)-F2(K1)*U3(K1) DU3IN=((S31-S33)+0.5D0*(U3(K1)-U3(K2)))*H1 DW3IN=((Z31-Z33)+0.5D0*(W3(K1)-W3(K2)))*H1
С	
189	IF(L2) 193, 193, 197
193	U1IN=U1OUT
	W1 IN=W1OUT
	112 IN=112011T
	W2IN-W2OUT
	$W_2 IN - W_2 OOI$
	UIKZ = UI(KZ)
	U2K2 = U2(K2)
	W1K2 = W1(K2)
	W2K2 = W2(K2)
	DU1IN=DU1OUT
	DU2IN=DU2OUT
	DW1IN=DW10UT
	DW2IN=DW2OUT
c	Dire in Dire of
c	CTART OUTWARD INTEGRATION
C	START OUTWARD INTEGRATION
C	
	$UI = I \cdot D - IO$
	$U2 = 1 \cdot D - 10$
	W1=U1*RS1
	W2=U2*RS2
C	
	K=0
	K1=1
	L1=JOUT
	12=1
	60 TO 135
c	
107	1 (K1) = 1 K2
1 7 1	112(k1) = 112k2
	$U_2(K1) = U_2K2$
	WI(KI) = WIKZ
	$W_2(KI) = W_2K_2$
198	GO TO (199,231),ICC
C	10.00.01 (C.P.40.40198)
C	OUTWARD U SOLUTION= B(1)*U1+B(2)*U2
C	OUTWARD W SOLUTION= B(1)*W1+B(2)*W2
C	INWARD U SOLUTION = $B(3) \times U1 + U2$
С	INWARD W SOLUTION = $B(3)*W1+W2$
C	MATCHING POINT CONDITIONS ARE
c	B(1)*U10UT+B(2)*U20UT = B(3)*U1IN+U2IN
č	P(1) + W10UT + P(2) + W20UT = P(3) + W115 + W21N
c	D(1) = D(2) =
C	B(1) * D(1) O(1 + B(2) * D(2) O(1 - B(3) * D(1) O(1) O(2))
C	B(1)*DMIOOI+B(5)*DM5OOI = B(3)*DMIIN+DM5IN
C	
199	C=1.DO/U2IN
	B=1.00
	B(2)=W2IN*C
С	
- L	A(1,1)=U10UT*C
	A(1,2) = U20UT * C
	A(1,3) = -U1IN * C
c	
-	

```
A(2,1)=W10UT*C
      A(2,2)=W2OUT#C
      A(2,3)=-W1IN*C
C
 201
      GO TO (205,209),M
 205
      B(3)=DU2IN*C
      A(3+1)=DU1OUT*C
      A(3,2)=DU2OUT*C
      A(3,3)=-DU1IN*C
      GO TO 213
C
 209
      B(3)=DW2IN*C
      A(3,1)=DW1OUT*C
      A(3,2)=DW2OUT*C
      A(3,3)=-DW1IN*C
C
 213
     CALL SYSTEM(A, 3, B)
C
 221
      GO TO (225,229) M
 225 WM=B(3)*W1IN+W2IN
      GO TO 237
 229
      UM=B(3)*U1IN+U2IN
 237
     GO TO (241,257,242,257,257), IPR
C
      OUTWARD U SOLUTION (E=0.) = B(1)*U1+B(2)*U2
C
C
      OUTWARD W SOLUTION (E=0.) = B(1)*W1+B(2)*W2
C
      INWARD U SOLUTION (E=0.) = B(3)*U1+B(4)*U2+U3
C
      INWARD W SOLUTION (E=0.) = B(3)*W1+B(4)*W2+W3
С
CCC
      MATCHING POINT CONDITIONS (E=0.) ARE
      B(1)*U1OUT+B(2)*U2OUT=B(3)*U1IN+B(4)*U2IN+U3IN
      B(1)*W10UT+B(2)*W20UT=B(3)*W1IN+B(4)*W2IN+W3IN
C
      B(1)*DU10UT+B(2)*DU20UT=B(3)*DU1IN+U(4)*DU2IN+DU3IN
C
      B(1)*DW10UT+B(2)*DW20UT=B(3)*DW1IN+B(4)*DW2IN+DW3IN
 231
     C=1.D0/U3IN
      B=1.DO
      B(2)=W3IN*C
      B(3)=DU3IN*C
      B(4)=DW3IN*C
C
      A(1,1)=U1OUT*C
      A(1,2)=U2OUT*C
      A(1,3)=-U1IN*C
      A(1,4)=-U2IM*C
С
      A(2,1)=W1OUT*C
      A(2,2)=W2OUT*C
      A(2,3)=-W1IN*C
      A(2,4)=-W2IN*C
C
      A(3,1)=DU1OUT*C
      A(3,2)=DU2OUT*C
      A(3,3)=-DU1IN*C
      A(3,4)=-DU2IN*C
C
```

A(4,1)=DW10UT*C A(4,2)=DW2OUT*C A(4,3)=-DW1IN*C A(4,4) = -DW2IN*CС CALL SYSTEM(A,4,B) С B1=1.D0/(B(3)+B(4)+1.D0)B=B1*B B(2) = B1 * B(2)B(3) = B1 * B(3)B(4) = B1 * B(4)С 233 GO TO (244,257,244,257,257), IPR С 241 IF(IT-MAXIT) 257,242,242 С IF(IT-1) 244,244,243 242 243 WRITE (6,522) II = 0C 244 DO 1246 JF=1,NT,300 IF(II) 245,245,1244 1244 WRITE (6,522) 245 WRITE (6,524) JL=MINO(JF+49,NT) DO 246 J1=JF,JL IL=MINO(J1+250,NT) 246 WRITE (6,540)(R(L), U1(L), L=J1,IL,50) 1246 II = II + 1C DO 247 JF=1.NT.300 WRITE (6,528) JL=MINO(JF+49,NT) DO 247 J1=JF, JL IL=MINO(J1+250,NT) WRITE (6.540)(R(1).12(1). 1=11.11.50) 217 0

WRITE (6,536)

```
JL=MINO(JF+49,NT)
      DO 252 J1=JF+JL
      IL=MINO(J1+250,NT)
      WRITE (6,540)(R(L), W2(L), L=J1,IL,50)
 252
C
      GO TO (257,253), ICC
      DO 254 JF=NT4,NT,300
 253
      WRITE (6,538)
      JL=MINO(JF+49,NT)
      DO 254 J1=JF, JL
      IL=MINO(J1+250,NT)
 254
      WRITE (6,540)(R(L), W3(L), L=J1,IL,50)
С
С
      SOLUTIONS
C
 257
      C1=0.D0
      C2=0.D0
      DO 265 L=1,NT3
 261
      U(L)=B*U1(L)+B(2)*U2(L)
      W(L) = B \times W1(L) + B(2) \times W2(L)
      U2S(L)=SIMP(L) \neq U(L) \neq U(L)
      W2S(L)=SIMP(L)*W(L)*W(L)
      C1=C1+U2S(L)
      C2=C2+W2S(L)
 265
C
      GO TO (269,329),1CC
 269
      DO 273 L=NT2 +NT1
      U(L) = B(3) + U1(L) + U2(L)
      W(L) = B(3) + W1(L) + W2(L)
      U2S(L)=SIMP(L)*U(L)*U(L)
      W2S(L)=SIMP(L)*W(L)*W(L)
      C1=C1+U2S(L)
 273
      C2=C2+W2S(L)
      U(NT)=B(3)*U1(NT)+U2(NT)
      W(NT) = B(3) * W1(NT) + W2(NT)
      U2S(NT) = (SIMP(NT)+P1)*U(NT)*U(NT)
      W2S(NT) = (SIMP(NT) + P2) * W(NT) * W(NT)
      C1=C1+U2S(NT)
      C2=C2+W2S(NT)
      C3=C1+C2
 281
      A1=1.D0/C3
С
С
      ENERGY CORRECTOR FORMULA
С
 285
      GO TO (289,293),M
 289
      F=(B*DW1OUT+B(2)*DW2OUT-B(3)*DW1IN-DW2IN)*WM
      GO TO 297
 293
      F=(B*DU10UT+B(2)*DU20UT-B(3)*DU1IN-DU2IN)*UM
 297 DE=F*A1
C
      WRITE (6,544) IT, EO, EE, DE,B(1),B(2),B(3)
C
      EE=EE+DE
 301
      IF(EE) 309,305,305
 305
      WRITE (6,564)
```

DE=DE-EE GO TO 409 E0=EE/HTM 309 K1=IT-MAXIT С IF(DABS(DE)-DABS(EPS)*HTM)317,321,321 313 317 K1 = 0C С NORMALIZE С 321 A2=DSQRT(A1) DO 325 L=1,NT 323 U(L)=U(L)*A2325 W(L) = W(L) * A2GO TO (341,341,345,345,353), IPR 337 C 329 DO 331 L=NT2,NT1 U(L) = B(3) * U1(L) + B(4) * U2(L) + B1*U3(L)W(L) = B(3) * W1(L) + B(4) * W2(L) + B1 * W3(L)U2S(L) = SIMP(L) * U(L) * U(L)W2S(L)=SIMP(L)*W(L)*W(L) 331 U(NT)=B(3)*U1(NT)+B(4)*U2(NT)+B1*U3(NT) W(NT)=B(3)*W1(NT)+B(4)*W2(NT)+B1*W3(NT) U2S(NT)=SIMP(NT)*U(NT)*U(NT) W2S(NT)=(SIMP(NT)+R(NT)/3.DO)*W(NT)*W(NT) 333 GO TO (345,345,345,345,353), IPR C 341 IF(K1)353,345,345 345 DO 347 JF=1,NT,300 WRITE (6,548) JL=MINO(JF+49,NT) DO 347 J1=JF, JL IL=MINO(J1+250,NT) WRITE (6,540)(R(L), U(L), L=J1,IL,50) 347 С DO 349 JF=1,NT,300 WRITE (6,552) JL=MINO(JF+49,NT) DO 349 J1=JF,JL IL=MINO(J1+250,NT) WRITE (6,540)(R(L),W(L), L=J1,IL,50) 349 C 353 GO TO(357,397),ICC 357 IF(K1)361,377,377 RF2=(B(3)*RF1+RF2)/(B(3)+1.D0) 361 RS2=(B*RS1+B(2)*RS2)/(B+B(2)) 373 c PERCENTAGE D-STATE AND QUADRUPOLE MOMENT С 377 PD=C2*A1 B2=RAD2+RAD2 Q=0.00 381 DO 385 L=1,NT1 385 Q=Q+SIMP(L)*W(L)*R(L)*R(L)*(B2*U(L)-W(L)) Q=0.05D0*(Q+((SIMP(NT)+P3)*B2*U(NT)-(SIMP(NT)+P4)*W(NT))*W(NT)

```
1
           *R(NT)*R(NT))
С
      WRITE (6,556)E0,0,PD
      WRITE (6,522)
С
      DE=DE-EE
      GO TO (409,393), IC
 393 ICC=2
      A=P*R(NT)
      B=1.D0/A
      RHOT=1.D0/P-2.D0*DEXP(-A-A)/(U(NT)*U(NT)+(W(NT)/(1.D0+3.D0*B*(1.D0
     1+B)))**2)
      GO TO 89
С
c
      SCATTERING LENGTH AND EFFECTIVE RANGE
C
 397 SCL=-1.D0/(G1*(B1+B(3))+G2*B(4))
      A=R(NT)/SCL
      ROT=R(NT)*(1.D0-A*(1.D0-A/3.D0))
      DO 405 L=1.NT
 401
      ROT=ROT-U2S(L)-W2S(L)
 405
      ROT=ROT+ROT
C
      IF(IC-2)406,407,406
      WRITE (6.560)SCL. RUT
 406
      WRITE (6,522)
      GO TO 408
C
 407
     A=DSQRT(-EE)-1.D0/SCL
      B=1.D0/(EE*EE*ROT**3)
      ASDP=(A+0.5D0*EE*ROT)*B
      SDP=(3.DO*A+EE*(ROT+C.5DO*RHOT))*B
      AMFR=(-A-A)/EE
      SSP=(-AMFR+0.5DO*(ROT+RHOT))*B/(ROT*ROT)
      WRITE (6,562)SCL .ROT, SDP, AMFR, RHOT, ASDP, SSP
С
 408
      DE=0.D0
 409
      GO TO (2,4,6), IR
С
      END
```

\$ I BFT	C PODD SUBROU DIMENS COMMON	NOLIST C TINE POT(IV ION N(10) H	ECK VVC VT	VL	•RC•RT•	RL.	JTOT, JO R (300) . F	5U F1	「•Ň•H•X (300)•F	• H 2 (V,R,F1,F2 300),F3(3	•F3) 00)
С												
	DOUBLE	PRECISION	н		HV		X	9	R	9	F1	
	DOUBLE	PRECISION	F2		F3		CC1	9	VC		HTM	
	DOUBLE	PRECISION	CT1		VT		CL1		VL		A	
	DOUBLE	PRECISION	DEXP	9	RC	9	RT		RL	9	н1	
	DOUBLE	PRECISION	В	9	B6	9	ECH		ETH	9	ELH	
	DOUBLE	PRECISION	EC1	9	ET1	9	EL1	9	CC	9	CT	
	DOUBLE	PRECISION	CL		RAD2		DFLOAT					
	DFLOAT	(1)=I										
C												
C	IV=1,2	9394 FOR SG	UARE, E	XP	ONENTIA	La	YUKAWA	AI	ND GAUSS	5	WELL	
С	POTE	NTIALS RESP	ECTIVEL	Υ.								
C												
	GO TO	(1,5,5,9),1	V									
1	CC1=VC	*HTM										
	CT1=(V	T+VT)*HTM										
	CL1=3.	DO*VL*HTM										
C												

	M1=1 M2=1 M3=1 GO TO 13
5	A=R-H CC1=VC*DEXP(-RC*A)*HTM CT1=(VT+VT)*DEXP(-RT*A)*HTM CL1=3。DO*VL*DEXP(-RL*A)*HTM
11	IF(IV-3)13,11,11 CC1=CC1/RC CT1=CT1/RT CL1=CL1/RL GO TO 13
9	A=R-H CC1=VC*DEXP(-RC*A*A)*HTM CT1=(VT+VT)*DEXP(-RT*A*A)*HTM CL1=3。DO*VL*DEXP(-RL*A*A)*HTM
13 17	K=0 DO 109 L=1,JTOT NL=N(L) H1=H(L) B=HV(L) B6=6,D0*B
21 25	GO TO (33,25,25,29),IV ECH=DEXP(-RC*H1) ETH=DEXP(-RT*H1) ELH=DEXP(-RL*H1) GO TO 33
C 29	ECH=DEXP(-RC*(A+A)*H1) ETH=DEXP(-RT*(A+A)*H1) ELH=DEXP(-RL*(A+A)*H1) EC1=DEXP(-RC*H1*H1) ET1=DEXP(-RT*H1*H1) EL1=DEXP(-RL*H1*H1)
C 33	DO 97 IB=1.NL K=K+1
C 37 41 45 49	GO TO (41,77,89,81),IV GO TO (45,53),M1 IF(R(K)-RC)53,49,49 M1=2 CC1=0.D0
C 53 57 61	GO TO (57,65),M2 IF(R(K)-RT)65,61,61 M2=2 CT1=0.D0
65 69 73	GO TO(69,85),M3 IF(R(K)-RL)85,73,73 M3=2 CL1=0.D0 GO TO 85
с 77	CC1=CC1*ECH CT1'=CT1*ETH CL1=CL1*ELH GO TO 85
С	

CC1=CC1*ECH*EC1 81 CT1=CT1*ETH*ET1 CL1=CL1*ELH*EL1 ECH=ECH*EC1*EC1 ETH=ETH*ET1*ET1 ELH=ELH*EL1*EL1 С 85 CC=CC1*B CT=CT1*B CL=CL1*B GO TO 93 С 89 CC1=CC1*ECH CT1=CT1*ETH CL1=CL1*ELH A=B/R(K) CC=CC1*A CT=CT1*A CL=CL1*A С 93 F1(K)=CC F2(K)=CT*RAD2 F3(K)=CC-CT-CL + B6/(R(K)*R(K)) 97 С 101 GO TO (109,109,109,105),IV 105 A=A+H1*DFLOAT(NL) CONTINUE 109 с NL=0 DO 113 L=1,JOUT 113 NL=NL+N(L) M1=JOUT+1 M2=JTOT-1 DO 117 L=M1,M2 NL=NL+N(L) B=X(L)*X(L) F1(NL)=B*F1(NL) F2(NL)=B*F2(NL) 117 F3(NL)=B*F3(NL) RETURN END

29.

29

1. 1.

APPENDIX B

LISTING OF A SAMPLE SET OF DATA

SDATA

0.	+0	0.00	1+0	4	6							
100	4	•+0	20		5•+0	30	2	• 5+0	20	1.+0	6	4.+0
60	4	•+0										
3	-39	•53+0	C	.8432	24+0	-33.(0431+0	0.	65229+	0	0++0	1.+0
-2.0	0+0	0	•+0	2	1	2	2	2	7			

0.4	+0	0.0	1+0	3	5							
20	2	• +0	30	2	•+0	25	1	•+0	5	10.+0	25	1.+0
3	-10	0.7+0)	1.23	+0	-25	7.+0		1.203+0	-1	5.+3	3.7+0
-2.0	÷0	1	•-3	2	2	2	2	2	7			

3	-100.7	+0	1.23	+0	-25	7.+0	1	•203+0	0++0	1.+0
-2.0+	0	14	2	1	2	2	2	7		

HARD CO	DRE INITIAL STEP LENGTH	NUMBER OF BLOCKS	
INWARD INTEGRATION - NUM	BER OF BLOCKS JOUT= 4	30	
N H X 100 C.100CD-02 0.4000D	N H X 20 0.4000D-02 0.5000D 01	N H X 30 0.2000D-C1 0.2500D 01	N H X 20 0.5000D-01 0.1000D 01
ATCHING DOINT ARSCISSA	. 0.17800.01		
MATCHING POINT ABSCISSA	= 0.1780D 01		
MATCHING POINT ABSCISSA =	= 0.1780D 01 BER OF BLUCKS JIN= 2		
NATCHING POINT ABSCISSA INWARD INTEGRATION - NUM N H X 6 Q.500GD-Q1 C.4000D	= 0.17800 01 BER OF BLOCKS JIN= 2 N H X C1 60 0.20000 00 0.10000 01	N H X	N H X
INWARD INTEGRATION - NUM N H X 6 0.5000D-01 C.4000D	= 0.17800 01 BER OF BLOCKS JIN= 2 N H X C1 60 0.20000 00 0.10000 01	N H X	N H X
MATCHING POINT ABSCISSA INWARD INTEGRATION - NUM N H X 6 0.5000D-01 C.4000D 0 PARAMETERS SPECIFYING PO	= 0.17800 01 BER OF BLOCKS JIN= 2 N H X C1 60 0.20000 00 0.10000 01	N H X	N H X
MATCHING POINT ABSCISSA INWARD INTEGRATION - NUM N H X 6 0.5000D-01 C.4000D 0 PARAMETERS SPECIFYING PO	= 0.17800 01 BER OF BLOCKS JIN= 2 N H X C1 60 0.20000 00 0.10000 01	N H X	N H X

SOLUTION OF SCHROEDINGER DEUTERON EQUATION

SAMPLE OUTPUT LISTING

APPENDIX C

REMAINING DATA SPECIFYING SOLUTION

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 IC
 M
 KCH
 G1
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 RS2
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 -C.1000000 01
 -0.5000000 00
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IT= 1 ED= -2.00000000 00 EE= -4.8228600D-02 DE= -4.8082717D-03 B(1/3)= 9.7654369D-01 -4.7954636D-01 2.9412434D 01

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IT= 2 ED= -2.19939500 00 EE= -5.3036872D-02 DE= -9.6792359D-05 B(1/3)= 1.1368639D-10 7.83197+2D-02 1.9650173D 00

IT= 3 ED= -2.2034C89D OC EE= -5.3133664D-02 DE= -3.5067806D-08 b(1/3)= 8.3269286D-13 2.7533173D-02 3.9703612D-02

IT= 4 ED= -2.2034104D OC EE= -5.3133699D-02 DE= 6.82724280-15 B(1/3)= 2.8353975D-16 2.6482157D-02 1.4377529D-05

11= 5 E0= -2.20341040 OC EE= -5.31336990-02 DE= -1.94217160-14 B(1/3)= 3.9287652D-18 2.6481777D-02 1.9197958D-12

IT= 6 ED= -2.2034164D OC EE= -5.3133699D-02 DE= 2.63193230-14 8(1/3)= 1.5638308D-19 2.6481777D-02 -3.1032615D-12

1T= 7 E0= -2.2034104D OC EE= -5.3133699D-02 DE= -1.6460529D-15 B(1/3)= -5.0890973D-19 2.6481777D-02 -4.6750432D-12

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	DEUTERON S-	WAVE SCLUT	TICN								
R(L)	U(L)	R(L)	U(L)	R(L)	U(L)	R(L)	U(L)	R(L)	U(L)	R(L)	U(L)
1.CCD-0	9.01318D-04	5.100-02	4.465220-02	1:040-01	8.81616D-02	8.300-01	4.31152D-01	7.08D 0	00 1.707460-01		
2.000-0	1.801700-03	5.20D-02	4.550050-02	1.08D-01	9.132520-02	8.800-01	4.41796D-01	7.28D 0	00 1.630750-01		
3.000-0	2.70106D-03	5.300-02	4.63478D-02	1.120-01	9-447180-02	9-300-01	4-512970-01	7.480	00 1.557440-01		
4.000-0	3.59940D-03	5.400-02	4.719410-02	1.160-01	9.760170-02	9.80D-01	4.597310-01	7.68D (00 1.487400-01		
5.00D-0	4.49671D-03	5.500-02	4-80393D-02	1.200-01	1.00715D-01	1.030 00	4.67172D-01	7.88D 0	00 1.420490-01		
6.000-0	5.39300D-03	5.60D-02	4.888340-02	1.24D-01	1.038110-01	1.08D 00	4.736900-01	8.080 0	00 1.356580-01		
7.000-0.	6.28826D-03	5.700-02	4.972650-02	1.280-01	1.068910-01	1.13D 00	4.793500-01	8.280	00 1.295520-01		
8.00D-0	7.18249D-03	5.8CD-02	5.056850-02	1.320-01	1.099540-01	1.18D OC	4.84213D-01	8.48D (00 1.237210-01		
9.000-0	8.0757CD-C3	5.900-02	5.140950-02	1.36D-01	1.130000-01	1.23D OC	4.88335D-01	8.680	00 1.181510-01		
1.000-0	8.96788D-03	6.00D-02	5.224950-02	1.40D-01	1.160290-01	1.280 00	4.91771D-01	8.88D (00 1.128310-01		
1.100-0	9.85903D-03	6.100-02	5.308830-02	1.440-01	1.190420-01	1.330 00	4.94570D-01	9.080	00 1.077500-01		
1.200-0	2 1.074910-02	6.200-02	5.392610-02	1.480-01	1.22038D-01	1.38D 00	4.967800-01	9.28D	CO 1.02898D-01		
1.300-0	2 1.163820-02	6.300-02	5.476290-02	1.520-01	1.250180-01	1.43D 00	4.984450-01	9.480	00 9.826340-02		
1.400-0.	2 1.252630-02	6.40D-02	5.559860-02	1.560-01	1.279810-01	1.48D 00	4.996040-01	9.68D	00 9.38376D-02		
1.500-0.	2 1.341330-02	6.500-02	5.643330-02	1.600-01	1.309270-01	1.53D OC	5.00297D-01	9.880	00 8.961090-02		
1.600-0	2 1.42993D-02	6.600-02	5.726690-02	1.640-01	1.338570-01	1.58D 00	5.005580-01	1.010	01 8.55744D-02		
1.7CD-0	2 1.518420-02	6.700-02	5.80994D-02	1.680-01	1.367700-01	1.630 00	5.00422D-01	1.030	01 8.171950-02		
1.800-0	2 1.60681D-C2	6.800-02	5.893090-02	1.720-01	1.39667D-01	1.68D 00	4.999190-01	1.050	01 7.80383D-02		
1.900-0	2 1.695100-02	6.900-02	5.976130-02	1.760-01	1.42548D-01	1.73D CO	4.990770-01	1.070	01 7.452270-02		
2.000-0	2 1.783290-02	7.000-02	6.05907D-02	1.800-01	1.454120-01	1.78D 00	4.97925D-01	1.090	01 7.116550-02		
2.100-0	2 1.871370-02	7.100-02	6.141900-02	2.000-01	1.594890-01	1.830 00	4.964860-01	1.110	01 6.79594D-02		
2.200-0	2 1.95934D-02	7.200-02	6.224630-02	2.20D-01	1.731630-01	1.88D 00	4.94784D-01	1.130	01 6.489770-02		
2.300-0	2.04722D-02	7.300-02	6.307250-02	2.400-01	1.864390-01	1.930 00	4.928410-01	1.150	01 6.197390-02		
2.40D-0	2 2.134980-02	7.400-02	6.389770-02	2.600-01	1.99324D-01	1.980 00	4.90676D-01	1.17D	01 5.91818D-02		
2.500-0.	2.222650-02	7.500-02	6.47218D-02	2.800-01	2.118220-01	2.03D 00	4.88309D-01	1.190	01 5.651550-02		
2.600-0	2.310210-02	7.600-02	6.554480-02	3.000-01	2.239420-01	2.080 00	4.85758D-01	1.210	01 5.396930-02		
2.700-0	2.39766D-02	7.700-02	6.63668D-02	3.200-01	2.356880-01	2.280 00	4.740100-01	1.23D	01 5.153780-02		
2.800-0	2.485020-02	7.800-02	6.71877D-02	3.400-01	2.470700-01	2.480 00	4.604150-01	1.25D	01 4.921580-02		
2.900-0	2.57226D-02	7.900-02	6.80076D-02	3.60D-01	2.580920-01	2.68D 00	4.456240-01	1.270	01 4.69984D-02		
3.000-0.	2.659410-02	8.000-02	6.882640-02	3.800-01	2.687630-01	2.88D 00	4.301210-01	1.29D	01 4.488090-02		
3.100-0	2 2.746450-02	8.100-02	6.964420-02	4.00D-01	2.790890-01	3.080 00	4.142630-01	1.31D	01 4.285880-02		
3.200-0	2.83338D-02	8.200-02	7.046090-02	4.200-01	2.89078D-01	3.28D 00	3.983150-01	1.330	01 4.092780-02		
3.300-0.	2.920210-02	8.300-02	7.127660-02	4.40D-01	2.98738D-01	3.48D 00	3.82468D-01	1.350	01 3.908380-02		
3.400-0	2 3.006930-02	8.400-02	7.209120-02	4.60D-01	3.08074D-01	3.680 00	3.668610-01	1.370	01 3.73228D-02		
3.500-0	2 3.093550-02	8.500-02	7.290470-02	4.80D-01	3.170950-01	3.88D 00	3.515920-01	1.390	01 3.564120-02		
3.600-0	2 3.18007D-02	8.600-02	7.371720-02	5.000-01	3.25808D-01	4.08D 00	3.367310-01	1.41D	01 3.403540-02		
3.700-0	2 3.26648D-02	8.700-02	7.45286D-02	5.20D-01	3.34219D-01	4.280 00	3.223210-01				
3.800-0	2 3.352790-02	8.800-02	7.533900-02	5.40D-01	3.423370-01	4.48D 00	3.083930-01				
3.900-0	2 3.438990-02	8.900-02	7.61483D-02	5.600-01	3.501670-01	4.68D 00	2.94962D-01				
4.000-0	3.525090-02	9.000-02	7.695660-02	5.80D-01	3.577170-01	4.88D 00	2.820360-01				
4.100-0	3.611C8D-02	9.100-02	7.776380-02	6.000-01	3.649950-01	5.08D 00	2.696120-01				
4.200-0	2 3.69696D-02	9.200-02	7.857000-02	6.200-01	3.720050-01	5.28D 00	2.57688D-01				
4.300-0	3.782750-02	9.30D-02	7.937510-02	6.400-01	3.787570-01	5.48D 00	2.462530-01				
4-40D-0	3.868420-02	9.400-02	8.017910-02	6.600-01	3.852550-01	5.68D 00	2.352950-01				
4-50D-C	2 3.953990-02	9.500-02	8.098210-02	6.80D-01	3.915060-01	5.88D 00	2.24802D-01	_			
4.600-0	4.03946D-02	9.600-02	8.17841D-02	7.000-01	3.975170-01	6.08D 00	2.147590-01				
4.7CD-0	4.124820-02	9.700-02	8.258490-02	7.200-01	4.032940-01	6.28D 00	2.051510-01				
4.80D-0	4.210C8D-02	9.800-02	8.338480-02	7.400-01	4.088430-01	6.48D 00	1.959610-01				
4.900-0	4.295230-02	9.900-02	8.41835D-02	7.600-01	4.141700-01	6.680 00	1.871740-01	_			
5.000-0	4.38028D-02	1.000-01	8.498130-02	7.80D-01	4.19281D-01	6.88D 00	1.787750-01				

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RILI	W(L)	R(L)	W(L)	R(L)	W(L)	R(L)	W(L)	R(L)	W(L)	R(L)
L-00D-03	7.91222D-07	5.100-02	1.62982D-03	1.040-01	5.78328D-03	8.300-01	9.155670-02	7.080 00	2.022180-02	
2.00D-03	3.07100D-06	5.200-02	1.688770-03	1.080-01	6.16872D-03	8.80D-01	9.529450-02	7.28D 00	1.836530-02	1820 (Star)
3.00D-03	6.85980D-06	5.300-02	1.748600-03	1.120-01	6.56250D-03	9.300-01	9.867520-02	7.480 00	1.700940-02	
4.00D-03	1.212050-05	5.400-02	1.809270-03	1.160-01	6.964340-03	9.800-01	1.017120-01	7.68D 00	1.644630-02	
5.000-03	1.882960-05	5.500-02	1.87080D-03	1.200-01	7.373940-03	1.030 00	1.044180-01	7.88D 00	1.536850-02	
6.000-03	2.696560-05	5.600-02	1.933180-03	1.240-01	7.791010-03	1.C8D 00	1.068100-01	8.080 00	1.436920-02	
7.000-03	3.650850-05	5.700-02	1.996380-03	1.280-01	8.215300-03	1.130 00	1.08903D-01	8.280 00	1.344220-02	
8.000-03	4.74390D-05	5.800-02	2.060420-03	1.320-01	8.646520-03	1.18D 00	1.107130-01	8.480 00	1.258170-02	0.000000
9.000-03	5.97388D-05	5.900-02	2.125270-03	1.360-01	9.08444D-03	1.230 00	1.122560-01	8.680 00	1.178260-02	
1.000-02	7.339040-05	6.000-02	2.190940-03	1.400-01	9.528790-03	1.280 00	1.135480-01	8.88D 00	1.103990-02	
1.100-02	8.837670-05	6.100-02	2.257410-03	1.44D-01	9.979340-03	1.330 00	1.146050-01	9.080 00	1.034930-02	
1.200-02	1.046810-C4	6.200-02	2.32468D-03	1.48D-01	1.043580-02	1.380 00	1.154410-01	9.280 00	9.70678D-03	
1.300-02	1.222880-C4	6.30D-02	2.392740-03	1.520-01	1.089810-02	1.430 00	1.160720-01	9.48D 00	9.108550-03	
1.400-02	1.411820-04	6.400-02	2.461590-03	1.560-01	1.136590-02	1.48D 00	1.165120-01	9.680 00	8.551260-03	
1.500-02	1.613470-04	0.50D-02	2.531210-03	1.600-01	1.183890-02	1.530 00	1.167730-01	9.88D 00	8.03178D-03	
1.600-02	1.827700-04	6.600-02	2.601600-03	1.640-01	1.231710-02	1.580 00	1.168700-01	1.010 01	7.547270-03	
1.700-02	2.05436D-04	6.70D-02	2.672750-03	1.680-01	1.28001D-02	1.630 00	1.168130-01	1.030 01	7.095090-03	
1.800-02	2.293300-04	6.80D-02	2.744650-03	1.720-01	1.328780-02	1.68D 00	1.166160-01	1.050 01	6.672870-03	
1.900-02	2.544400-04	6.90D-02	2.81731D-03	1.760-01	1.378000-02	1.730 00	1.162900-01	1.070 01	6.278370-03	
2.000-02	2.807510-04	7.000-02	2.890700-03	1.800-01	1.42766D-02	1.780 00	1.15844D-01	1.090 01	5.909590-03	
2.100-02	3.082510-04	7.100-02	2.964830-03	2.000-01	1.681760-02	1.830 00	1.152880-01	1.110 01	5.564650-03	
2.200-02	3.369270-04	7.200-02	3.039690-03	2.200-01	1.944100-02	1.88D 00	1.14632D-01	1.130 01	5.241850-03	
2.300-02	3.667670-04	7.300-02	3.115270-03	2.400-01	2.212820-02	1.930 00	1.138860-01	1.15D 01	4.93961D-03	
2.400-02	3.977570-04	7.400-02	3.191570-03	2.600-01	2.486300-02	1.980 00	1.130560-01	1.17D 01	4.656470-03	
2.500-02	4.29887D-04	7.500-02	3.268580-03	2.800-01	2.763120-02	2.C3D 00	1.12150D-01	1.190 01	4.391110-03	
2.600-02	4.631440-04	7.600-02	3.346280-03	3.000-01	3.042000-02	2.080 00	1.111770-01	1.210 01	4.142280-03	
2.700-02	4.975160-04	7.700-02	3.424690-03	3.200-01	3.321830-02	2.28D 00	1.06732D-01	1.230 01	3.908860-03	
2-800-02	5.329920-04	7.800-02	3.50378D-03	3.400-01	3.601630-02	2.48D 00	1.016650-01	1.25D 01	3.689790-03	
2.900-02	5.695620-04	7.900-02	3.583560-03	3.600-01	3.880540-02	2.68D 00	9.62506D-02	1.270 01	3.48411D-03	
3.000-02	6.07212D-04	8.000-02	3.664020-03	3.800-01	4.157780-02	2.880 00	9.069350-02	1.290 01	3.290910-03	
3.100-02	6.45934D-C4	8.100-02	3.745150-03	4.00D-01	4.432690-02	3.08D 00	8.514060-02	1.31D 01	3.109360-03	
3.200-02	6.85716D-04	8.200-02	3.826940-03	4.200-01	4.704680-02	3.28D CO	7.96960D-02	1.33D 01	2.93871D-03	
3.300-02	7.265470-04	8.300-02	3.909390-03	4-400-01	4.973220-02	3.48D 00	7.443150-02	1.350 01	2.77824D-03	
3.400-02	7.68418D-04	8.400-02	3.992500-03	4.600-01	5.237860-02	3.68D 00	6.939400-02	1.37D 01	2.627290-03	-
3.500-02	8-113170-04	8.500-02	4.076250-03	4.80D-01	5.498210-02	3.88D 00	6.461220-02	1.390 01	2.485240-03	
3.600-02	8.55236D-04	8.600-02	4.160650-03	5.000-01	5.753930-02	4.08D 00	6.010110-02	1.410 01	2.35154D-03	
3.700-02	9.001630-04	8.700-02	4.24568D-03	5.200-01	6.004730-02	4.28D 00	5.586610-02			
3.800-02	9.460890-04	8.8CD-02	4.331350-03	5.400-01	6.250340-02	4.48D 00	5.190550-02	1.		_
3.900-02	9.93005D-04	8.900-02	4.417630-03	5.600-01	6.490560-02	4.680 00	4.821260-02			
4.000-02	1.04090D-C3	9.000-02	4.504540-03	5.800-01	6.725220-02	4.88D 00	4.477750-02	1.0		
4.100-02	1.089770-03	9.100-02	4.59206D-03	6.000-01	6.95410D-02	5.08D 00	4.158800-02			
4.200-02	1.13959D-03	9.200-02	4.680200-03	6.200-01	7.177260-02	5.28D 00	3.863070-02			
4.30D-02	1.190370-03	9.300-02	4.768930-03	6.400-01	7.394440-02	5.480 00	3.589160-02			
4.400-02	1.242100-03	9.400-02	4.858260-03	6.600-01	7.605610-02	5.680 00	3.335670-02			
4.500-02	1.294750-03	9.500-02	4.948180-03	6.80D-01	7.810740-02	5.880 00	3.101190-02			
4.600-02	1.348330-03	9.600-02	5.038690-03	7.000-01	8.009790-02	6.08D 00	2.884370-02	-		
4.70D-02	1.40283D-03	9.700-02	5.129780-03	7.200-01	8.202750-02	6.280 00	2.683910-02			
4.800-02	1.458240-03	9.800-02	5.221450-03	7.400-01	8.389600-02	6.48D 00	2.498590-02			
	1.514540-03	9.900-02	5.313690-03	7.600-01	8.570380-02	6.68D 00	2.327230-02			
4.900-02		1 000-01	5 404500-03	7-800-01	8.74510D-02	6.88D 00	2.168770-02			

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	1	DEDIEKUN S-	HAVE SULU	TICN							
	R(L)	U(L)	R(L)	U(L)	R(L)	U(L)	R(L)	U(L)	R(L)	U(L)	R(L)
-	1.000-03	1.121680-03	5.100-02	5.556770-02	1.040-01	1.097050-01	8.300-01	5.325760-01	7.080	00-3.152490-01	
	2.000-03	2.242190-03	5.200-02	5.662340-02	1.080-01	1.136410-01	8.800-01	5.451530-01	7.280	00-3.534660-01	
	3.000-03	3.361430-03	5.300-02	5.767780-02	1.120-01	1.175500-01	9.300-01	5.562450-01	7.480	00-3.976820-01	
	4.000-03	4.479400-03	5.400-02	5.873090-02	1.160-01	1.214490-01	9.800-01	5.659490-01	7.680	00-4.278950-01	
	5.00D-03	5.596100-03	5.5CD-02	5.978260-02	1.200-01	1.253220-01	1.030 00	5.743550-01	7.880	00-4.651050-01	
	6.000-03	6.71151D-C3	5.600-02	6.083310-02	1.240-01	1.291740-01	1.080 00	5.915490-01	8.080	00-5.02314D-01	
_	7.000-03	7.825650-03	5.700-02	6.188220-02	1.28D-01	1.330040-01	1.130 00	5.876100-01	8.28D	00-5.395200-01	
	8.000-03	8.938520-03	5.800-02	6.293000-02	1.320-01	1.358140-01	1.180 00	5.926150-01	8.480	00-5.767240-01	
	9.00D-03	1.005010-02	5.900-02	6.397650-02	1.360-01	1.406030-01	1.230 00	5.966330-01	8.680	00-6.139260-01	
	1.000-02	1.11604D-02	6.000-02	6.502170-02	1.400-01	1.443710-01	1.280 00	5.997320-01	8.880	00-6.511270-01	
	1.100-02	1.226940-02	6.100-02	6.606550-02	1.440-01	1.481180-01	1.330 00	6.019740-01	9.080	00-6.88326D-01	
	1.200-02	1.337720-02	6.200-02	6.710810-02	1.480-01	1.519440-01	1.380 00	6.034160-01	9.280	00-7.255240-01	
-	1.300-02	1.448360-02	6.300-02	6.814930-02	1.520-01	1.555500-01	1.430 00	6.041130-01	9.480	00-7.627210-01	
	1-400-02	1.55888D-C2	6.400-02	6.918920-02	1.560-01	1.592350-01	1.48D CC	6.041150-01	9.680	00-7.999170-01	
	1.5CD-02	1.669260-02	6.500-02	7.022780-02	1.600-01	1.623990-01	1.530 00	6.034710-01	9.880	00-8.37111D-01	
	1.600-02	1.779520-02	6.600-02	7.126510-02	1.640-01	1.665420-01	1.580 00	6.022240-01	1.010	01-8.743050-01	
	1.700-02	1.889650-02	6.700-02	7.230110-02	1.680-01	1.701650-01	1.630 00	6.004150-01	1.030	01-9.114990-01	
	1.800-02	1.999650-02	6.800-02	7.333570-02	1.720-01	1.737570-01	1.680 00	5.98084D-01	1.050	01-9.486910-01	
	1.900-02	2.109530-02	6.900-02	7.436900-02	1.760-01	1.773490-01	1.730 00	5.952660-01	1.070	01-9.358830-01	
	2.000-02	2.219270-02	7.000-02	7.540100-02	1.800-01	1.809100-01	1.760 00	5.919950-01	1.090	01-1.023(80 00	-
	2.100-02	2.328880-02	7.100-02	7.043170-02	2.00D-01	1.984090-01	1.830 00	5.883020-01	1.110	01-1.050270 00	
	2.200-02	2.438370-02	7.200-02	7.746110-02	2.200-01	2.154030-01	1.880 00	5.842150-01	1.130	01-1.097460 00	
	2.300-02	2.547720-02	7.300-02	7.848920-02	2.400-01	2.318770-01	1.930 00	5.797630-01	1.150	01-1.134650 00	
	2.400-02	2.656950-02	1.400-02	7.951590-02	2.600-01	2.473990-01	1.980 00	5.749700-01	1.170	01-1.17184D 00	
-	2.500-02	2.766040-02	7.500-02	8.054130-02	2.800-01	2.634170-01	2.030 00	5.698610-01	1.190	01-1.209030 00	
	2.600-02	2.875010-02	7.600-02	8.156540-02	3.000-01	2.78+570-01	2.080 00	5.644560-01	1.210	01-1.24622D 00	
	2.7CD-02	2.98384D-C2	7.700-02	8.258820-02	3.200-01	2.930270-01	2.28D 00	5.402760-01	1.230	01-1.283410 00	
	2.800-02	3.092550-02	7.800-02	8.360970-02	3.400-01	3.071370-01	2.48D 00	5.127780-01	1.250	01-1.320600 00	
	2.900-02	3.201120-02	7.900-02	8.462930-02	3.600-01	3.207950-01	2.680 00	4.827940-01	1.270	01-1.357790 00	
	3.000-02	3.309570-02	8.000-02	8.564870-02	3.800-01	3.340090-01	2.880 00	4.509460-01	1.290	01-1.394980 00	
-	3.100-02	3.417890-02	8.100-02	8.606020-02	4.000-01	3.467880-01	3.080 00	4.177050-01	1.310	21-1.432170 00	
	3.200-02	3.526070-02	8.200-02	8.768240-02	4.200-01	3.5914:)0-01	3.280 00	3.834200-01	1.330	01-1.409360 00	2
	3.300-02	3.634130-02	8.300-02	8.869730-02	4.400-01	3.710750-01	3,480 00	3.483570-01	1.350	01-1.506540 00	
	3.400-02	3.742050-02	8.400-02	8.971080-02	4.600-01	3.826010-01	3.680 00	3.127130-01	1.370	01-1.543730 00	
	3.500-02	3.849850-02	8.500-02	9.072310-02	4.800-01	3.937270-01	3.850 00	2.766390-01	1.390	01-1.580920 00	
	3.600-02	3.957510-02	8.6CD-C2	9.173400-02	5.000-01	4.044620-01	4.080 00	2.402440-01	1.410	01-1.618110 00	
	3.700-02	4.065C4D-02	8.700-02	9.274360-02	5.200-01	4.148150-01	4.280 00	2.036130-01			
	3-80D-C2	4.172450-02	8.8CD-02	9.375190-02	5.400-01	4.247940-01	4.480 00	1.668090-01			
	3.900-02	4.279720-02	8.900-02	9.475880-02	5.600-01	4.34+070-01	4.680 00	1.298780-01			
	4.000-02	4.386860-02	9.000-02	9.576450-02	5.800-01	4.436640-01	4.880 00	9.285520-02			
	4.100-02	4.453870-02	9.100-02	9.676880-02	6.CCD-01	4.525730-01	5.080 00	5.576640-02			
	4-200-02	4.600750-02	9.200-02	9.777180-02	0.20D-C1	4.611420-01	5.280 00	1.863090-02			
_	4.300-02	4.7075CD-C2	9.300-02	9. 277350-02	6.400-01	4.693790-01	5.480 00	-1.853710-02			
	4-400-02	4.814120-02	9.400-02	9.977390-02	6.600-01	4.772930-01	5.680 00	-5.572720-02			
	4.500-02	4.920600-02	9.500-02	1.00773D-01	6.800-01	4.848910-01	5.880 00	-9.293190-72	1.		
	4.600-02	5.026960-02	9.6CD-C2	1.017710-01	7.000-01	4.921800-01	6.080 00	-1.301460-01			
	4.700-02	5.133190-02	9.700-02	1.027670-01	7.200-01	4.991/00-01	6.280 00	-1.673650-01			
	4-800-02	5.239280-02	9-800-02	1.037620-01	7.400-01	5.058670-01	6.480 00	-2.045860-01			
-	4.900-02	5.34524D-C2	9.900-02	1.047500-01	7.600-01	5.122780-01	6.680 00	-2.418080-01			
	5.00D-02	5.451070-02	1.000-01	1.05749D-01	7.800-01	5.18412D-01	6.880 00	-2.190290-01			

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<pre>1.000-03 1543400-01 17:010-02 2:01010-03 1:000-01 1:010-01 1:01030-01 1:0100-01 1:01030-01 1:01030-01 2:000-03 12333400-01 1:010-02 2:0100-03 1:000-01 1:010-01 1:0100-01 1:0100-01 2:000-03 12333400-01 1:010-02 2:010-03 1:010-01 1:010-01 1:0100-01 1:0100-01 2:000-03 12333400-01 1:010-02 2:010-00 1:010-010-01 1:010-01 2:000-03 1:3010-01 2:010-02 2:010-00 1:010-010-01 1:010-01 2:000-03 1:3010-01 2:010-01 1:010-01 1:010-01 1:010-01 2:000-03 1:3010-01 2:010-01 1:010-01 2:000-03 1:3010-01 2:010-01 1:010-01 2:000-03 1:3010-01 2:010-01 1:010-01 2:000-03 1:3010-01 1:010-01 2:000-03 1:3010-01 2:010-01 1:010-01 2:000-03 1:3010-01 1:010-01 2:000-03 1:3010-01 1:010-01 2:000-03 1:3010-01 1:010-01 2:000-03 1:3010-01 1:010-01 2:000-03 1:3010-01 1:010-01 2:000-03 1:3010-01 1:010-01 2:000-03 1:3010-01 1:010-01 2:000-03 1:3010-01 1:010-01 2:000-03 1:3010-01 1:010-01 2:000-03 1:3010-01 1:010-01 2:000-03 1:3010-01 1:010-01 2:000-03 1:3010-01 1:010-01 2:000-03 1:3010-01 1:010-01 2:000-03 1:3010-01 1:010-01 2:000-03 1:3010</pre>	Income Service of Service	RILI	DEVIENUN U-	R(L)	HILD NO.	RILL	W(L)	R(L)	M(L)	K(L)	M(L)	RILI
 2.4000-03 3.2213100-05 5.300-07 2.11910-00 1.120-01 1.2010-03 5.400-01 1.221930-01 7.280 00 1.159720-02 2.2000-03 5.3100-05 5.400-05 1.200-01 1.2010-01 1	 J. GODO-33 3 2313101-06 5.300-07 2.175300-03 1.120-01 1.275103-01 7.280 00 1.235370-02 1.25570-02 1.25770-02 1.25770-02 1.2500-02 1.2570-02 1.2500-02 1.2500-02 1.2500-02 1.2500-02 1.2570-02 1.2570-02 1.2570-02 1.2500-02	1.CCD-03	5.84664D-C7	5.100-02	2.028110-03	1.040-01	7.19556D-03	8.300-01	1.13166D-01	7.080 0	1.612220-07	
 MODCO 3 1393070-C5 5:100-C2 2:123400-01 1.120-01 5:400-01 1.221750-01 7:400 00 1.1237570-01 7:400 00 1.1237570-01 1.400-01 1.247590-01 1.417590-01 1.247590	<pre>Acc00-03 5.39300-04 5.3400-02 2.133490-01 1.130-01 8.144710-03 9.400-01 1.237390-01 7.440 00 1.236770-02 7.400 00 1.339710-01 2.7374790-01 1.140-01 8.144710-03 1.200 00 1.349710-01 8.460 00 1.236770-02 7.400 00 1.339710-01 1.400-01 1.400-01 1.400-01 1.400-01 1.400-01 1.400-01 7.400 00 1.347710-01 7.400 00 1.347710-01 8.444790-01 1.400-01 1.444710-02 1.200 00 1.347970-01 7.400 00 1.347710-01 7.400 00 1.347710-01 8.444790-01 1.400-01 1.436-01 1.13070 7.400 00 1.347710-01 8.400 00 1.357770-01 7.400 00 1.347710-01 7.400 00 1.347710-01 7.400 00 1.447720-01 7.400 00 1.447720-01 7.400 00 7.40000 7.400000 7.400000 7.400000 7.400000 7.400000 7.400000 7.400000 7.400000 7.400000 7.400000 7.400000 7.400000 7.400000 7.400000 7.400000 7.400000 7.400000 7.400000 7.400</pre>	2.000-03	3.82181D-C6	5°200-02	2.101460-03	1.080-01	7.675030-03	8.800-01	1.176910-01	7.280 0	1 1 48023D-02	
<pre># 000-03 1 2333300-05 2.237390-03 1.100-01 0.437110-03 9.600 1.2336000-11 7.600 00 1.133500-03 7.000-03 7.33390-05 2.437390-01 1.000-01 1.000 1.133500-01 2.630 00 1.133500-03 7.000-03 7.33390-05 2.437390-01 1.000-01 1.000 1.133500-01 2.630 00 1.133500-03 7.000-03 7.332500-05 2.437390-01 1.000-01 1.000 1.133500-01 2.630 00 1.437950-03 7.000-02 1.30720-01 2.247490-01 1.24110-02 7.000-02 1.30720-01 1.24110-02 7.000-02 1.30720-01 1.24110-01 1.24110-01 7.000-02 1.30720-01 1.24110-02 7.000-02 1.30720-01 1.24110-01 7.000-02 1.30720-01 1.24110-01 7.000-02 1.30720-01 1.24110-02 7.100-02 1.30720-01 1.24110-02 7.100-02 1.47110-01 7.000-02 1.47110-01 7.000-02 1.47110-01 7.000-02 1.47110-01 7.000-02 1.47110-02 7.100-02 1.47110-01 7.000-02 1.47110-02 7.100 7.100-02 1.47110-02 7.100-02 7.100 7.100-02 7.100-02 7.100-02 7.100-02 7.100 7.110 7.110 7.110 7.111 7.111 7.11 7.</pre>	 A.000-31 3.33309-05 3.400-07 2.43739-01 1.400-01 0.477110-01 9.4501 00 1.339590-01 4.4610 01.453570-02 A.000-31 3.33309-05 3.400-07 2.447390-01 1.400-01 1.400-01 1.4010-01 1.4010-01 1.4010-01 0.4810 00 4.473790-01 A.000-31 2.335920-05 4.000-02 2.474590-01 1.400-01 1.4010-01 1.4010-01 1.4010-01 1.4010-01 1.4010-01 1.4010-01 A.000-21 2.374590-05 4.000-02 2.474590-01 1.400-01 1.4410-02 1.330 00 1.470100-01 8.480 00 0.439780-01 A.000-21 2.374590-06 4.000-02 2.474590-01 1.400-01 1.4410-02 1.430 00 1.470100-01 8.480 00 0.439780-01 A.000-21 2.37450-06 4.000-02 2.474590-01 1.400-01 1.4410-02 1.430 00 1.471040-01 8.480 00 0.439780-01 A.000-21 2.37450-06 4.000-02 2.474570-01 1.400-01 1.44110-02 A.000-22 2.44400-01 1.4410-01 1.4410-01 1.44110-02 A.000-22 2.44400-01 1.4410-01 1.44110-02 A.000-22 2.44400-01 1.44110-01 1.44110-02 A.000-22 2.44400-01 1.44110-01 1.44110-01 1.44110-01 1.44110-01 A.000-22 2.44400-01 1.400-01 1.44110-02 A.000-22 2.44400-01 1.44110-01 1.44110-01 1.44110-02 A.000-22 2.44400-01 1.44110-02 A.000-22 2.44400-01 1.44110-02 A.000-22 2.44400-01 1.44110-02 A.000-22 2.44400-01 1.44110-02 A.000-22 2.44110-02 A.000-22 2.44110-02<!--</td--><td>3.000-03</td><td>8.536900-C6</td><td>5.300-02</td><td>2.175900-03</td><td>1.120-01</td><td>8.164870-03</td><td>9.300-01</td><td>1.217630-01</td><td>7.480 0</td><td>1.360920-02</td><td></td>	3.000-03	8.536900-C6	5.300-02	2.175900-03	1.120-01	8.164870-03	9.300-01	1.217630-01	7.480 0	1.360920-02	
<pre>compond ::::::::::::::::::::::::::::::::::::</pre>	 A. MORDON J. A. MARDONE C. S. MANDONE J. LANDON D. M. MANDONE J. LANDONE J. MANDONE J.	4. COD-03	1-508370-C5	5.4CD-02	2.251400-03	1.160-01	8-66471D-03	9.800-01	1.253960-01	7-680 0	1-253070-02	
 March 31 ANSTRUCT 31 AND TARGENED 1 LAND TARGENED	 	50-000°C	2.34330U-02	20-006.6	2. 32 1960-03	10-002-1	9-174140-03	1.030 00	1.286100-01	1.8810	20-044411 0	
 M. M. C. M. M.	 M. C. M. M.	6.000-03	3-319610-05	5.6CU-02	2.405570-03	1-240-01	9.692960-03	1.080 00	1.314240-01	8.080 0	1.067370-02	
<pre># conc-d</pre>	 Marcoll 7, Namber 5, Sander 5, Sander 1, Lay 2001, L	1.000-03	4.243390-05	20-001 -02	2.+H4220-03	10-082-1	1.022010-02	1.130 00	10-0/6866.1	8.280 0	60-019218-b (
<pre>1.000-02 01:0393DF0: 0.00002 01:0393DF0: 0.00002 01:0393DF0: 0.04004001 01:03000-01 1.000-02 11:0373DF0: 0.00002 01:03739DF0: 0.00002 01:0373DF0: 0.04004000 1.000-02 11:0373DF0: 0.00002 01:0373DF0: 0.00002 01:0373DF0: 0.04004000 1.000-02 11:0373DF0: 0.00002 01:0373DF0: 0.00002 01:0373DF0: 0.04004000 1.000-02 11:037DF0: 0.00002 01:0377DF0: 01:037DF0: 01:040000 1.00002 01:04004000 01:04004000 1.000-02 10:030DF0: 01:04004000 1.000-02 10:030DF0: 01:0400400 1.00000 01:0400400 1.00000 01:0400400 1.00000 01:0400400 1.00000 01:040040 1.00000 01:040040 1.00000 01:040040 1.00000 01:040040 1.00000 01:040040 1.00000 01:040040 1.00000 01:040040 1.00000 01:040040 1.00000 01:040040 1.00000 01:040040 1.00000 01:040040 1.0000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0</pre>	 1.000-02 10 (3373) (2000 (2) (2) (2000 (2) (2) (2000 (2) (2) (2) (2) (2) (2) (2) (2) (2) (2)	8°000-03	20-0020757 C	20-0.08 - 6	2. 203890-03	10-076-1	20-00/0201	1.150 00	10-0156551	8.480 0	EC-058561.9 0	
<pre>1.000-02 *13252-05 *100-02 *1726700-01 *1241370-02 *1350 01 *1411370-01 *226 00 05 *333700-07 1.000-02 *137370-01 *2717200-01 *1241710-01 *1241710-01 *124170-01 *124170-01 *124170-01 1.000-02 *137370-01 *1241710-01 *1241710-01 *1241710-01 *1241710-01 *1241710-01 1.000-02 *137370-01 *1241710-01 *1241710-01 *1241710-01 *1241710-01 *1241710-01 1.000-02 *1353900-06 *1710-02 *127500-01 *1241710-02 *12400 01 *141110-01 *1241710-01 1.000-02 *1353900-06 *1710-02 *127500-01 *1241710-02 *124170-02 *124170-00 1.000-02 *1353900-06 *1710-02 *127500-01 *1241710-02 *12400 00 *1451390-01 1.000-02 *1353900-06 *1710-02 *127500-01 *1241710-02 *15500 01 *141110-01 *1050 01 *253490-01 1.000-02 *1353900-06 *1710-02 *1241710-02 *124170-02 *1050 01 *1241710-01 *1250 01 2.000-02 *1353900-06 *1710-02 *127500-01 *1241710-02 *1050 01 *137590-01 2.000-02 *1353900-06 *1710-02 *127500-01 *1241710-02 *1050 01 *1375900-01 2.000-02 *1353900-06 *1710-02 *127500-01 *1241710-02 *1050 01 *1375900-01 2.000-02 *1353900-06 *1710-02 *127500-01 *1241710-02 *1050 01 *1375900-01 2.000-02 *1353900-06 *1710-02 *127500-01 *1241710-02 *13900 11 *279170-01 2.000-02 *1353900-06 *1710-02 *1253900-01 *1210 01 *239390-01 2.000-02 *1353900-06 *1710-02 *1253900-01 *1210 01 *123900 2.000-02 *1353910-03 *100-01 *123900-01 *123900 11 *239390-01 2.000-02 *1353910-03 *100-01 *123900-01 *123900 11 *239390-01 2.000-02 *1353910-03 *100-01 *123900-01 *123900 11 *239390-01 2.000-02 *1353910-03 *100-01 *123900-01 *123900 11 *239390-01 2.000-02 *1353910-03 *100-01 *123900 11 *2391390-01 2.000-02 *1353910-03 *100-01 *123900-01 *123900 11 *2391390-02 2.000 01 *1393910-01 *123900 11 *2391390-01 2.000-02 *1353910-03 *10000 11 *123900 11 *2391390-01 2.000-02 *1353910-03 *10000 11 *123900 11 *2391390-01 2.000-02 *1353910-03 *10000 11 *123900 11 *2391390-02 2.000 01 *1393910-01 *123900 11 *2391390-01 2.000-02 *1353910-03 *10000 11 *123900 11 *2391390-01 2.000-02 *1353910-03 *10000 11 *123900 11 *2391390-02 2.000 01 *1393910-01 *2391390-02 2.000 01 *1393910-01 *2391390-02 2.000 01</pre>	<pre>1.000-02 * 1.377370-03 * 1.37770-03 * 1.37770-03 * 1.390 * 01 * 1.47970-03 * 0.377570-03 * 1.300-02 * 1.377570-55 * 5.77770-03 * 1.479770-03 * 1.390 * 01 * 1.47970-01 * 2.200 * 00 * 4.47570-03 * 1.400-02 * 1.377570-56 * 4.570-02 * 3.72770-03 * 1.479770-02 * 1.390 * 01 * 1.475940-03 * 1.400-02 * 1.377570-56 * 4.570-02 * 3.72770-03 * 1.479770-02 * 1.390 * 01 * 1.417970-01 * 2.490 * 00 * 4.44540-03 * 1.400-02 * 1.4757960-66 * 7.700-02 * 3.72770-03 * 1.479770-02 * 1.390 * 01 * 1.417970-01 * 2.490 * 00 * 4.44540-03 * 1.400-02 * 1.4937910-66 * 7.700-02 * 3.72770-03 * 1.479770-02 * 1.490 * 01 * 1.417970-03 * 1.400-02 * 1.493970-66 * 7.700-02 * 3.72770-03 * 1.47970-02 * 1.400 * 01 * 1.417970-03 * 1.400-02 * 1.493970-67 * 1.000-02 * 3.72790-03 * 1.400 * 01 * 1.414970-03 * 1.400-02 * 1.493970-67 * 1.000-02 * 3.7770-03 * 1.41970-02 * 1.400 * 01 * 1.417970-03 * 1.400-02 * 1.400-02 * 3.77790-03 * 1.4100-02 * 1.4100-02 * 1.4100 * 01 * 1.475990-03 * 1.400-02 * 1.400-02 * 3.77790-01 * 1.414770-02 * 1.4100 * 01 * 1.475990-03 * 1.400-02 * 1.400-02 * 3.77790-01 * 1.414770-02 * 1.400 * 01 * 1.475990-03 * 1.400-02 * 1.475970-03 * 1.400-01 * 1.414770-02 * 1.4100 * 01 * 3.75950-01 * 1.4100 * 1.425990-03 * 1.400-02 * 1.475970-03 * 1.400-01 * 1.414770-02 * 1.400 * 01 * 1.475970-03 * 1.400-02 * 1.475770-03 * 1.400-01 * 1.414770-02 * 1.4100 * 1.425970-03 * 1.400-02 * 1.477970-01 * 1.400-02 * 1.71470-02 * 1.400 * 01 * 1.475770-01 * 1.475770-03 * 1.400-02 * 1.477570-03 * 4.600-03 * 4.600-01 * 4.775770-01 * 1.475770-01 * 1.275970-03 * 1.400-02 * 1.477570-03 * 4.600-03 * 4.600-01 * 1.475770-00 * 1.475770-00 * 1.400-02 * 1.47770-02 * 1.47770-02 * 1.47970-02 * 1.4900-02 * 1.4900-02 * 1.4000-02 * 1.47970-00 * 1.400-02 * 1.47770-02 * 1.47770-00 * 1.4000-02 * 1.4000-02 * 1.4000-02 * 1.47770-00 * 1.400-02 * 1.47770-00 * 4.477470-02 * 1.4700-02 * 1.4990-00 * 1.477470-00 * 1.400-02 * 1.47770-00 * 1.477470-02 * 1.477470-00 * 1.4990-00 * 1.477470-00 * 1.400-02 * 1.477570-03 * 4.600-01 * 1.477470-00 * 1.4900-00 * 1.4990-00 * 1.400-02 * 1.477570-03</pre>	50-303°6	1.434340-05	20-006.0	50-066660°7	1360-01	20-011051=1	1.230 00	12 (0000-01	0 (189 °P	50-00000cc*8 0	
<pre>1.100-02 1.03930-16 4.100-02 2.054500-03 1.440-01 1.2392700-02 1.430 00 1.441510-01 9.260 00 6.439400-03 1.400-02 1.2235930-16 4.100-02 2.054500-03 1.4400 01 1.234160-01 9.250 00 1.441510-01 9.260 00 6.439400-03 1.400-02 1.2235930-04 4.000-02 2.054700-01 1.237210-021 1.630 01 1.441510-01 9.260 00 6.434440-03 1.400-02 1.235930-04 4.000-02 2.4354500-03 1.4200 00 1.441510-01 01 4.253440-03 1.400-02 1.455390-04 4.000-02 2.4354500-03 1.4700 00 1.441510-01 1.455300-03 1.400-02 1.455390-04 1.000 01 4.453440-03 1.400-02 1.455390-04 4.000-02 2.4554500-03 1.4500 00 1.441510-01 01 4.757770-03 2.400-02 1.459390-04 1.000 01 4.59340-03 2.400-02 1.459390-04 1.000 01 4.453400-03 2.400-02 1.459390-04 1.000 01 4.453400-03 2.400-02 1.459390-04 1.000 01 4.45390-03 2.400-02 1.459390-04 1.000 01 4.45390-03 2.400-02 1.459390-04 1.000 01 4.45390-03 2.400-02 1.459390-04 1.000 01 4.45390-03 2.400-02 1.459390-04 1.000 01 4.45390-03 2.400-02 1.459390-04 1.000 01 4.45390-03 2.400-02 1.459390-04 1.000 01 4.45390-03 2.400-02 1.459390-04 1.000 01 4.45390-03 2.400-02 1.459390-04 2.400-02 1.459390-03 1.400-01 1.40090-02 1.400 00 01 1.455390-01 2.455490-03 2.400-02 1.459390-04 1.4100-02 1.40090-01 2.40010 1.455990-03 2.400-02 1.459390-04 2.400-02 1.471710-02 1.471710-02 1.471710-01 1.471910-01 2.455490-03 2.400-02 1.459390-04 1.4100-02 1.401910-01 2.4010-01 1.471910-01 2.455490-03 2.400-02 1.459390-04 1.4100-02 1.471720-02 1.4300 101 1.47290-02 2.400-02 1.471710-02 1.471710-02 1.471710-02 2.400-02 1.471710-02 2.400-02 1.471710-02 2.4010-01 1.471710-02 2.4010-01 1.471710-02 2.4010-01 1.471710-02 2.4010-01 1.471710-02 2.4010-01 1.471710-02 2.4010-01 1.471720-02 2.4010 2.4010-02 2</pre>	<pre>1.100-02 1.03973D-t6 4.100-02 2.454500-03 1.440-01 1.424160-07 1.3597 07 01 4.410190-01 9.260 00 6.433400-07 1.400-02 1.232490-t6 4.507-02 2.457790-03 1.440-01 1.424160-07 1.42690-01 9.260 00 6.434940-07 1.4500-02 2.429390-t6 4.507-02 2.427790-03 1.440-01 1.427713-01 2.4490 07 01 4.44299-01 01 5.38740-01 1.400-02 2.429390-t6 4.507-02 2.427790-01 1.477713-01 1.2010 01 4.44299-01 01 5.38740-01 2.400-02 2.429390-t6 4.507-02 2.427790-01 1.477710-02 1.4200 00 1.4415970-01 1.4201 00 1.4759340-01 2.400-02 2.429390-t6 4.507-02 2.427790-01 1.477710-02 1.4200 00 1.4415970-01 1.400 01 4.459340-03 2.4500-02 2.429390-t6 4.507-02 2.425770-01 1.477710-02 1.4200 00 1.239579-01 1.100 01 2.459340-01 2.4500-02 2.429900-t1 7.500-02 2.459770-01 2.4701 00 01 235579-01 1.100 01 2.459340-03 2.4500-02 2.429900-t1 7.500-02 2.459770-01 2.4701 00 01 235579-01 1.100 01 2.459340-03 2.4500-02 2.49900-t1 7.500-02 2.459770-00 1.447770-02 2.4600 01 1.2500 11.2500 11.2700 11.2700 11.270920-03 2.4500-02 2.449900-t1 7.500-02 4.457970-03 2.4600 01 1.2301 1.2200 11.2200 11.2709101 2.7395570-01 2.4500-02 2.449900-t1 7.500-02 4.457970-00 2.4400 00 1.11170 01 2.739570-01 2.4500-02 1.4277910-00 11.2500 11.2200 11.2200 11.2200 11.2200 11.2200 11.2200 11.2200 11.2200 11.2700 11.2700 11.2709570-03 2.4500-02 1.4277910-00 2.4457970-00 2.4400 00 01 1.2301 01 2.7395790-01 2.4500-02 1.4277910-02 4.457970-00 2.4400 00 01 1.2301 01 2.7395790-01 2.4500-02 1.4277910-03 4.4000 01 1.477770-02 4.4500 00 2.447770-02 4.4500 00 11.2200 11.2200 11.2200 11.2200 11.2700 10 1.2709570-03 2.4500-02 1.4277970-03 4.400-02 4.457770-01 4.427970-02 4.4500 00 01 1.2200 11.2200 11.2200 11.2200 11.2700 11.2700 10 1.2795570-03 2.4500-02 1.447770-02 4.457770-03 4.4000-01 4.477770-02 4.447970-02 4.44</pre>	1.000-02	9.133210-05	6.000-UZ	2.726290-03	1.400-01	1.185430-02	1.280 00	1.39081D-01	8.880 0	7.907580-03	
<pre>1.400-02 1.30730-04 6.200-02 2.402700-03 1.4480-01 1.2593240-03 1.4500 00 1.4418340-01 9.480 00 6.479370-03 1.400-02 2.593690-04 6.200-02 2.402700-01 1.4717370-02 1.450 00 1.4418340-01 1.4201 00 6.479370-03 1.400-02 2.593690-04 6.200-02 2.40270-01 1.4717370-02 1.450 00 1.4418340-01 1.401 01 15.2938470-03 1.400-02 2.593690-04 6.200-02 2.40270-01 1.4717370-02 1.450 00 1.4418340-01 1.401 01 15.2938470-03 2.2000-02 2.593690-04 7.100-02 2.40270-01 1.4717370-02 1.450 00 1.4418340-01 1.101 01 15.293840-03 2.2000-02 2.593690-04 7.100-02 2.40210-01 1.471770-02 1.450 00 1.4418340-01 1.101 01 15.473770-0 2.2000-02 2.493820-04 7.100-02 2.40210-01 2.471570-02 1.450 00 1.3418340-01 1.1101 01 1.477370-0 2.2000-02 2.493820-04 7.100-02 2.40210-01 2.471570-02 1.450 00 1.336250-01 1.110 01 1.477370-0 2.2000-02 5.4949950-04 7.100-02 2.40110-00 1 2.471490-02 1.450 00 1.336540-01 2.2000-02 5.4949950-04 7.100-02 2.40110-00 1 2.471490-02 1.420 00 1.336540-01 2.2000-02 5.4949950-04 7.100-02 2.40110-00 1 2.471490-02 1.420 00 1.336540-01 2.2000-02 5.4949950-04 7.100-02 4.421390-01 2.471490-02 1.220 00 1.2307390-01 2.2000-02 5.4949950-04 7.100-02 4.421390-01 2.471490-02 2.480 00 1.2301390-01 2.2000-02 5.489990-04 7.200-23 4.471490-02 1.471490-02 2.480 00 1.2301390-01 2.2000-02 5.489990-04 7.200-23 4.471490-02 1.471490-02 2.480 00 1.2301390-01 2.2000-02 7.489390-04 1.2200 01 1.2200 01 1.2200 01 1.2200 01 1.2200 01 2.2000-02 7.489390-04 4.400-01 4.412310-02 2.480 00 1.2011390-01 1.2200 11 2.201990-03 2.400-22 2.480 00-04 4.400-24 4.471490-02 2.480 00 01 1.2201 01 2.201990-03 2.400-22 2.480 00-04 4.400-24 4.471490-02 2.480 00 01 1.2200 10 1.220190-01 2.480 00 01 2.481490-02 2.480 00 01 2.481490-02 2.480 00 01 2.481490-02 2.480 00 01 2.481490-02 2.480 00 01 2.481490-02 2.480 00 01 2.481490-02 2.480 00 01 2.481490-02 2.480 00 01 2.481490-02 2.480 00 01 2.481490-02 2.480 00 01 2.481490-02 2.480 00 01 2.481490-02 2.480 00 02 2.481490-02 2.480 00 02 2.481490-02 2.480 00 02 2.481490-02 2.480 00 02 2.481490-02 2.480 00 02 2.481490-02 2.480 00</pre>	1.400-02 1.400-02 1.400-02 1.400-02 1.400-02 1.400-01 0.44010-01 0.44010-01 0.44010-01 1.400-02 2.402100-04 0.4001-02 2.402700-01 1.400-01 0.44010-01 0.44010-01 0.44010-01 1.400-02 2.402100-04 0.4001-02 2.402700-01 1.400-01 0.44010-01 0.44010-01 1.400-02 2.40210-04 0.4001-02 1.40110-01 0.44010-01 0.44010-01 1.400-02 2.40210-02 3.40110-01 3.40110-01 1.40110-01 0.44010-01 1.400-02 2.40110-02 3.40110-01 3.40110-01 1.40110-01 4.40110-01 2.400-02 3.40110-01 3.40110-01 3.40110-02 3.40110-01 3.40110-01 2.400-02 3.40110-01 3.40110-02 3.40110-01 3.40110-01 3.40110-01 2.400-02 4.40110 3.40110-02 3.40110-01 3.40110-01 3.40110-01 3.40100-01 2.400-02 4.40110 3.40110-02 3.40110-02 3.40110-01 3.40100-01 3.40100-01 3.40100-01 2.400-02 4.40110 3.40100-02 <	1.100-02	1.09982D-C4	6.10D-02	2.809000-03	1.440-01	1.241460-02	1.330 OC	10-086104.1	9.080 0	7.370450-03	
1.400-02 1.521830-04 6.5070-02 3.194707-05 1.590701 1.4010-02 1.4010-01 9.4610 00 6.4144957-01 1.400-02 2.595950-04 6.5070-02 3.1947070-05 1.5070-01 1.477710-02 1.590 01 4.477770-03 1.400-02 2.595950-04 6.5070-02 3.1947070-05 1.5070-01 1.477770-02 1.590 01 4.477770-03 1.400-02 2.595950-04 7.0010-02 3.57590-01 1.500-01 1.477770-02 1.590 01 4.777770-03 1.400-02 2.595950-04 7.0010-02 3.575590-02 1.480 01 4.77770-03 1.590 01 4.777770-03 2.4000-02 3.495970-04 7.0010-02 3.475790-02 1.590 01 1.477770-03 1.590 01 4.777770-03 2.4000-02 3.497770-03 1.7000-02 1.590 01 1.477770-03 1.590 01 1.477770-03 1.590 01 1.777770-03 1.590 01 1.777770-03 1.590 01 1.777770-03 1.590 01 1.777777770-03 1.590 01 1.47777	1.400-02 1.535395-04 4.500-02 2.677300-05 1.505700 1.4600-02 1.6400-01 1.6400-02 1.6400-02 1.6400-01 1.6400-02 1.6400-01 1.6400-02 1.6400-01 1.6400-01 1.6400-01 1.6400-01 1.6400-02 1.6400-01 1.6400-02 1.6400-01 1.6400-01 1.6400-01 1.6400-01 1.6400-01 1.6400-01 1.6400-01 1.6400-01 1.6400-01 1.6400-01 1.6400-01 1.6400-01 1.6400-01 1.6400-01 1.6400-01 1.6400-01 1.6400-01 1.6400-01	1.200-02	1.30272D-C4	6.200-02	2.892700-03	1.480-01	1 = 298240-02	1.330 00	1.410340-01	9.280 0	0 6.833060-03	
1.400-22 2.073970-76 6.400-02 3.003400-76 6.600-02 3.27740-73 1.600-01 9.600 00 6.472390-76 6.600-62 3.277740-73 1.600-01 9.600 00 6.472390-76 6.600-62 3.277740-73 1.600-01 9.600 01 4.672390-76 6.600-62 3.277740-73 1.600-02 3.75730-73 1.600-01 1.600 1.600 01 4.672390-76 1.600 01 4.777770-70 1.600 01 4.777770-70 1.600 01 4.777770-70 1.600 01 4.777770-70 1.600 01 4.777770-70 1.600 01 4.777770-70 1.600 01 4.777770-70 1.600 01 4.777770-70 1.600 01 4.777770-70 1.600 01 4.777770-70 1.600 01 4.777770-70 1.77770-70 1.600 01 4.777760-70 1.600 01 4.77760-70 1.600 01 4.77760-70 1.7200-70 1.7200-70 1.7200-70 1.7200-70 1.7200-70 1.7200-70 1.7200-70 1.7200-70 1.7200-70 1.7200-70 1.7200-70 1.7200-70 1.7200-70 1.720	1.*600-02 :.003700-06 :.000-02 :.003700-06 :.000-02 :.003700-06 :.000-02 :.003700-06 :.000-01<	1.300-02	1.521830-04	6.300-02	2.977390-03	1.520-01	1.355720-02	1.430 00	1.416100-01	9.480 0	0 6.440450-03	
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1900-05 3 453900-06 3 457590-01 1 775001 1 775207-02 1 775001 1 775207-02 1 775000-02 1 775000-02 1 775500-02 1 775	1.000-07 3.000000 3.000000 1.700010 3.000000 1.700010 3.77590-01 1.77590-01 <t< td=""><td>1 200-02</td><td>2 554540-04</td><td>5 7CD-02</td><td>2 275770-03</td><td>10-089-1</td><td>1 602230-02</td><td>1 630 00</td><td>1 414530-01</td><td>1 020 0</td><td>5 036800-03</td><td></td></t<>	1 200-02	2 554540-04	5 7CD-02	2 275770-03	10-089-1	1 602230-02	1 630 00	1 414530-01	1 020 0	5 036800-03	
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2.4300-02 4.461730-03 2.400-01 2.435570-01 1.4170 01 3.555470-01 2.405460-07 2.400-02 4.40617100-03 2.406170-01 2.445100 01 1.555770-01 1.1170 01 3.555470-03 2.400-02 5.449500-07 4.607110-03 2.400170 3.455470-03 2.400170 1.4270 1.2570 1.210 1.2570 1.210 1.2570 1.210 1.2570 1.210 1.2570 1.2700 1.2700 1.2700 1.2700 1.2570 1.2700 1.2570 1.2700 1.2570 1.2700 1.2570 1.2700 1.2570 1.2700 1.2570 1.2700 1.2700 1.2570 1.2700 1.2570 1.2700 1.2700 1.2700 1.2757 1.2700	2.4000-02 4.94520-06 7.500-02 3.976300-03 2.460-01 2.75160-02 1.990 00 1.555370-01 1.170 01 3.578300-03 2.4000-02 4.94520-06 7.500-02 4.6137100-03 2.460-01 3.475170-02 2.000 01 1.251101 1.1250 01 3.578300-03 2.5000-02 5.1453710-06 4.200-02 4.6137100-03 2.4600 00 1.121101 1.250 01 3.578450-03 2.6000-02 5.19326-04 7.700-02 4.213710-03 3.400-01 4.423710-02 2.000 01 1.251101 1.250 01 3.578450-03 2.000-02 1.681710-06 4.200-02 4.213710-03 3.400-01 4.427970-02 2.460 00 1.1211001 1.250 01 2.709360-03 3.000-02 1.681710-06 4.200-02 4.429990-03 3.400-01 4.427970-02 2.460 00 1.1117001 2.700 01 2.709360-03 3.000-02 1.681710-06 4.200-02 4.429990-03 3.400-01 4.427970-02 2.460 00 1.1117001 2.700 01 2.709360-03 3.000-02 1.681710-06 4.200-02 4.429990-03 3.400-01 4.427970-02 1.1200 01 2.70970-03 3.400-02 4.30130-06 4.200-02 4.477750-03 4.400-01 4.477970-02 1.1200 01 2.70970-03 3.400-02 4.30130-06 4.200-02 4.477750-03 4.400-01 4.477970-02 1.1200 01 2.70970-03 3.400-02 4.47170-03 4.000-02 4.477750-03 4.400-01 4.47750-02 1.477100 12.248900-03 3.400-02 1.400270-03 4.600-01 4.47750-03 2.400-01 4.47750-02 1.4770 01 2.748900-03 3.400-02 1.477270-03 4.600-01 4.47750-03 2.400-01 4.47750-02 1.4770 01 2.748900-03 3.400-02 1.477270-03 4.600-01 4.47750-03 2.400-01 4.47750-02 1.4770 01 2.748900-03 3.400-02 1.47770-03 4.000-02 5.47770-03 5.400-01 4.47750-02 1.4770 01 2.749500-03 4.400-02 1.47770-03 4.000-02 5.47770-03 5.400-01 4.47750-02 1.47770-02 4.400-02 1.47770-03 4.000-01 4.47750-03 2.400-02 5.47770-02 1.47770-02 4.400-02 1.47770-03 4.000-01 4.47750-02 5.4800 00 3.477550-02 4.400-02 1.497570-03 4.000-01 4.47750-02 5.49950-03 4.400-02 1.499570-03 9.400-02 5.477570-01 1.47750-02 1.47750-02 4.400-02 1.497570-03 9.400-02 5.477570-02 5.49950-03 6.400-01 4.27550-02 4.400-02 1.497570-03 9.400-02 5.477570-02 5.49950-03 7.000-01 4.47750-02 1.47750-02 4.400-02 1.497550-03 9.400-02 5.477570-02 1.4995670-02 2.57560-02 4.400-02 1.495540-03 9.400-02 5.477570-02 1.4995670-02 2.575560-02 4.400-02 1.495540-03 9.400-02 5.477570-03 1.499570-02 2.57560-02 4.4	2.200-02	4.192870-04	1-200-02	3. 782330-03	10-002°2	20-04/1140-05	1.880 00	1.377860-01	1.130 0	3.854480-03	
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Ze300-02 5-375350-04 7.650-02 4.1057100-03 2.4807-01 3.435190-02 2.480 00 1.251130-01 1.230 01 3.239450-03 2.700-02 6.491260-04 7.650-02 4.261390-03 3.400-01 4.428190-02 2.480 00 1.161190-01 1.250 01 3.219990-03 3.500-02 1.521790-64 7.500-02 4.559910-03 3.400-01 4.4281910-02 2.480 00 1.1611900-01 1.250 01 2.479590-03 3.500-02 1.521790-64 7.500-02 4.559910-03 3.400-01 4.421910-02 2.480 00 1.1611900-01 1.250 01 2.477590-03 3.500-02 1.521790-64 8.100-02 4.5600720-03 4.500-01 5.4873101-02 2.480 00 1.16710 01 2.6775790-03 3.500-02 1.525730-64 8.100-02 4.5600720-03 4.500-01 5.487310-02 2.480 00 1.177510-01 1.26775790-03 3.500-02 1.525730-64 8.200-02 4.4660720-03 4.500-01 5.487390-02 1.4810 01 2.477570-01 3.500-02 1.525730-64 8.200-02 4.4660720-03 4.500-01 5.4873300-02 2.480 00 6.4813670-02 1.370 01 2.477570-03 3.500-02 1.525730-64 8.200-02 4.4660720-03 4.500-01 5.481340-02 4.480 00 6.4813670-02 1.370 01 2.477570-03 3.500-02 1.527700-68 8.400-02 5.407510-03 4.400-01 4.414440-02 4.480 00 6.4777550-02 1.4910 01 2.477570-03 3.500-02 1.177720-03 8.600-02 5.494560-03 4.400-01 4.414440-02 4.480 00 6.477750-02 1.4910 01 2.438900-03 3.600-02 1.177720-03 8.600-02 5.499510-03 5.600-01 8.4074470-02 4.480 00 6.477750-02 1.2910 01 2.438900-03 3.600-02 1.177720-02 8.50070-03 5.600-01 8.40710-02 4.680 00 5.7411470-02 3.600-02 1.177720-02 8.607890-03 5.600-01 8.40710-02 4.680 00 5.7411470-02 4.400-02 1.177720-02 8.50070-03 5.600-01 8.40710-02 4.680 00 5.7471470-02 4.400-02 1.177720-02 8.50070-03 5.600-01 8.40710-02 4.680 00 5.4711470-02 4.400-02 1.177720-02 5.49910-03 5.600-01 8.42101-02 4.680 00 5.4711470-02 4.400-02 1.177720-02 5.49910-03 5.600-01 8.422101-02 5.680 00 5.4711470-02 4.400-02 1.44181290-03 5.400-01 9.4000-01 9.421110-02 5.680 00 5.4711470-02 4.400-02 1.44181290-03 5.400-01 9.42010-02 5.680 00 5.4711470-02 4.400-02 1.44181290-03 5.400-01 9.421110-02 5.680 00 5.4711470-02 4.400-02 1.44181290-03 5.400-01 9.421110-02 5.680 00 5.4711470-02 4.400-02 1.4418290-03 5.4000-01 9.4200-01 9.421110-02 5.680 00 5.471470-02 4.400-02	Z. 4000-02 5. 4149500-04 7. 6067190-03 J. 2007-01 3. 44510-02 Z. 2003 00 01. 23100-01 1. 210 01 3. 239520-03 2. 7000-02 6. 4191260-04 7. 7000-02 4. 261930-03 3. 2007-01 4. 1281791-02 Z. 2618 00 01. 129110-01 1. 251 01 2. 2991090-03 2. 7000-02 6. 4391260-04 7. 7000-02 4. 559931-03 3. 600-01 4. 421971-02 Z. 648 00 01. 1129130-01 1. 251 01 2. 2991090-03 2. 2000-02 1. 6217391-04 8. 7000-02 4. 4559931-03 3. 600-01 4. 421971-02 Z. 648 00 01. 1129130-01 1. 251 01 2. 479350-03 3. 2000-02 8. 439332700-04 8. 7000-02 4. 4559931-03 3. 600-01 4. 421911-02 Z. 648 00 01. 1129130-01 1. 251 01 2. 6739597-03 3. 2000-02 8. 459126-04 8. 7000-02 4. 4559991-03 4. 600-01 5. 5108300-02 2. 548 00 01. 717350-02 1. 330 01 2. 573970-03 3. 2000-02 8. 45910-04 8. 4000-02 4. 455970-03 4. 400-01 1. 411010-02 4. 468 00 07 7. 510260-02 1. 337 01 2. 573970-03 3. 5000-02 8. 45000-03 8. 4000-01 8. 4500-01 1. 421840-02 4. 468 00 07 5. 175950-02 1. 337 01 2. 573970-03 3. 5000-02 1. 1271220-03 8. 4000-01 1. 411110-02 4. 468 00 07 5. 175950-02 1. 377 01 2. 479550-03 3. 5000-02 1. 1271220-03 8. 6000-02 5. 479570-03 5. 6000-01 1. 7141440-02 4. 688 00 04. 177550-02 1. 377 01 2. 479550-03 3. 5000-02 1. 1271220-03 8. 6000-02 5. 44900-01 1. 7141440-02 4. 688 00 04. 477450-02 4. 6000-02 1. 1271220-03 8. 6000-03 5. 44900-01 1. 7141440-02 4. 688 00 04. 477450-02 4. 6000-02 1. 1271220-03 8. 6000-03 5. 6400-01 1. 7754490-02 4. 688 00 04. 477450-02 4. 6000-02 1. 1271220-03 8. 6000-02 5. 643910-03 8. 4000-01 1. 4795490-02 4. 6000-02 1. 1271220-03 8. 6000-03 5. 4400-01 1. 4000-02 1. 4795490-02 4. 6000-02 1. 1271220-03 8. 6000-03 5. 643910-03 8. 4000-01 1. 4795490-02 4. 6000-02 1. 141810-03 9. 2000-02 5. 429310-03 8. 4000-01 1. 4795490-02 4. 6000-02 1. 141810-03 9. 4000-01 1. 401810-02 5. 4400 00 2. 279540-02 4. 6000-02 1. 141810-03 9. 4400-02 5. 429310-03 8. 4000-01 1. 4795490-02 4. 6000-02 1. 141810-02 5. 449310-03 9. 4400-01 1. 479540-02 4. 6000-02 1. 1475560-03 9. 4400-01 1. 401810-02 5. 4400 00 0. 2715560-02 4. 6000-02 1. 1475560-03 9. 4400-02 5. 459310-03 9. 4	2.400-02	4.949850-04	7-400-02	3.971290-03	2.600-01	3.091400-02	1.980 00	1.353570-01	1.17D 0	1 3-520830-03	
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4.100-02 1.356110-03 9.100-02 5.71367D-03 6.000-01 8.62210D-02 5.680 00 3.63254D-02 4.200-02 1.441811U-03 9.200-02 5.4331D-03 6.200-01 9.43057D-02 5.480 00 3.31259D-02 4.300-02 1.441811U-03 9.500-02 5.4310-03 5.400-01 9.4307D-02 5.460 00 3.1129D-02 4.400-02 1.6511180-03 9.500-01 9.400-01 9.4600-01 9.4600-02 5.460 00 3.7121D-02 4.400-02 1.6511180-03 9.500-03 6.000-01 9.47482D-03 5.600-01 9.47970-02 4.400-02 1.47566D-03 9.500-03 7.000-01 1.015500-01 6.0810 00 2.754010-02 4.400-02 1.81456D-03 7.600-01 1.015500-01 6.0810 00 2.75956D-02 4.400-02 1.81456D-03 7.600-01 1.031350-01 6.480 00 1.75823D-02 4.800-02 1.984677-03 7.600-01 1.031350-01 6.480 00 1.75823D-02 4.800-02 1.984677-03 7.600-01 1.00133150-01	4.100-02 1.356110-03 9.100-02 5.13677-03 6.000-01 8.622100-02 5.423910-03 8.0200-02 4.200-02 1.4418110-03 9.200-02 5.423910-03 6.200-01 9.4806570-02 5.4280 00 3.612210-02 4.200-02 1.4418110-02 5.801 00 3.011290-02 4.400-02 4.400-02 1.4418110-02 5.93370-03 6.800-01 9.41710-02 5.480 00 3.112210-02 4.400-02 1.454560-03 9.400-02 6.504830-03 6.800-01 9.41710-02 5.480 00 3.112210-02 4.400-02 1.61577850-03 9.500-03 5.800-03 7.600-01 9.417210-02 5.45010-02 5.45010-02 4.400-02 1.614180-03 7.000-01 1.015500-01 9.47010-02 5.259560-02 5.45010-02 5.45010-02 4.400-02 1.8146670-03 7.400-01 1.015500-01 6.880 00 1.919710-02 5.5000-02 4.400-02 1.8146670-03 7.400-01 1.0381730-01 6.880 00 1.758230-02 5.44010-02 4.400-02 1.846670-03 7.400-01 <td>4.000-02</td> <td>1.295300-03</td> <td>9.000-02</td> <td>5.604780-03</td> <td>5-800-01</td> <td>8.340110-02</td> <td>4.88D CO</td> <td>4.371870-02</td> <td></td> <td></td> <td></td>	4.000-02	1.295300-03	9.000-02	5.604780-03	5-800-01	8.340110-02	4.88D CO	4.371870-02			
#.200-02 1.41811U-03 9.200-02 5.4231D-03 6.400-01 9.46371D-02 5.480 00 3.63254D-02 #.400-02 1.4481279-02 5.9370D-03 6.400-01 9.463711D-02 5.480 00 3.61127D-02 #.400-02 1.4481279-03 9.400-01 9.45371D-02 5.480 00 3.01127D-02 #.400-02 1.4481279-03 9.400-01 9.45371D-02 5.480 00 3.01127D-02 #.500-02 1.641180-03 9.500-03 6.400-01 9.451820-02 5.480 00 2.75501D-02 #.500-02 1.67185D-03 9.600-01 1.051500-01 9.480 0 2.25550-02 #.600-02 1.87185D-03 7.000-01 1.033350-01 6.480 0 2.25550-02 #.600-02 1.81465D-03 7.000-01 1.033350-01 6.480 0 2.255340-02 #.600-02 1.81465D-03 7.000-01 1.031730-01 6.480 0 2.754710-02 #.600-02 1.81465D-03 7.000-01 1.031730-01 6.480 0 2.754710-02 #.600-02 1.81465D-03 <	#.200-02 1.4418110-03 9.200-02 5.42310-03 6.4200-01 9.463710-02 5.4800 00 3.612540-02 #.400-02 1.4418290-02 5.933100-03 6.400-01 9.41637110-02 5.6480 00 3.612510-02 #.400-02 1.4481290-03 9.5400-01 9.4163710-02 5.6480 00 3.01127002 #.400-02 1.4481290-03 6.400-01 9.418310-02 5.680 00 3.0112702 #.500-02 1.611180-03 9.500-03 6.156700-03 6.800-01 9.6131490-02 #.400-02 1.67785D-03 9.800-02 6.326590-03 7.400-01 1.0315500-01 6.480 00 2.514490-02 #.400-02 1.81460-03 7.400-01 1.0155500-01 6.480 00 2.514490-02 4.466650-02 #.400-02 1.81460-03 7.400-01 1.0155500-01 6.480 00 2.514490-02 4.466650-02 #.400-02 1.81460-03 7.400-01 1.0153500-01 6.480 00 1.514400-02 #.400-02 1.886470-03 1.000-01 1.0181350-01 6.480 00 1.758230-02<	4.100-02	1.356110-03	9.100-02	5.71367D-03	0-000-91	8.62210D-02	5.080 00	3.985280-02			
4.300-02 1.481290-03 5.37CD-02 5.49370D-03 6.400-01 9.163710-02 5.480 00 3.31129D-02 4.400-02 1.554565D-03 9.400-01 9.45311D-02 5.880 00 3.71931D-02 4.400-02 1.6517850-03 9.400-01 9.45311D-02 5.880 00 3.71931D-02 4.500-02 1.6517850-03 9.400-01 9.45300-01 9.46300-02 5.880 00 2.75910-02 4.500-02 1.6117850-03 9.5000-01 9.45200-01 9.41800-02 5.8800-02 5.313490-02 4.700-02 1.81466C-03 9.4000-01 1.015500-01 6.680 00 2.759560-02 4.700-02 1.81466C-03 9.4000-01 1.015500-01 6.680 00 2.759560-02 4.500-02 1.81466C-03 7.4000-01 1.015500-01 6.880 00 1.758230-02 4.500-02 1.84466C-03 7.4000-01 1.081730-01 6.880 00 1.758230-02 5.000-02 1.9554470-03 7.4000-01 1.081730-01 6.880 00 1.758230-02 5.0000-02 1.9554470-01	4.300-02 1.481290-03 5.3700-02 5.400-01 9.163710-02 5.480 00 3.311290-02 4.500-02 1.54565D-03 9.400-01 9.423110-02 5.8860 00 3.11290-02 4.500-02 1.651765D-03 9.400-01 9.453110-02 5.8860 00 2.754010-02 4.500-02 1.651700-03 9.400-01 9.45810-02 5.8860 00 2.754010-02 4.500-02 1.61785D-03 9.400-01 9.45800-01 9.4810-02 5.8860 00 2.75560-02 4.500-02 1.8846770-03 9.700-01 1.015500-01 6.480 02 2.055560-02 2.995560-02 4.800-02 1.8846770-03 9.900-02 6.611400-03 7.600-01 1.0155070-02 5.995570-02 2.9955570-02 5.000-02 1.8846770-03 9.900-02 1.8846770-03 7.600-01 1.0155070-01 6.880 00 1.758230-02 5.000-02 1.8846770-03 7.600-01 1.0191730-01 6.880 00 1.758230-02 5.000-02 1.9554470-03 7.4800-03 7.600-01 1.099330700 00 1.758230-	4-200-02	1.418110-03	9.200-02	5.823310-03	6.200-01	8.89667D-02	5.280 00	3.632540-02			
4.400-02 1.545650-03 9.400-02 6.044830-03 6.600-01 9.423110-02 5.680 00 3.01210-02 4.500-02 1.6611120-02 5.156700-03 6.800-01 9.674820-02 5.860 00 2.7549010-02 4.600-02 1.6611120-03 9.500-02 6.259290-03 7.000-01 9.015800-01 6.280 00 2.5154010-02 4.700-02 1.614560-03 9.700-02 6.382610-03 7.400-01 1.015500-01 6.280 00 2.255560-02 4.8000-02 1.814660-03 9.500-02 6.456550-03 7.400-01 1.0181730-01 6.480 00 1.915710-02 4.900-02 1.9955440-03 1.000-01 6.71400-03 7.400-01 1.0081730-01 6.880 00 1.758230-02 5.000-02 1.955440-03 1.000-01 6.728500-03 7.800-01 1.0381730-01 6.880 00 1.758230-02 5.001-02 1.955440-03 1.000-01 6.728500-03 7.800-01 1.0381730-01 6.880 00 1.758230-02 5.001-02 1.955440-03 1.000-01 6.728500-03 7.800-01 1.0381730-01 6.880 00 1.758230-02 5.001-02 1.95544000 00 1.778200000000000000000000000000000000000	4.400-02 1.54555D-03 9.4400-02 6.04483D-03 6.600-01 9.473110-02 5.4501 00 3.112210-02 4.500-02 1.611180-02 9.4500+02 6.800+01 9.61743D-02 5.4501 00 2.754010-02 4.500-02 1.611180-02 9.4500+02 6.800+01 9.617450+02 9.800+02 5.800+02 5.754010-02 4.500-02 1.6177450-03 9.800+02 6.325290-03 7.400-01 1.015500-01 6.725550+02 4.500-02 1.81460-03 9.800+02 6.611400-02 7.400-01 1.003350-01 6.880 00 1.919710-02 4.900-02 1.891460-03 7.400-01 1.003430-01 6.880 00 1.755230-02 5.000-02 1.9955470-03 7.400-01 1.031730-01 6.880 00 1.755230-02 5.000-02 1.9554470-03 7.800-01 1.0931730-01 6.880 00 1.755230-02 5.000-02 1.9554470-03 7.800-01 1.0931730-01 6.880 00 1.755230-02 5.000-02 1.9554470-03 7.800-01 1.0931730-01 0.5959470-02 1.4476 <	4.300-02	1.481290-03	5.3CD-02	5.93370D-03	6.40D-01	9.163710-02	5.480 00	3.311290-02	-		
4.500-02 1.611180-03 9.55700-03 6.800-01 9.614820-02 5.8840 00 2.754010-02 4.500-02 1.6774550-03 9.600-01 9.918800-02 6.28550-02 9.455650-02 4.600-02 1.6774550-03 9.600-01 9.918800-01 6.28560-02 9.455650-02 4.800-02 1.814660-03 9.600-02 6.382610-03 7.600-01 1.038350-01 6.480 00 2.95560-02 4.800-02 1.814660-03 9.800-02 6.41400-03 7.600-01 1.038350-01 6.480 00 1.9197110-02 4.900-02 1.814660-03 9.600-01 1.0381730-01 6.880 00 1.9197110-02 5.000-02 1.886470-03 1.0000-01 6.726850-03 7.600-01 1.0381730-01 6.880 00 1.758230-02 5.000-02 1.9558470-03 1.0000-01 6.726850-03 7.600-01 1.0604300-01 6.880 00 1.758230-02 5.000-02 1.9558470-03 1.0000-01 1.0381730-01 6.880 00 1.758230-02 5.000-02 1.9558470-03 1.0000-01 1.090430 00 <	4.500-02 1.6111E0-03 9.500-02 6.156700-03 6.800-01 9.674320-02 5.800 00 2.515490-02 4.600-02 1.677859-03 7.000-01 9.183500-01 6.280 00 2.515490-02 4.600-02 1.677859-03 7.000-01 9.183500-01 6.280 00 2.25550-02 4.600-02 1.844660-03 9.200-02 1.496650-03 7.400-01 1.033350-01 6.480 02 2.55560-02 4.600-02 1.844660-03 9.500-02 1.846650-03 7.400-01 1.031730-01 6.480 02 2.058250-02 4.900-02 1.884670-03 9.5000-02 6.611400-03 7.600-01 1.031730-01 6.880 00 1.758230-02 5.000-02 1.955440-03 1.0000-01 6.726850-03 7.6400-01 1.081730-01 6.880 00 1.758230-02 5.000-02 1.955440-03 1.0000-01 6.726850-03 7.6400-01 1.060430-02 0.5595470-02 5.000-02 1.955440-03 1.0000-01 6.16410930 00 1.7582300-01 0.5595470-02 5.0179200 1.6410930 00<	4-400-02	1-545650-03	9.400-02	6.044830-03	6.600-01	9.423110-02	5.680 00	3.019210-02			
4.60D-02 1.67785D-03 9.60D-02 6.26929D-03 7.00D-01 9.918800-02 6.08D 00 2.51349D-02 4.70D-02 1.74566D-03 9.70D-03 7.20D-01 1.015500-01 6.48D 00 2.25556D-02 4.60D-02 1.81466D-03 9.50D-02 6.611400-03 7.40D-01 1.015350-01 6.48D 00 2.997550-02 4.90D-02 1.88467D-03 9.90D-02 6.611400-03 7.60D-01 1.016730-01 6.86D 00 1.91971D-02 5.00D-02 1.95584D-03 1.00D-01 6.72685D-03 7.60D-01 1.016730-01 6.86D 00 1.91971D-02 5.00D-02 1.95584D-03 1.00D-01 6.72685D-03 7.60D-01 1.016730-01 6.86D 00 1.75823D-02 5.00D-02 1.95584D-03 1.00D-01 6.72685D-03 7.60D-01 1.016730-01 6.86D 00 1.75823D-02 5.00D-02 1.95584D-03 1.00D-01 6.72685D-03 7.60D-01 1.016730-01 6.86D 00 1.75823D-02 5.00D-02 1.95584D-03 1.00D-01 6.72685D-03 7.60D-01 1.016740-01 0.65959700-02 6.810 00 0.595947D-02 6.810 00 0.595947D-02 7.60D-02 1.95584D-03 1.00D-01 6.72685D-03 7.60D-01 1.016740 6.810 00 0.595947D-02 6.810 00 0.595947D-02 7.60D-02 1.955847D-02 7.60D-02 1.955847D-02 0.0000000000000000000000000000000000	4.600-02 1.67735D-C3 9.600-02 6.28250-03 7.000-01 9.918800-02 6.080 00 2.51349D-02 4.700-02 1.874566-03 9.600-02 6.38261D-03 7.200-01 1.01530350-01 6.480 00 2.955560-02 4.800-02 1.88467D-03 9.900-02 6.496650-03 7.400-01 1.0183730-01 6.480 00 2.096250-02 4.900-02 1.88467D-03 9.900-02 6.611400-03 7.400-01 1.0181730-01 6.860 00 1.91971D-02 5.000-02 1.95584D-03 1.000-01 6.726850-03 7.600-01 1.0181730-01 6.860 00 1.91971D-02 5.000-02 1.95584D-03 1.000-01 6.726850-03 7.600-01 1.0181730-01 6.860 00 1.758230-02 5.000-02 1.95584D-03 1.000-01 6.726850-03 7.600-01 1.0181730-01 6.860 00 1.7758230-02 5.000-02 1.95584D-03 1.000-01 6.726850-03 7.600-01 1.0181730-01 6.860 00 1.7758230-02 5.000-02 1.95584D-02 1.000-01 6.726850-03 7.600-01 0.017720400-01 0.01230570 90 1.64773540 CC 0.17720400-01 0.01200-01 0.01230570 90	4-500-02	1.611180-03	9.5CD-02	6.156700-03	6.800-01	9.674820-02	5.840 00	2.754010-02			
4.705-C2 1.775560-C3 9.7CU-C2 6.382610-C3 7.200-01 1.015500-01 6.280 00 2.255560-02 4.800-C2 1.8814605-03 9.800-02 6.46160550-03 7.4000-01 1.0081350-01 6.680 00 1.919710-02 4.900-C2 1.8814605-03 9.900-02 6.611400-03 7.4000-01 1.0081750-01 6.480 00 1.758230-02 5.000-02 1.955840-03 1.0000-01 6.726850-03 7.800-01 1.081730-01 6.880 00 1.758230-02 5.3779210 00 1.000000 1.000000 1.000000 0.0000000 0.5595470-02 5.3779210 00 10000000000000000000000000000000	4.705-C2 1.74560-C3 9.700-C2 5.302610-C3 7.200-01 1.0015500-01 6.2810 0C 2.255560-02 4.800-C02 1.881460C-03 9.800-02 5.4511400-03 7.400-01 1.0038350-01 6.4580 00 1.9919710-02 5.000-02 1.881460C-03 7.400-01 1.008430-01 6.4580 00 1.9919710-02 5.000-02 1.891400-03 7.400-01 1.008430-01 6.4580 00 1.9919710-02 5.000-02 1.891400-03 7.400-01 1.0081730-01 6.4580 00 1.919710-02 5.000-02 1.955940-03 7.800-01 1.0081730-01 6.880 00 1.755230-02 5.000-02 1.955950-03 7.800-01 1.081730-01 6.880 00 1.755230-02 5.000-02 1.975850-03 7.800-01 1.091030 00 0.5595470-01 0.775230-02 8.000-01 1.0610930 00 1.6410930 00 0.5959470-01 0.7720400-01 9.1.75540 CC 0.1720400-01 0.7720400-01 0.61230570 0.61230570	4.600-02	1.67785D-C3	9.600-02	6.269290-03	7.0000-01	9.918800-02	6. C8D 00	2.513490-02			
4.800-02 1.80146.0C-03 9.800-02 6.400 665-03 7.400-01 1.038350-01 6.480 00 1.91971D-02 4.900-02 1.88467D-03 9.900-02 6.611400-03 7.600-01 1.006435D-01 6.880 00 1.91971D-02 5.000-02 1.88467D-03 1.8000-01 6.7865D-03 7.800-01 1.006435D-01 6.880 00 1.758239D-02 5.000-02 1.95544D-03 1.000-01 6.77685D-03 7.800-01 1.018173D-01 6.880 00 1.758239D-02 5.000-02 1.95544D-03 1.000-01 6.77685D-03 7.800-01 1.019173D-01 6.880 00 0.1.758239D-02 5.000-02 1.95544D-03 1.000-01 6.7100-03 7.800-01 0.00 0.5595947D-02 MIXED EFFECTIVE RANGE D.01 0.7595947D-01 MIXED EFFECTIVE RANGE	4.800-02 1.8146CD-03 9.800-02 6.495655D-03 7.400-01 1.03835D-01 6.480 0C 2.00825D-02 4.900-02 1.88467D-03 9.900-02 6.611400-03 7.400-01 1.00143D-01 6.880 00 1.91971D-02 5.000-02 1.95544D-03 1.000-01 6.72685D-03 7.800-01 1.00173D-01 6.880 00 1.91971D-02 5.000-02 1.95544D-03 1.000-01 6.72685D-03 7.800-01 1.08173D-01 6.880 00 1.75523D-02 5.001-02 1.95544D-03 1.000-01 6.72685D-03 7.800-01 1.08173D-01 6.880 00 1.75523D-02 5.001-02 1.95544D-02 0.000-01 6.7168100 0 0.55547D-02 0.55547D-02 6.810 0.0 1.5523D-02 0.600-01 1.641093D 00 0.55547D-02 0.5404F 8.010 0.0 1.641093D 00 0.55547D-61 0.6100 0.55547D-61 0.61075 0.555477D-61 9.010 0.772040D-61 0.61000	4.700-02	1.745660-03	9.700-02	6.382610-03	7.200-01	1.015500-01	6.28D 00	2.255560-02			
4.900-02 1.884670-03 9.900-02 6.611400-03 7.600-01 1.060430-01 6.680 00 1.919710-02 5.000-02 1.9558470-03 1.000-01 6.726850-03 7.8600-01 1.081730-01 6.880 00 1.758230-02 5.000-02 1.9558470-03 1.000-01 6.726850-03 7.8600-01 1.081730-01 6.880 00 1.758230-02 5.3779210 00 MIXED EFFECTIVE RANGE DEUTENDN EFFECTIVE RANGE APPROX. SHAPE PARAMETER SFC0D SHAPE PARAMETER	4.900-02 1.884670-03 9.900-02 6.611400-03 7.600-01 1.060430-01 6.680 00 1.91971D-02 5.000-02 1.95584D-03 1.000-01 6.726850-03 7.800-01 1.081730-01 6.880 00 1.758230-02 5.000-02 1.95584P-03 1.000-01 6.726850-03 7.800-01 1.081730-01 6.860 00 1.758230-02 5.3779210 00 1.6410930 00 0.5959470-01 6.5959470-01 0.5959470-01 1.6473540 CC 0.1720400-01 0.1230570 90	4.800-02	1.814600-03	9.800-02	6.496650-03	7.400-01	1.038350-01	6.48D 0C	2.098250-02			
5.000-02 1.955840-03 1.0000-01 6.726850-03 7.800-01 1.081730-01 6.880 00 1.758230-02 Scattering Length Effective Range 0.5959470-01 5.3779210 00 1.6410930 00 0.5959470-01 Mixed Effective Range Deutendin Effective Range Approx. Shape Parameter Sfcund Shape Parameter	5.000-02 1.955840-03 1.000-01 6.726850-03 7.800-01 1.081730-01 6.880 00 1.758230-02 SCATTERING LENGTH EFFECTIVE RANGE SHAPE PARAMETER 5.377921D 00 1.45410930 00 0.595947D-01 MIXED EFFECTIVE RANGE DEUTENON EFFECTIVE RANGE APPRUX. SHAPE PARAMETER SFCUND SHAPE PARAMETER 1.473540 CC 0.1230570 90	4.900-02	1.884670-03	9.900-02	6.611400-03	7.600-01	1.060430-01	6.68D 00	1.91971D-02			
SCATTERING LENGTH EFFECTIVE RANGE SHAPE PARAMETER 5.377921D 00 1.6410930 00 0.595947D-C1 Mixed Effective Range Deutendn Effective Range Approx. Shape Parameter SFCOND SHAPE PARAMETER	SCATTERING LENGTH EFFECTIVE RANGE SHAPE PARAMETER 5.377921D 00 1.6410930 00 0.595947D-C1 Mixed Effective Range Approx. Shape Parameter SFCOND SHAPE PARAMETER 1.6773540 CC 0.123057D 90	5.000-02	1-95584D-03	1.000-01	6.726850-03	7.800-01	1.081730-01	6.88D 00	1.758230-02			
SCATTERING LENGTH EFFECTIVE RANGE SHAPE PARAMETER 5.377921D 00 1.641093D 00 0.595947D-C1 Mixed Effective Range Approx. Shape Parameter Sfcond Shape Parameter	SCATTERING LENGTH EFFECTIVE RANGE SHAPE PARAMETER 5.377921D 00 1.641093D 00 0.595947D-C1 Mixed Effective Range Approx, Shape Pakameter SFCUND SHAPE PARAMETER 1.477354D CC 0.123057D 90				a state -							
5.377921D 00 1.641093D 00 0.595947D-C1 MIXED EFFECTIVE RANGE DEUTENDN EFFECTIVE RANGE APPROX. SHAPE PANAMETER SFCOND SHAPE PARAMETER	5.377921D 00 1.641093D 00 0.595947D-C1 Mixed Effective Range Deutendn Effective Range Approx. Shape Parameter SFCUND SHAPE Parameter 1.677554D CC 0.123057D 90			SCATTERING	LENGTH	EFI	ECTIVE RANG		SHAPE PAR	AMETER		
MIXED EFFECTIVE RANGE DEUTENON EFFECTIVE RANGE APPROX. SHAPE PARAMETER SFCOND SHAPE PARAMETER	MIXED EFFECTIVE RANGE DEUTERON EFFECTIVE RANGE APPROX. SHAPE PARAMETER SECOND SHAPE PARAMETER 1.6773540 CC 0.1230570 90			5.37792	21D 00		1.641093D 00		0.59594	70-C1		
MIXED EFFECTIVE RANGE DEUTERON EFFECTIVE RANGE APPROX. SHAPE PARAMETER SECOND SHAPE PARAMETER	MIXED EFFECTIVE RANGE DEUTENDN EFFECTIVE RANGE APPROX. SHAPE PARAMETER SFCOND STAPE PARAMETEN 1.42733540 CC 1.7218650 CC 0.7720400-C1 0.1230570 90					•					and the second	
	1.6773540 CC 1.7218850 CC 0.7720400-01 0.12318850 CC	MIXED	EFFECTIVE R	ANGE DE	UTERON EFFE	CTIVE RAN	SE APPRUX	. SHAPE P	ARAME TER	SECCIND	HAPE PARAMETE	æ

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