

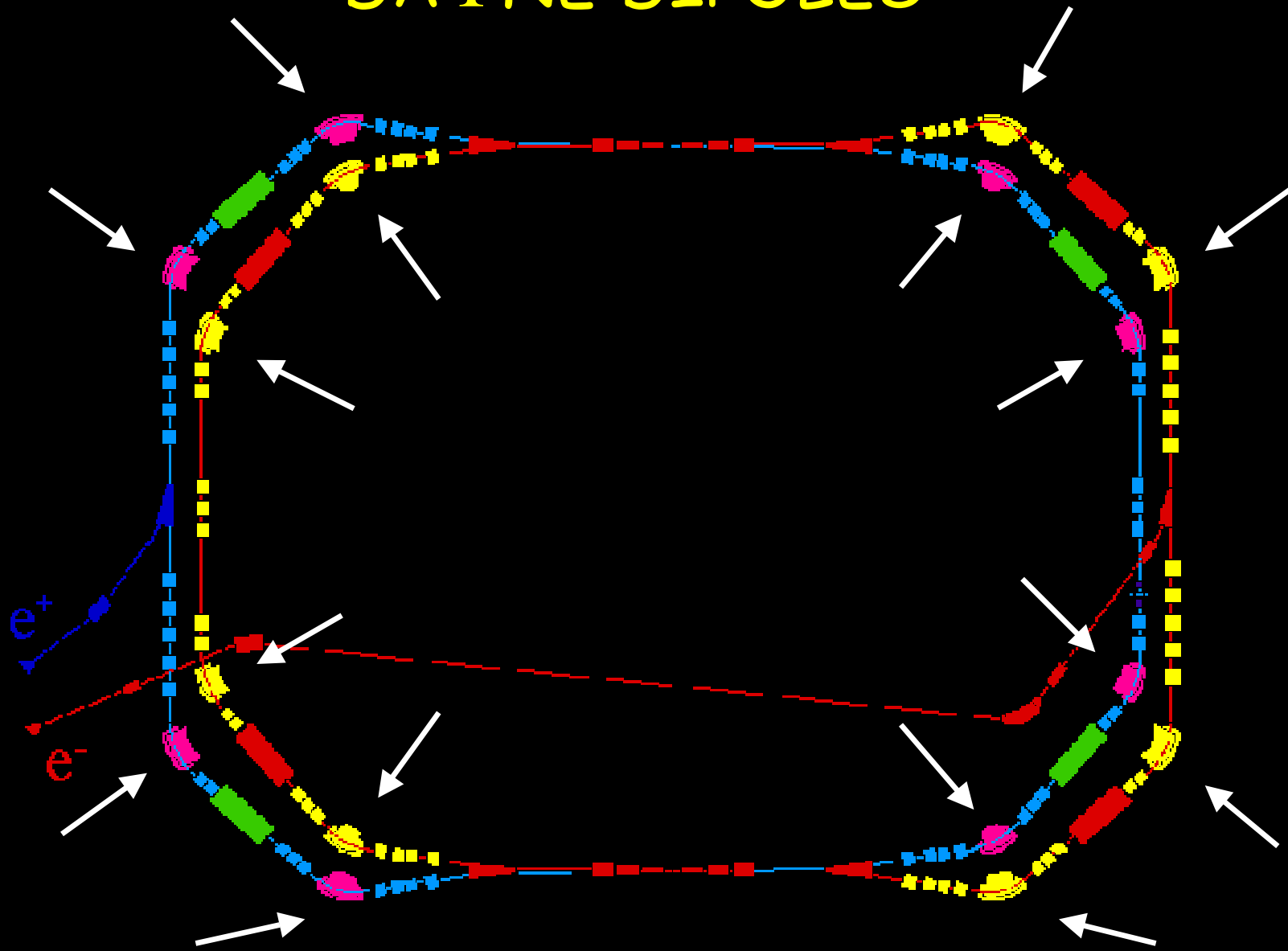


- DAΦNE UPGRADE -

PRELIMINARY FEASIBILITY STUDY ON
1.1 - 2.4 T RAMPING DIPOLES
FOR DAFNE2

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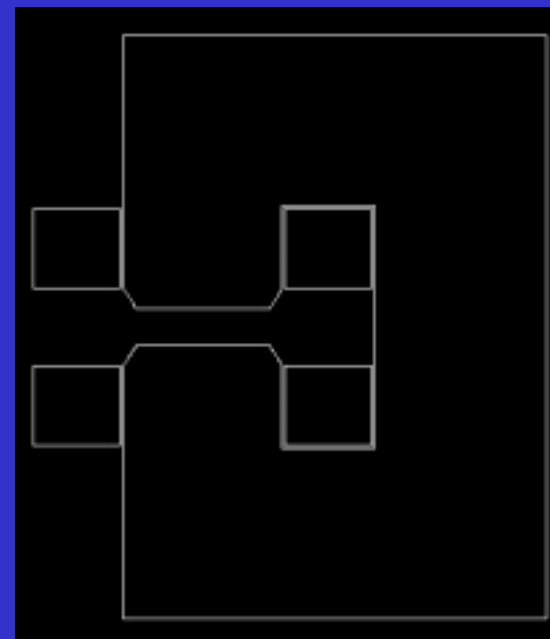
DAΦNE DIPOLES



DAΦNE DIPOLES:

- 8 C-shape bending magnets in each ring,
4 sector like + 4 parallel end

| | |
|-------------------|-----------------------|
| e^+/e^- Energy | 510 MeV |
| $B\rho$ | 1.7 T m |
| Nominal Field | 1.214 T |
| Bending Radius | 1.400 m |
| Nominal Current | 262.8 A |
| Current Density | 2.5 A/mm ² |
| Magnet Gap | 75 mm |
| Good Field Region | ± 30 mm |





FROM DAΦNE TO DAFNE2

NEW DIPOLES REQUIREMENTS AND CONSTRAINTS

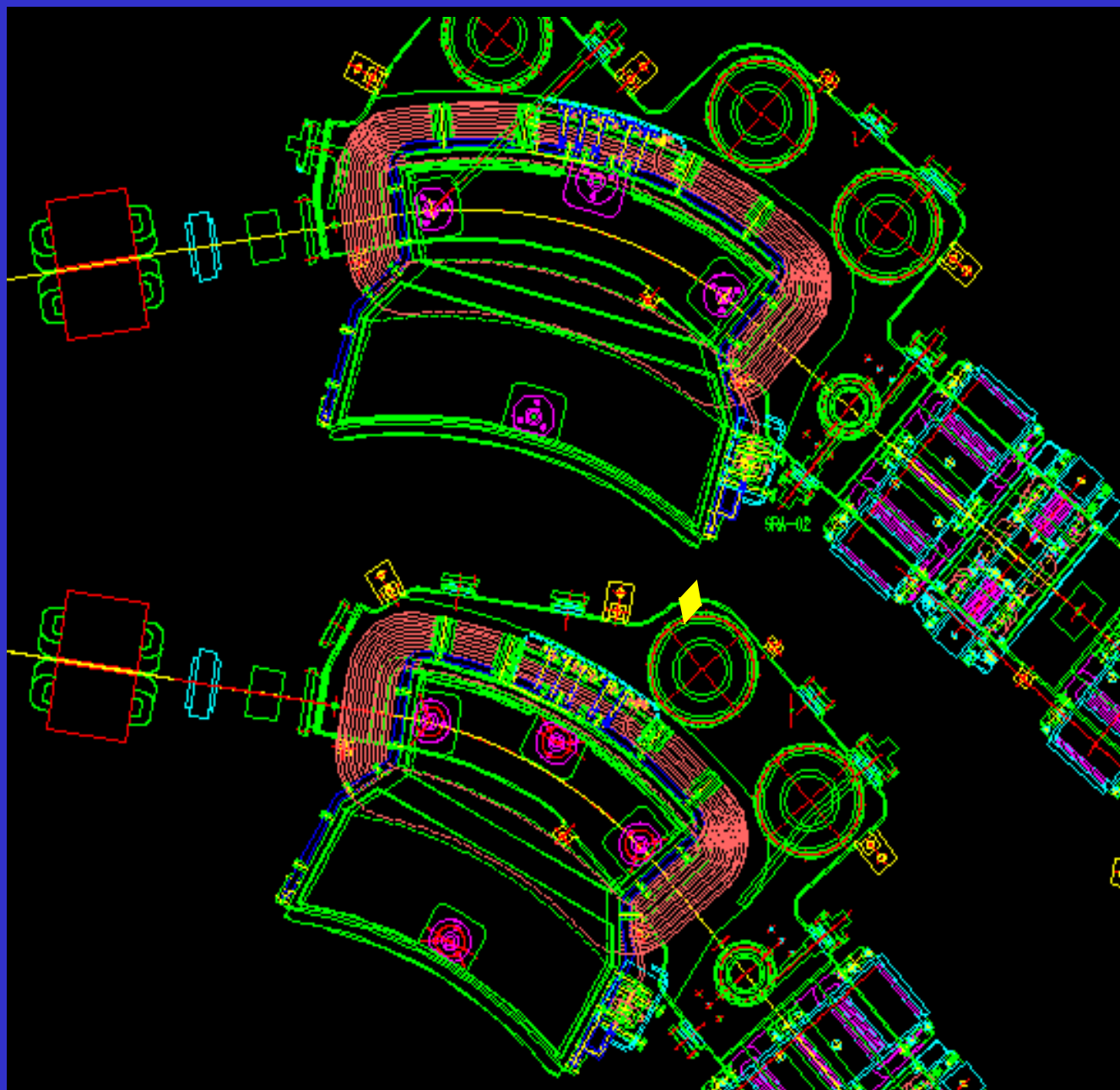
- Energy increase to 1.1 GeV
 - Larger fields, up to the saturation for iron magnet
- Ramping magnets from 0.51 to 1.1 GeV



FROM DAΦNE TO DAFNE2

NEW DIPOLES REQUIREMENTS AND CONSTRAINTS

- Same DaΦne vacuum chamber
 - Magnet gap height ≥ 70 mm
 - Same bending angle
- Same DaΦne layout
 - Constraints in the dimension





NEW DIPOLES DESIGN

In order to achieve the field requirement, given the machine layout, it is possible to:

LOWER THE MAGNET GAP

It is possible to reduce the magnet gap from 75 mm to 70 mm, removing the vacuum chamber thermal insulation

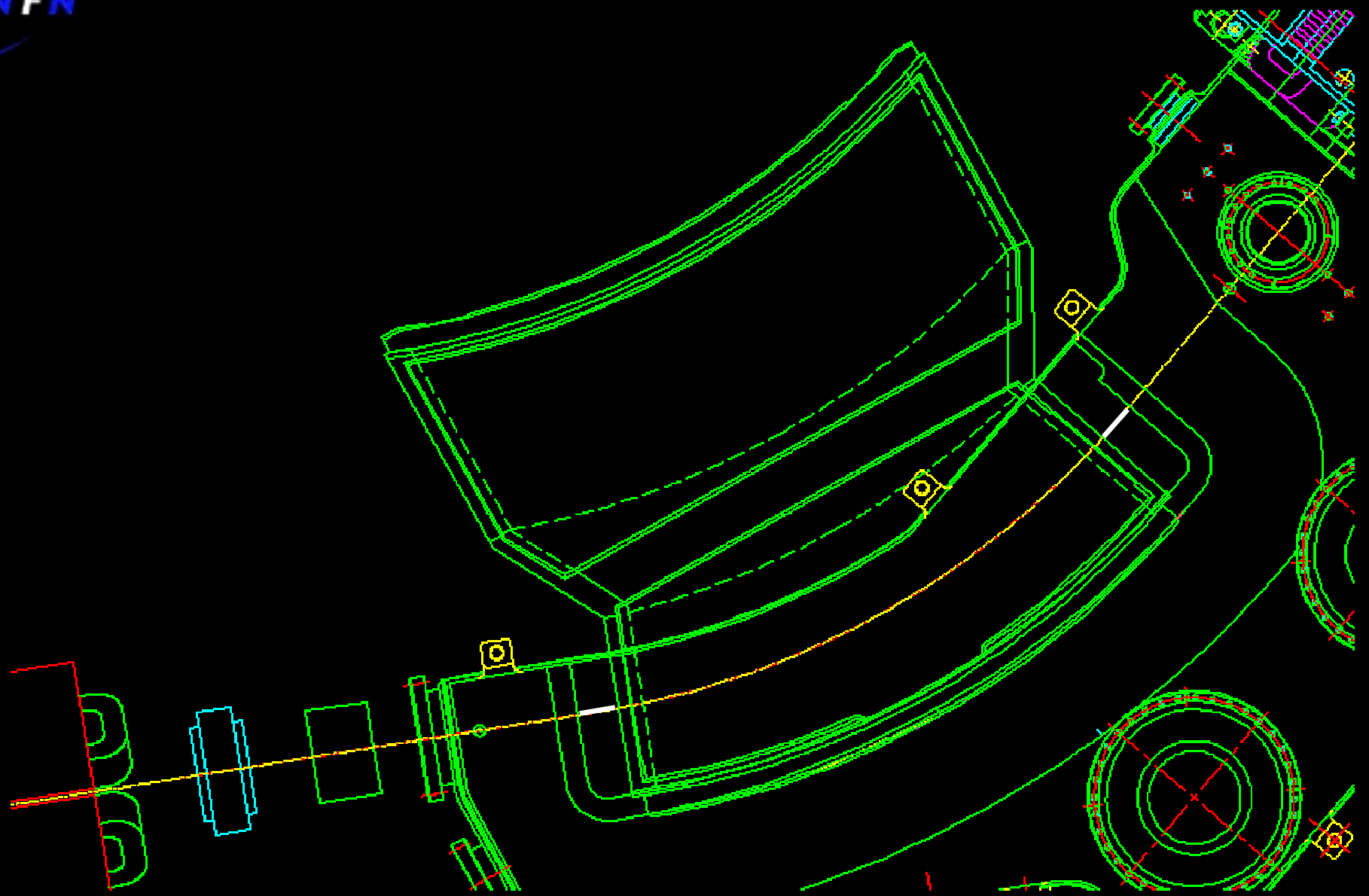


NEW DIPOLES DESIGN

In order to achieve the field requirement, given the machine layout, it is possible to:

INCREASE THE BENDING RADIUS

With the DaΦne vacuum chamber it is possible to increase the bending radius from 1.4 m to about 1.53 m, but it involves mechanical complications in the installation.





NEW DIPOLES DESIGN

Also, we should consider the possibility to:

- reduce the good field region
- increase the dipole iron yoke
- accept larger stray fields



NEW DIPOLES DESIGN

Field vs Beam Energy
relative to 1.53 m bending radius

| E (GeV) | B (T) |
|---------|-------|
| 0.510 | 1.11 |
| 1.000 | 2.18 |
| 1.100 | 2.40 |
| 1.150 | 2.50 |
| 1.200 | 2.61 |



REQUIREMENTS TABLE

| | |
|---------------------|----------------|
| • BEAM ENERGY | 0.51 - 1.1 GeV |
| • $B\rho$ | 1.7 - 3.7 T m |
| • MAGNETIC FIELD: | 1.1 - 2.4 T |
| • MAGNET GAP | 70 mm |
| • BENDING RADIUS | 1530 mm |
| • GOOD FIELD REGION | ± 20 mm |



WE HAVE TRIED TO SOLVE THE PROBLEM IN
TWO DIFFERENT WAYS ...

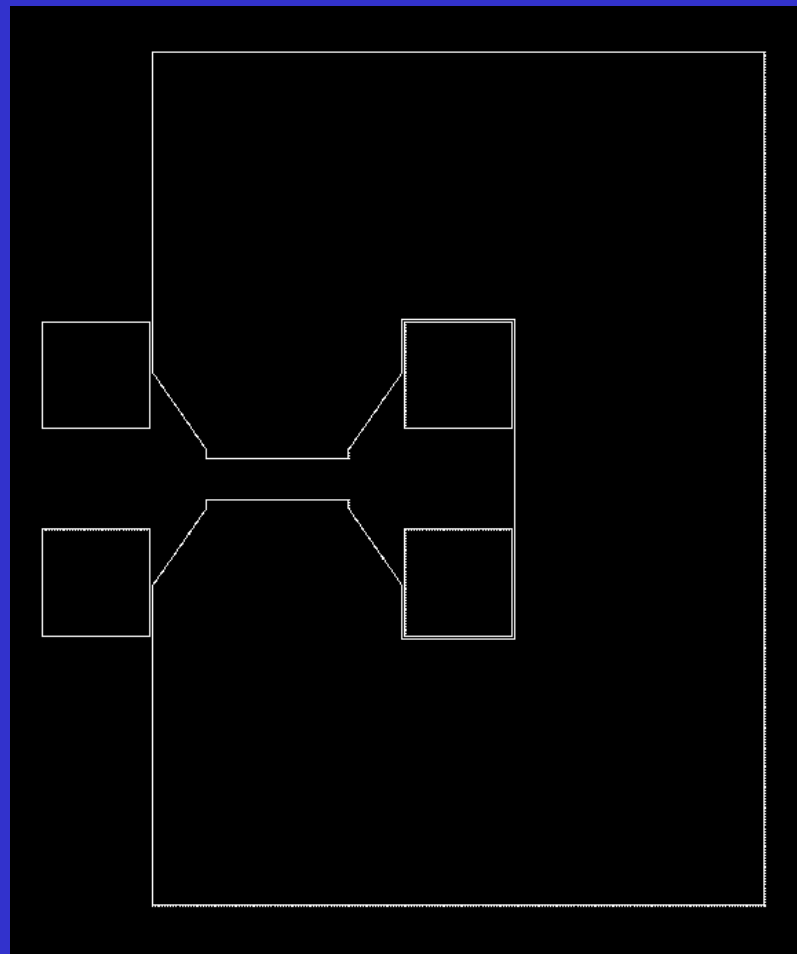
FIRST SOLUTION: CONVENTIONAL IRON MAGNETS

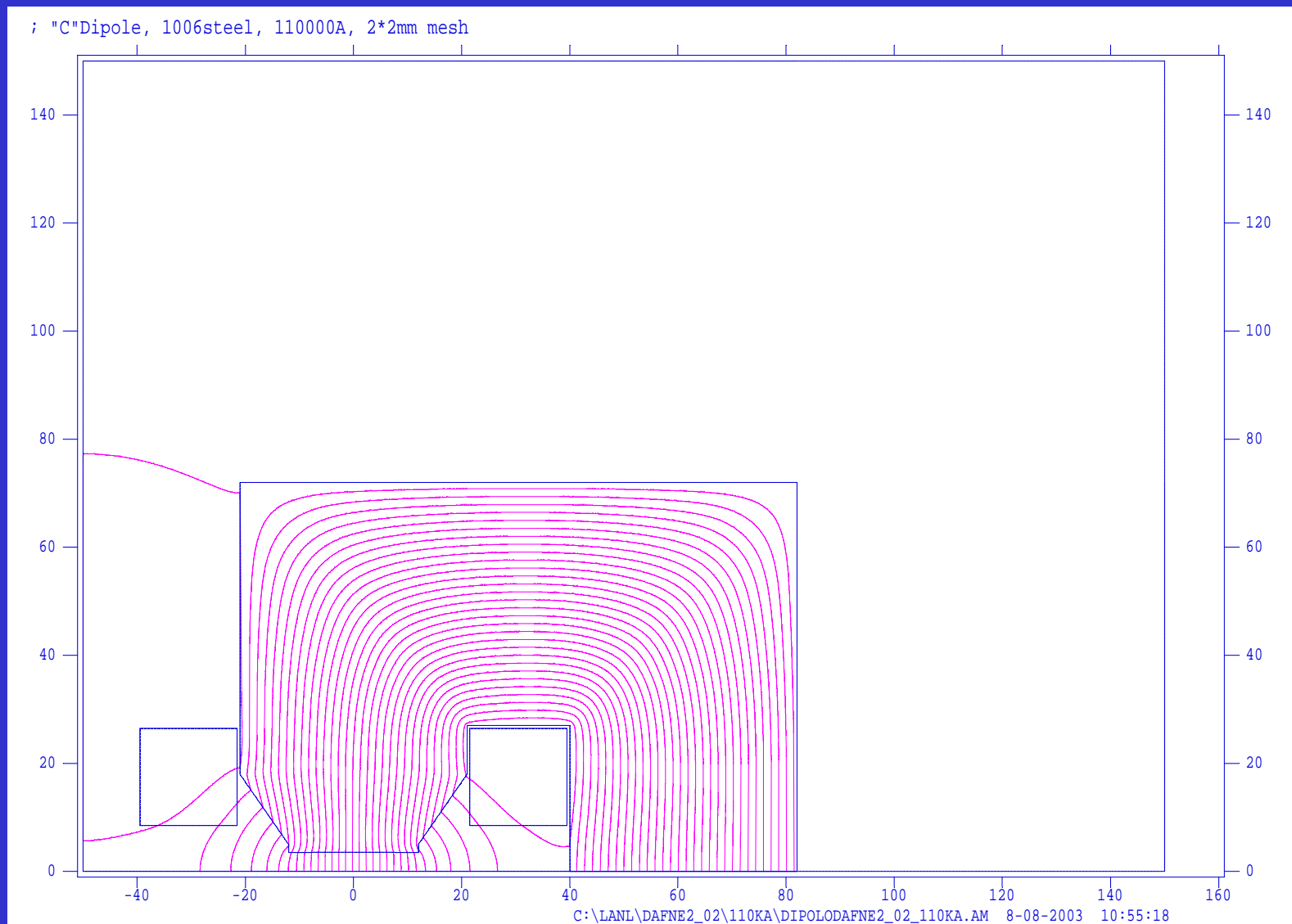
We ran a simulation with
POISSON 2D FEM code.

The material considered is the
1006 iron in all the yoke.

The current ranges from **31.5** to
150 kA*turns

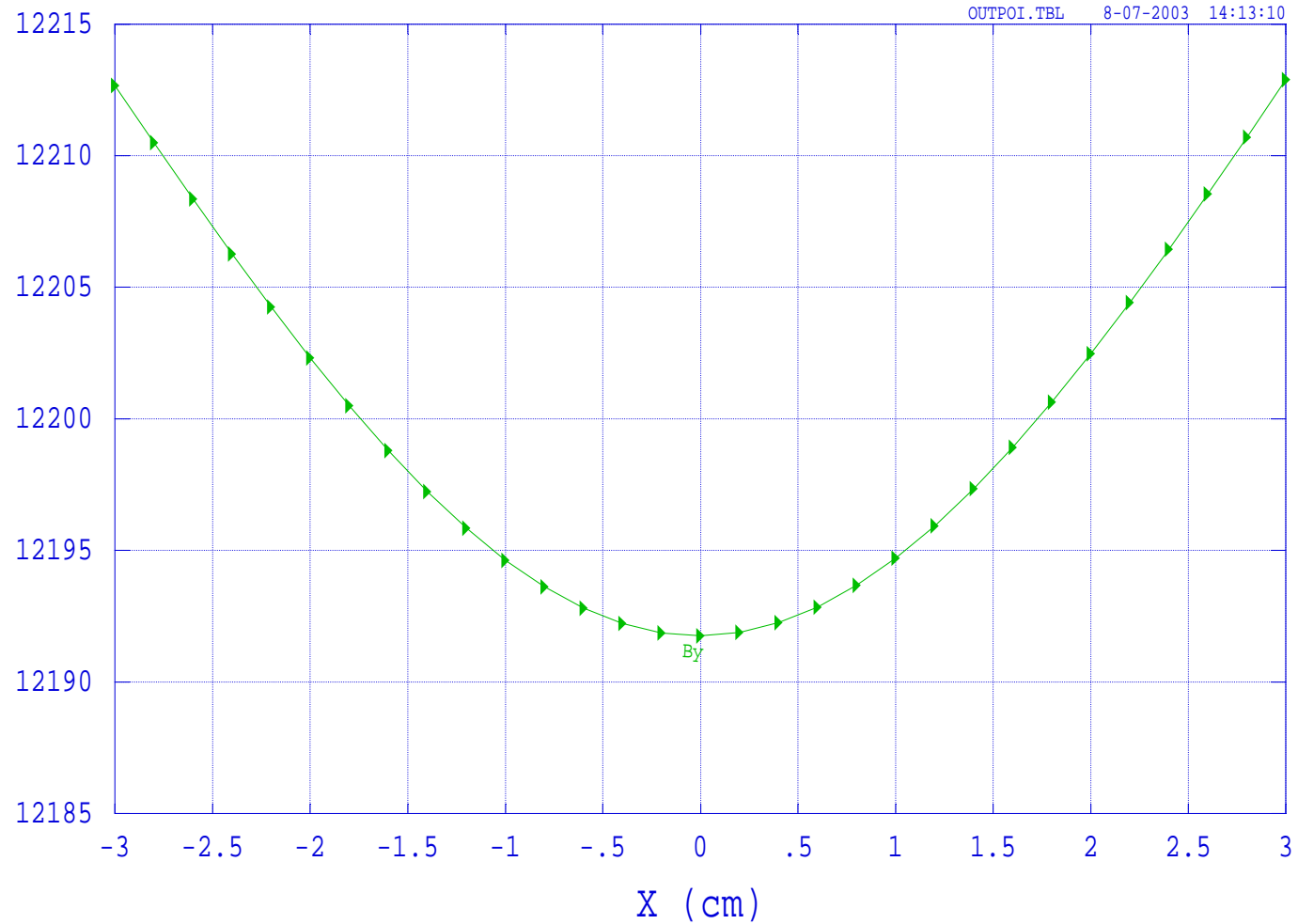
With 32400 mm² cross-section
coils and a filling factor of
0.55, the current density in
the coil ranges from **1.8** to
8.4 A/mm²





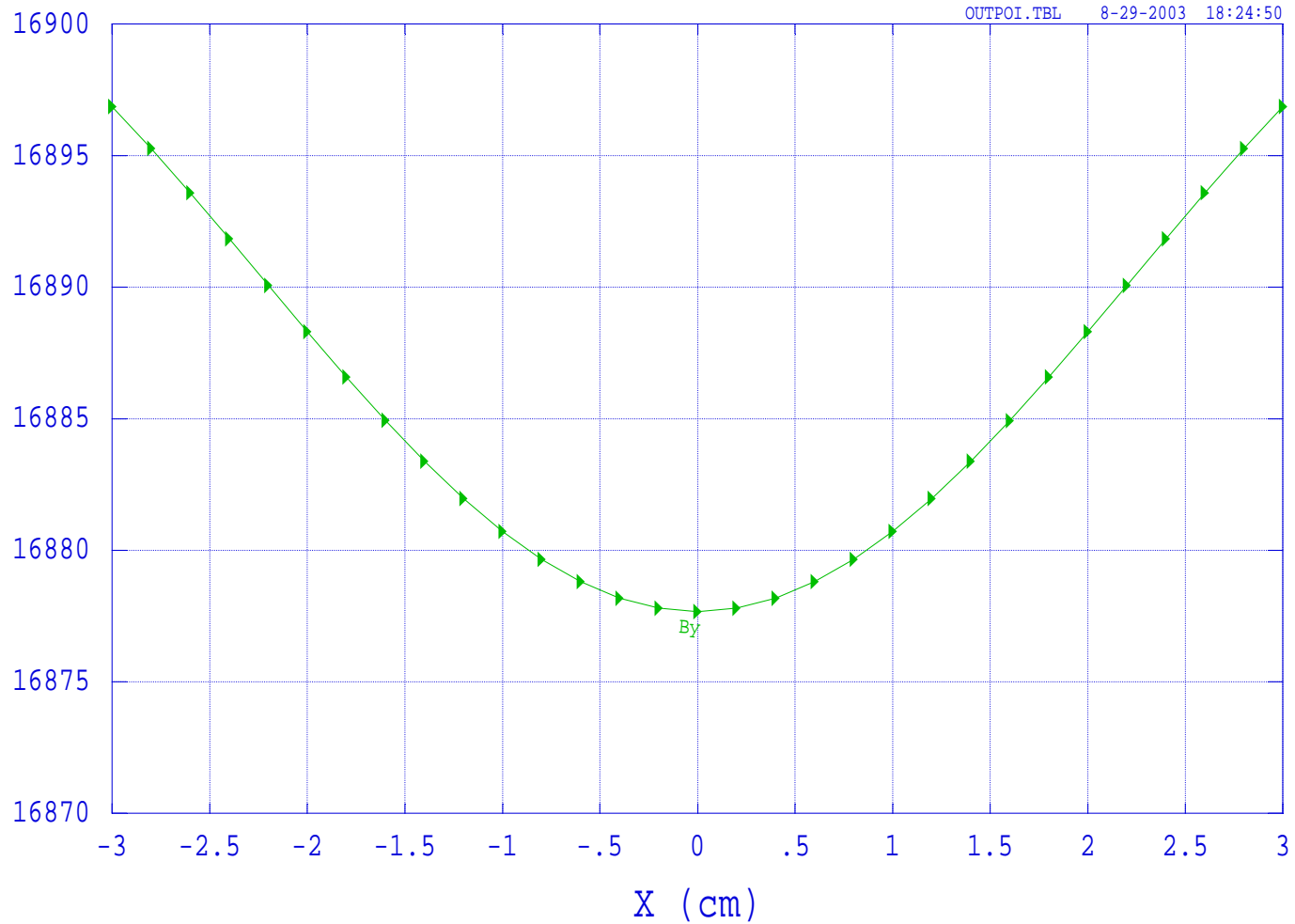


Magnetic field from Poisson run on file DIPOLODAFNE2_02_35KA.AM
Problem title line 1: ; "C"Dipole, 1006steel, 35000A, 2*2mm mesh



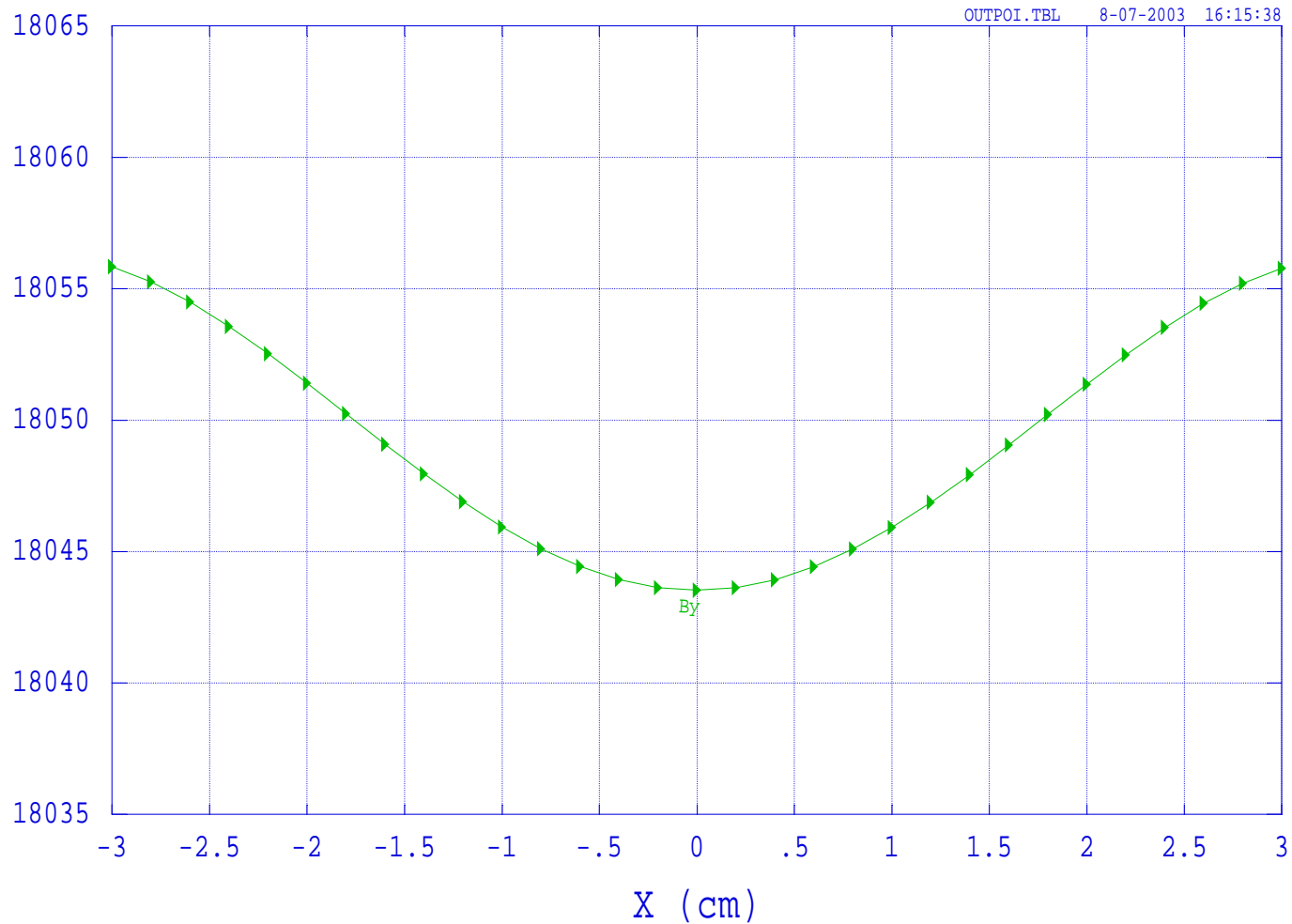


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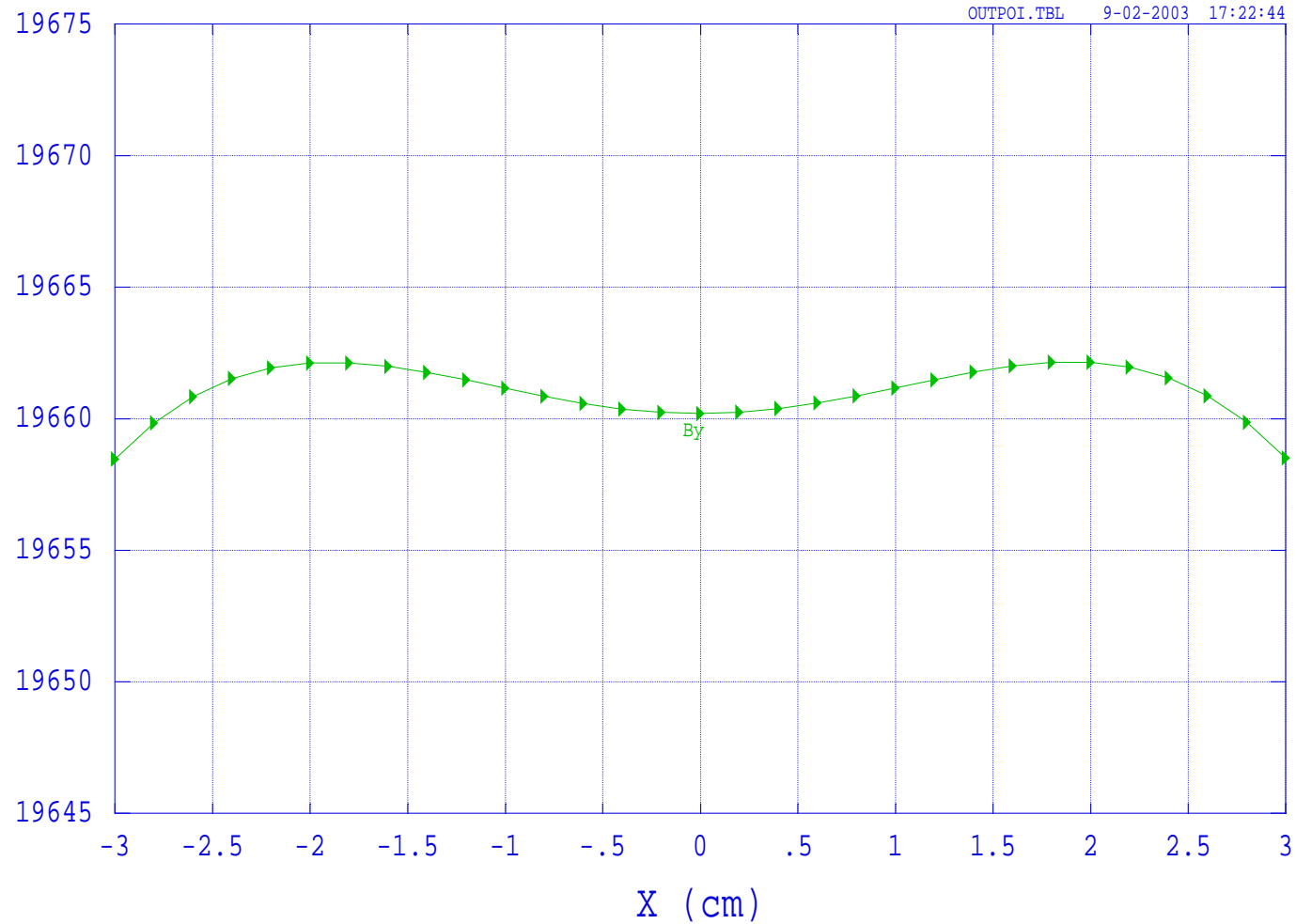


Magnetic field from Poisson run on file DIPOLODAFNE2_02_55KA.AM
Problem title line 1: ; "C"Dipole, 1006steel, 55000A, 2*2mm mesh



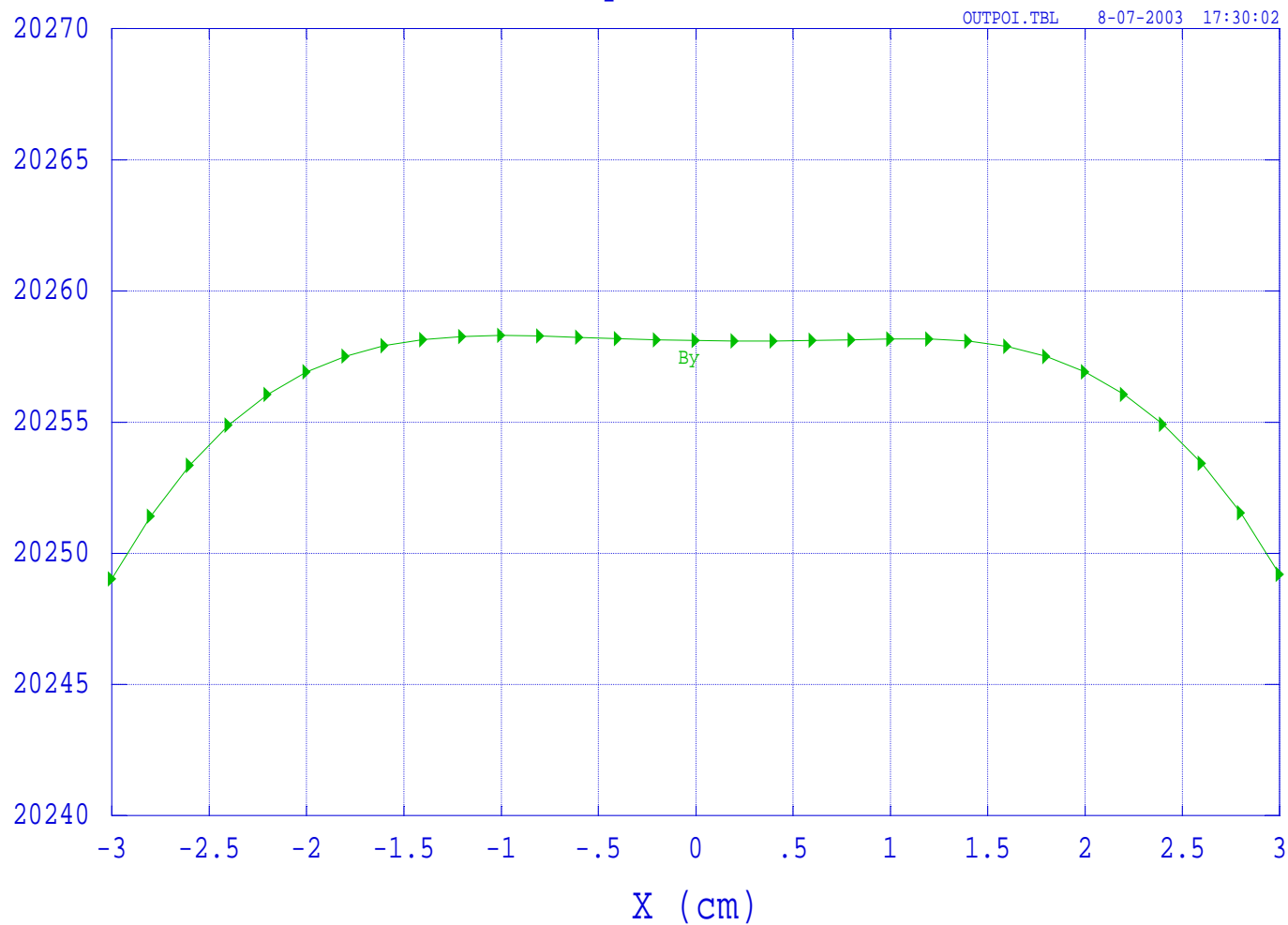


Magnetic field from Poisson run on file DIPOLODAFNE2_02_65KA.AM
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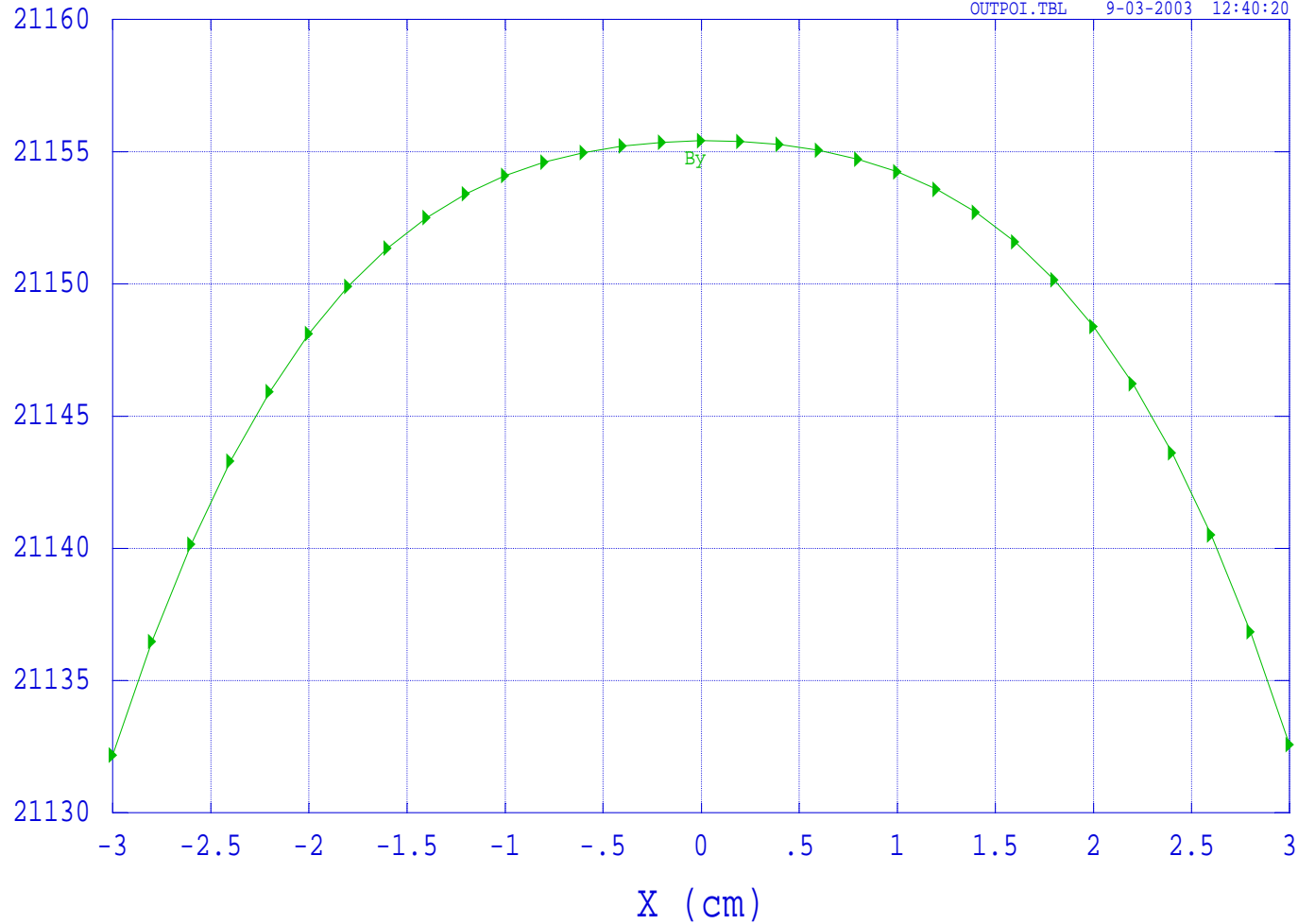
Magnetic field from Poisson run on file DIPOLODAFNE2_02_70KA.AM
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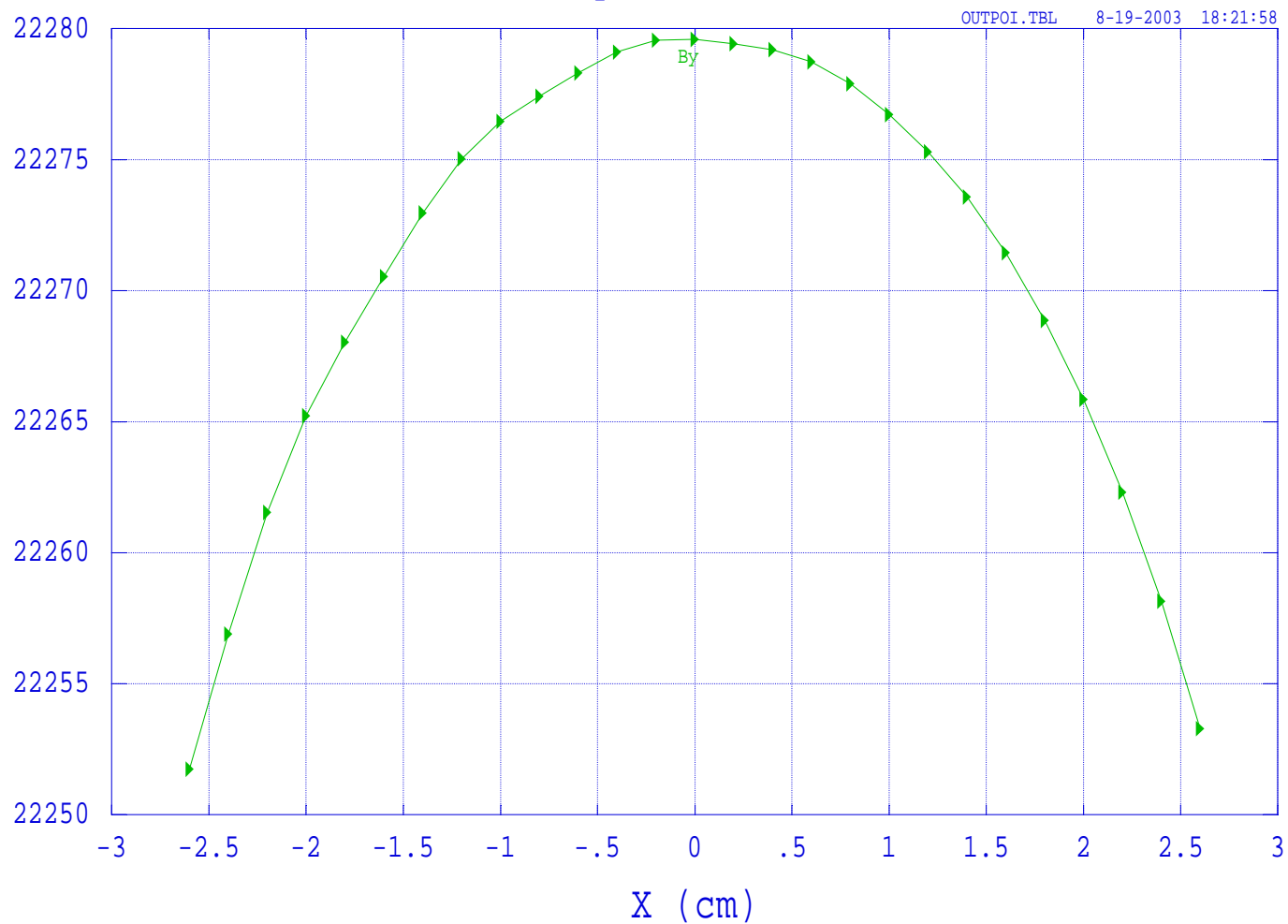


Magnetic field from Poisson run on file DIPOLODAFNE2_02_80KA.AM
Problem title line 1: ; "C"Dipole, 1006steel, 80000A, 2*2mm mesh

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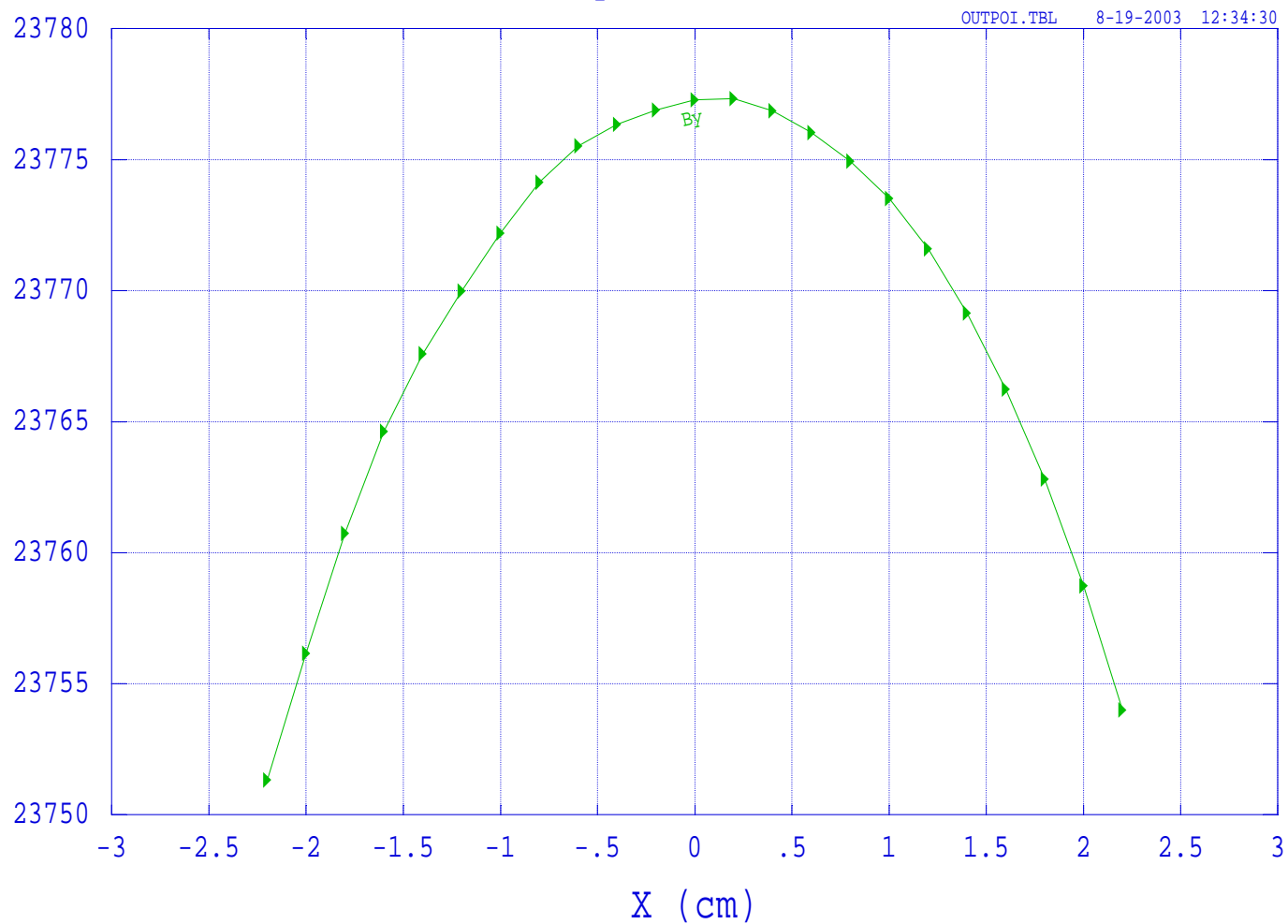


Magnetic field from Poisson run on file DIPOLODAFNE2_02_100KA.AM
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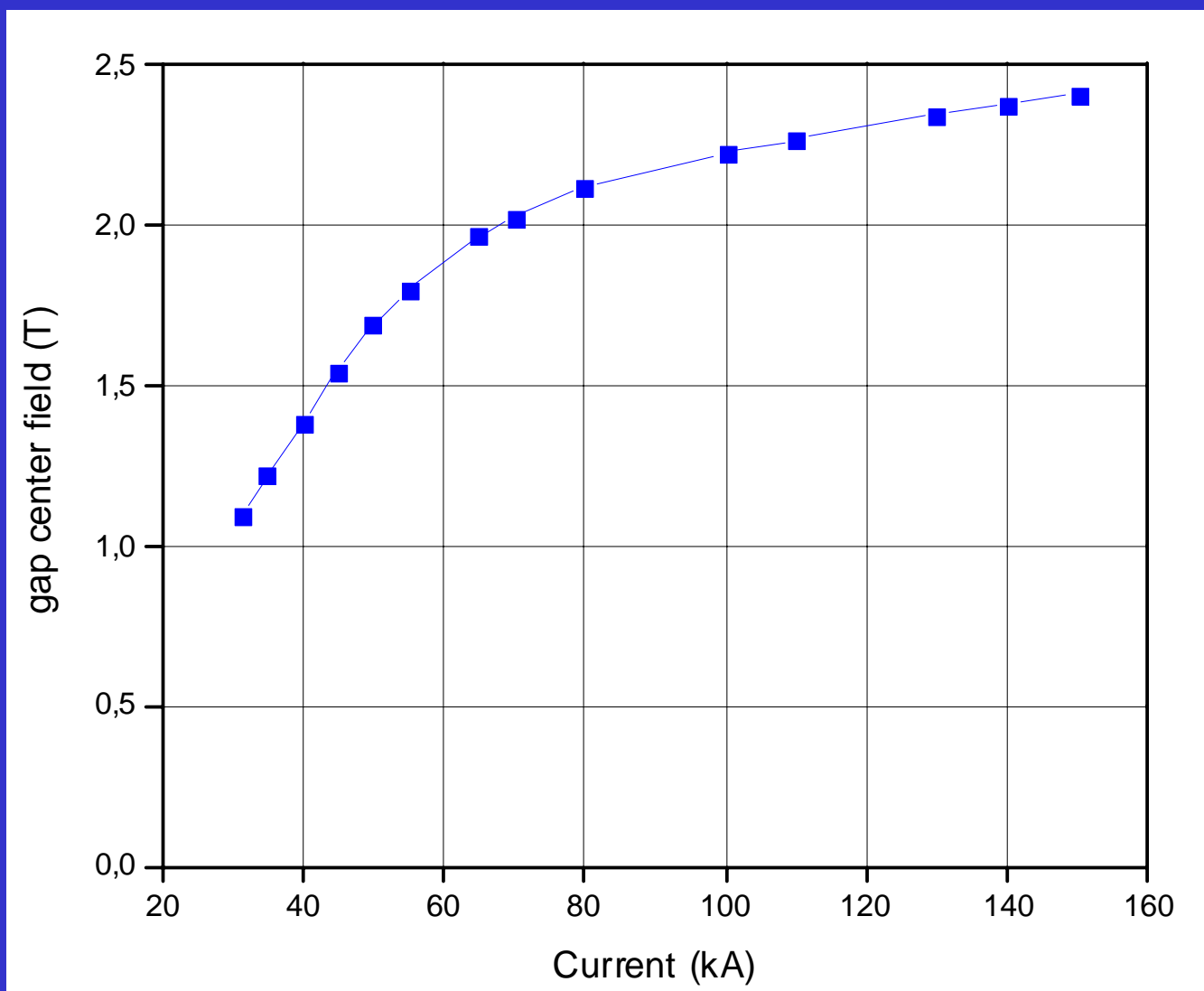


Magnetic field from Poisson run on file DIPOLODAFNE2_02_140KA.AM
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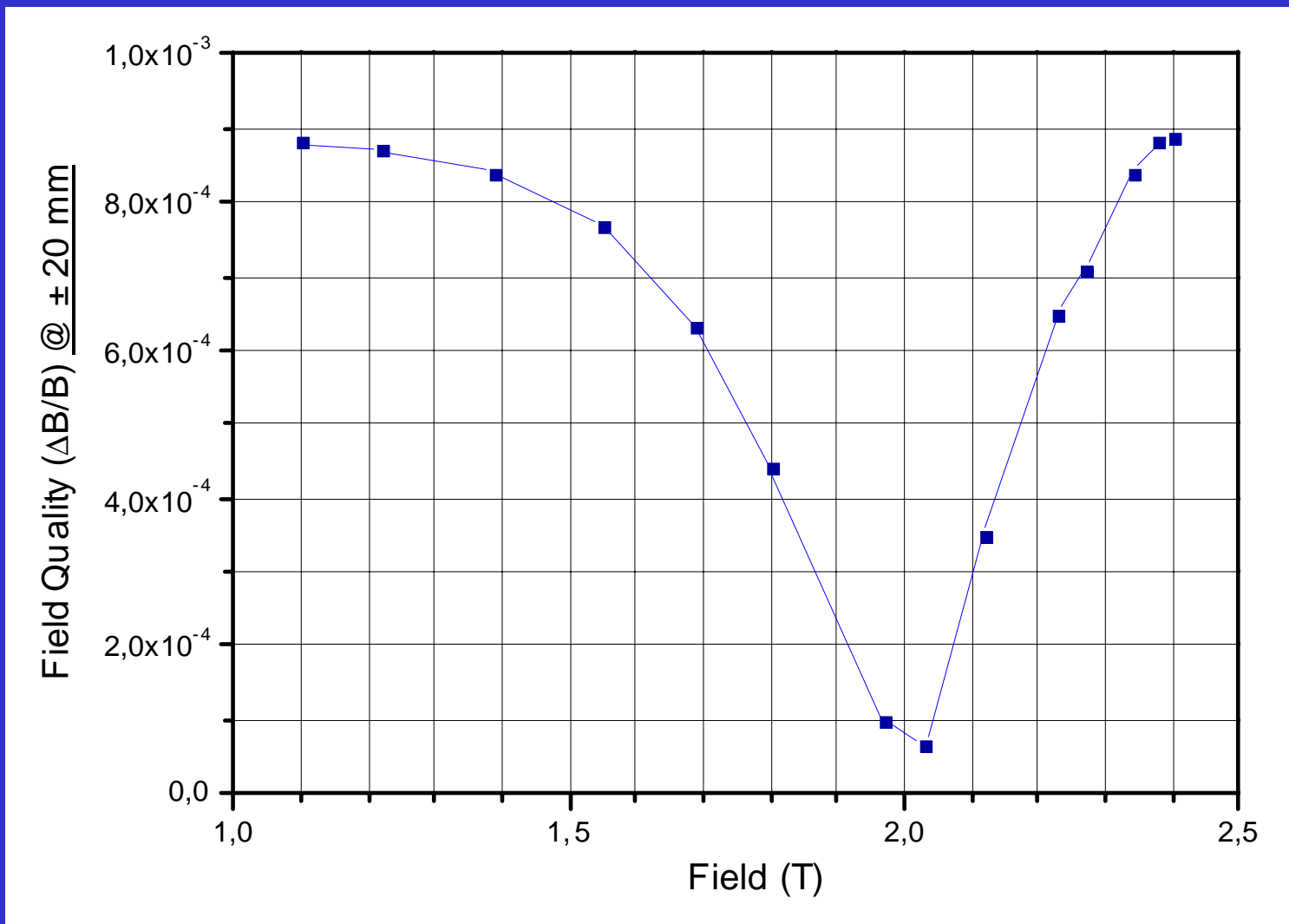


FIELD vs CURRENT IN THE GAP CENTER





FIELD QUALITY IN THE GOOD FIELD REGION





SIMULATION RESULTS

($B = 1.1 \div 2.4 \text{ T}$, $GFR = \pm 20 \text{ mm}$)

- CURRENT DENSITY = $1.8 \div 8.4 \text{ A/mm}^2$
- FIELD QUALITY ($\Delta B/B$) = $9 \cdot 10^{-4}$ @ 1.1 & 2.4 T
- STRAY FIELDS = 500 G @ 1 m, 2.4 T

CONCLUSIONS

about the first solution - iron dipole

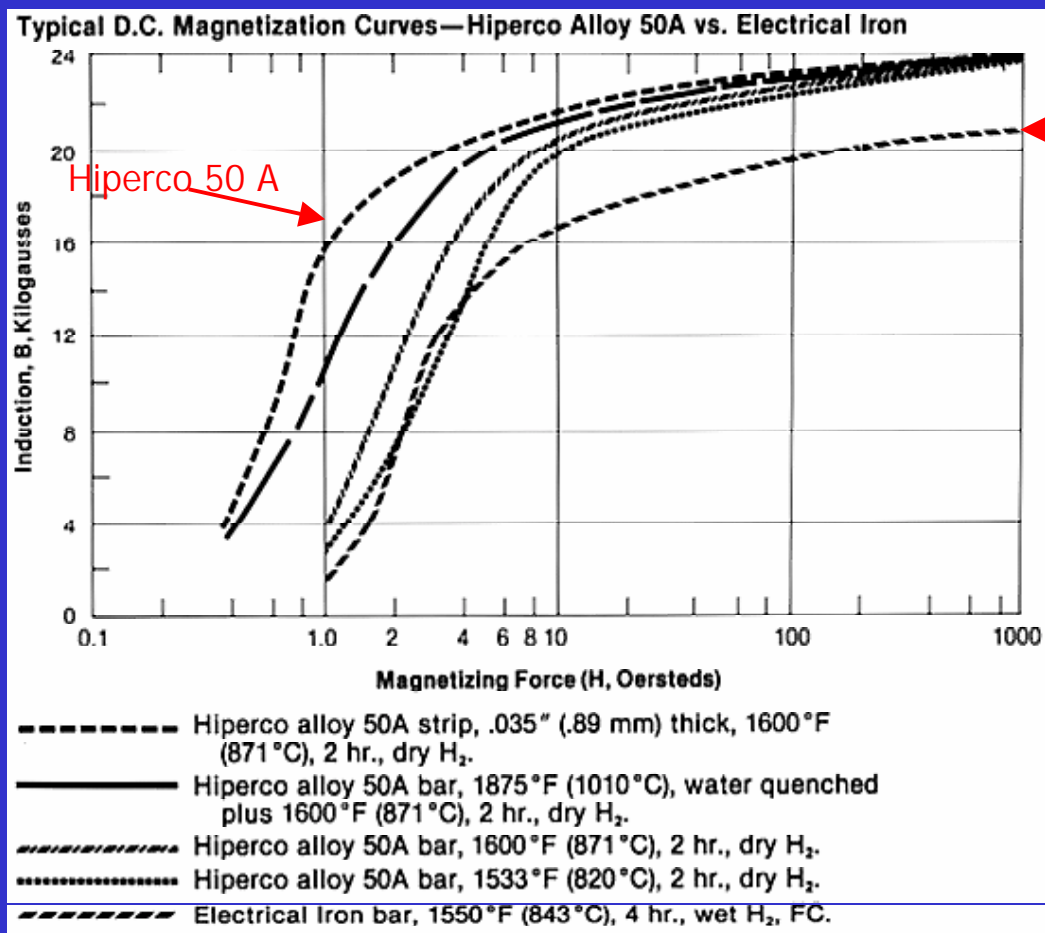
The constraints in the design of the dipoles are so strong. In principle, it is possible to use traditional iron dipoles, but:

- The simulations indicate that at energy above 1 GeV the dipole is saturated from the corresponding magnetic field, not just in the pole tips, but also in the iron yoke. This also implies very high stray fields!
- At high fields the current density is very high. This involves very high electric power cost and new power supply.
- The field quality is about 10^{-3} , even in a good field region of ± 20 mm. It can be better without the ramping.



SECOND SOLUTION: HIGH PERFORMANCE MATERIAL

Permendur (Hyperco 50 A)



Iron

| Material | B _{sat} [Tesla] | Coercitive Force [Amp/m] |
|-------------|--------------------------|--------------------------|
| Hyperco 50A | 2.40 | 79.6 |
| Pure Iron | 2.15 | 79.6 |
| 1008 Steel | 2.09 | 64 |

Design Criteria

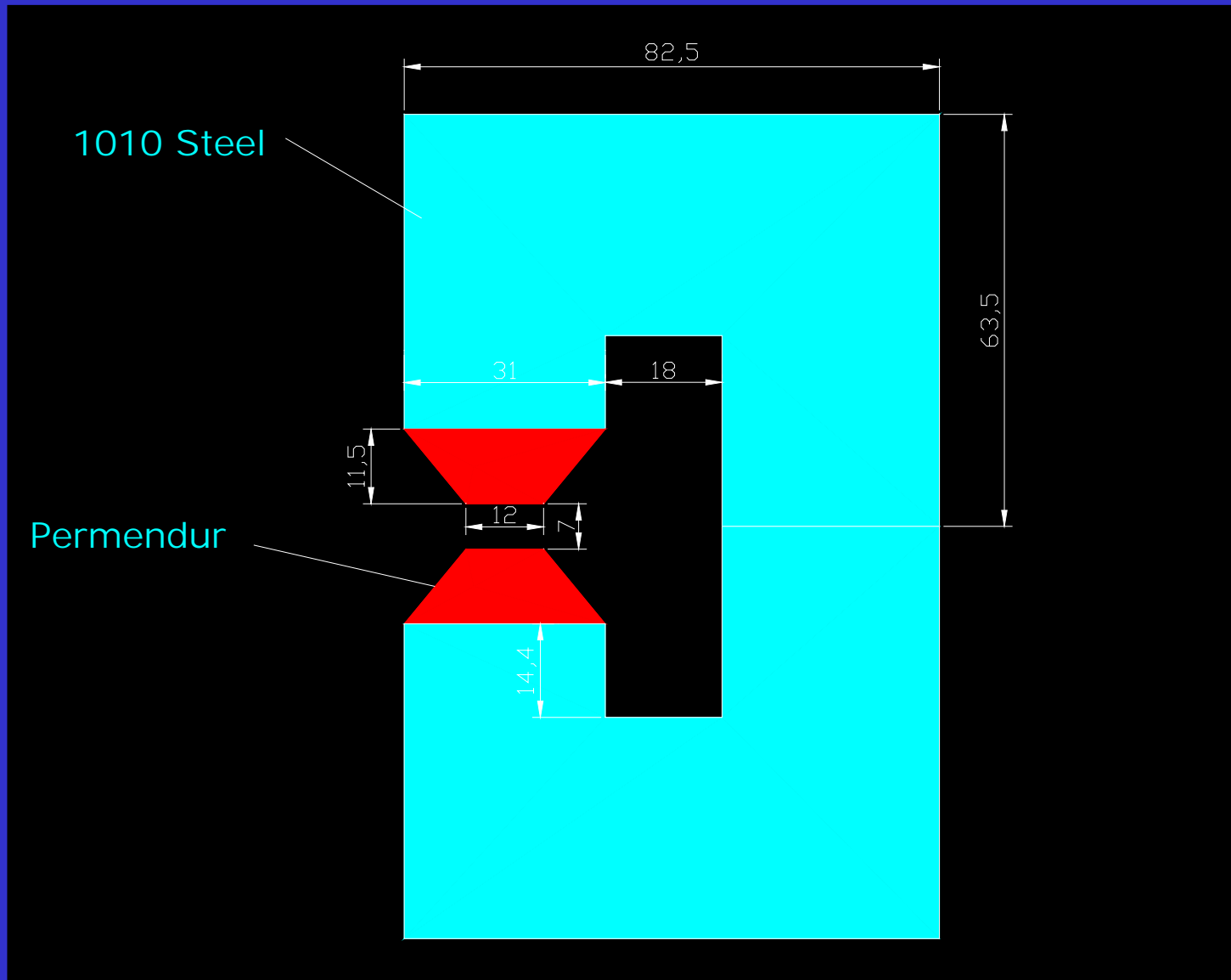
Target: Use the same section of Dafne Dipoles

- Concentrate the flux reducing the tip pole section
- Reduce NI

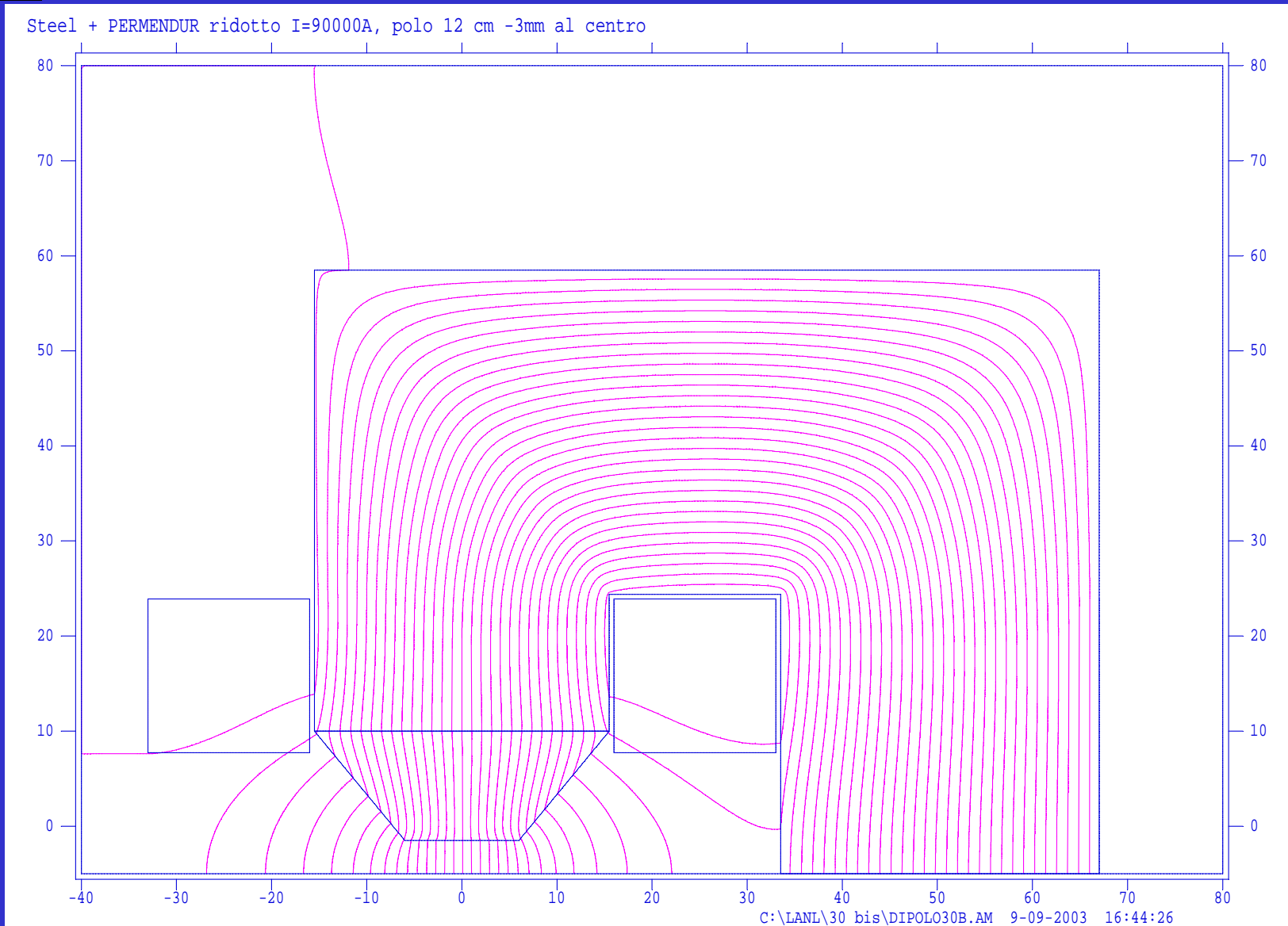


| | | |
|--------------------------------|---|-----------|
| Normal flux density in yoke | → | Steel |
| High flux density in tip poles | → | Permendur |

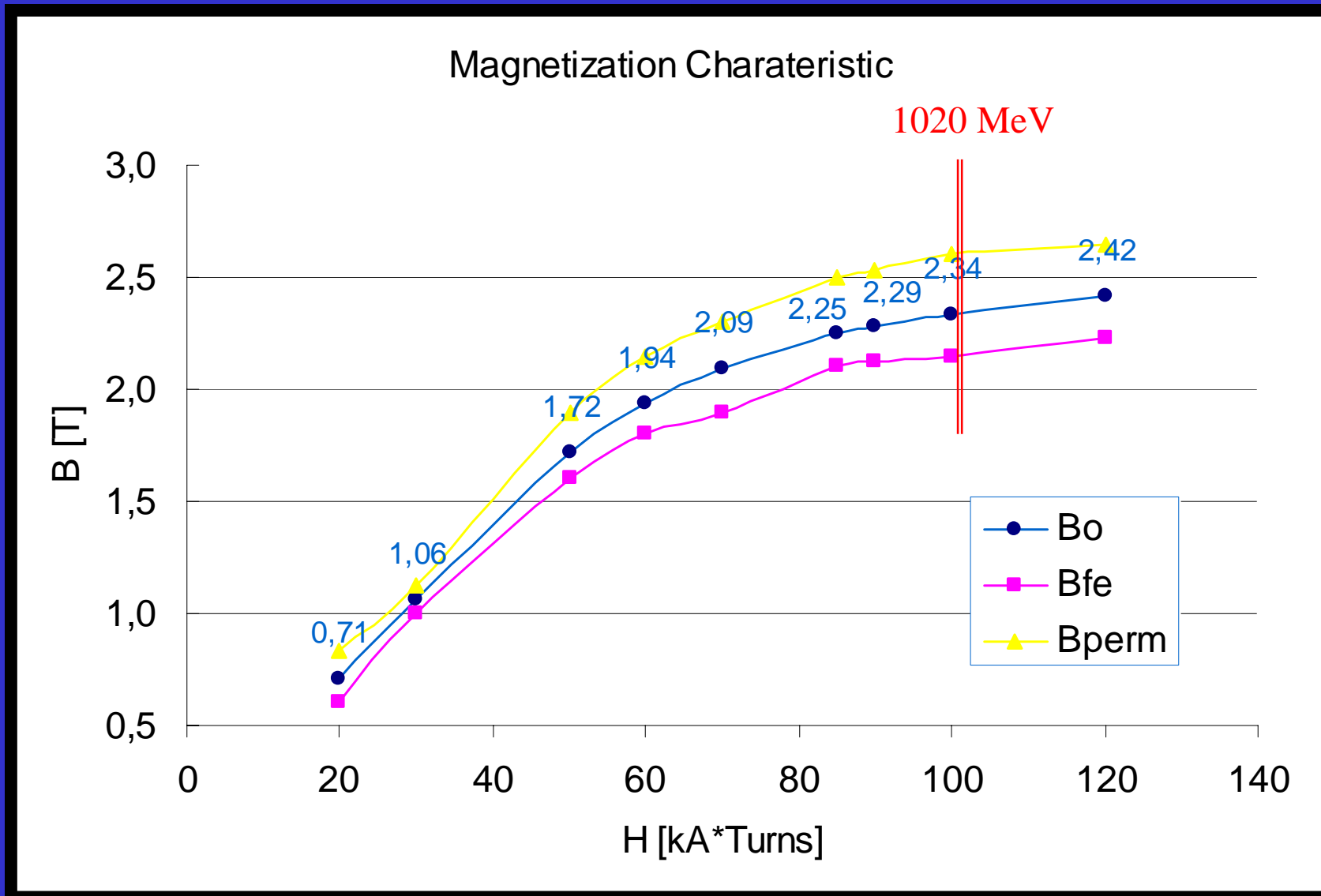
Dipole Section



Poisson 2d Output



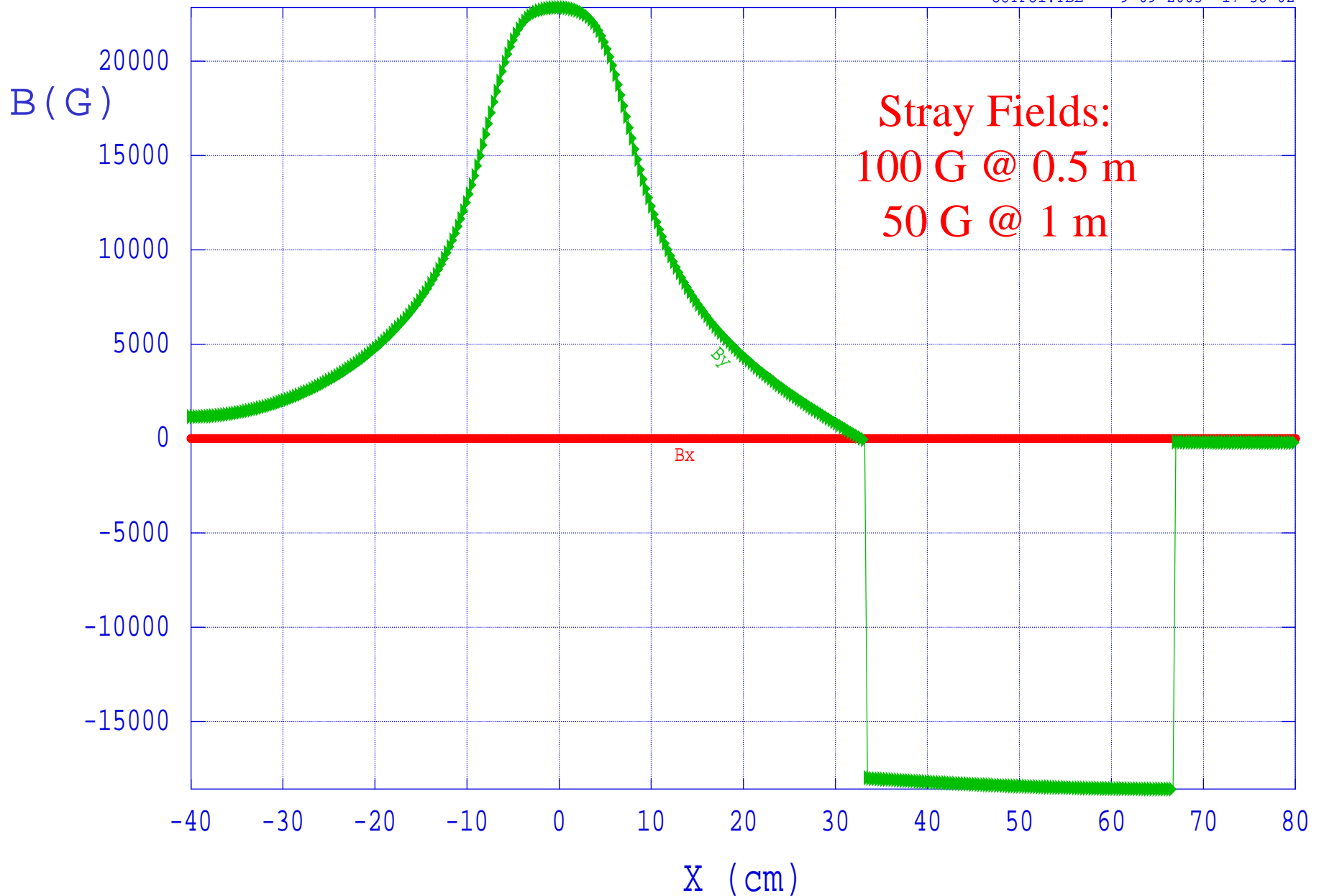
Magnetization Curve



Magnetic field from Poisson run on file DIPOL030B.AM

Problem title line 1: Steel + PERMENDUR ridotto I=90000A, polo 12 cm -

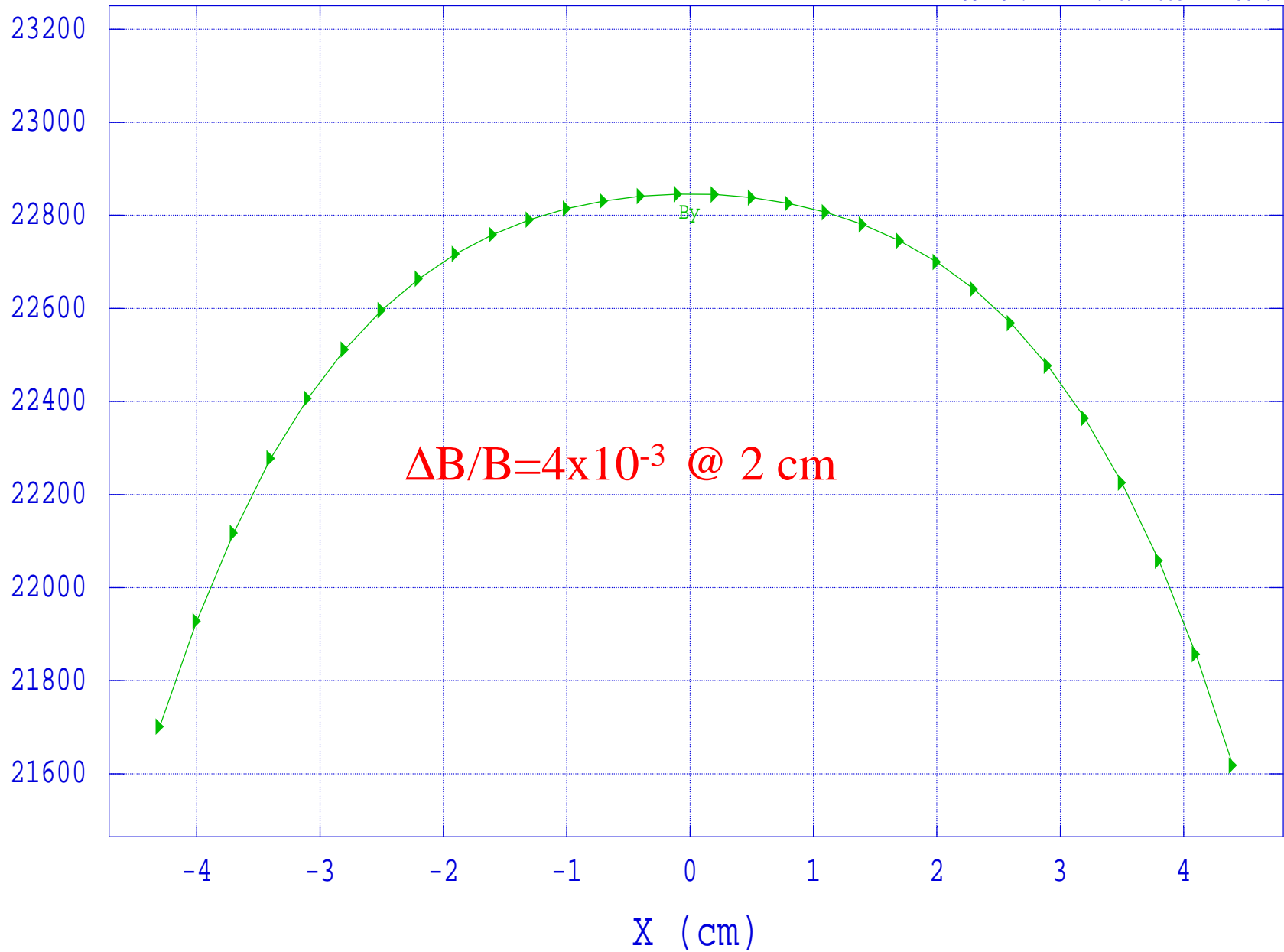
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Magnetic field from Poisson run on file DIPOL030B.AM

Problem title line 1: Steel + PERMENDUR ridotto I=90000A, polo 12 cm -

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Steel/Permendur Dipole Summary

$B = 2.22 \text{ T @ } 1020 \text{ MeV}$

$NI = 90 \text{ kA} \quad J = 6 \text{ A/mm}^2$

| | Dipole Type | | Total Dafne 2 |
|-------------------------------|-------------|-------|------------------|
| | Long | Short | |
| Volume [m³] | | | |
| Steel | 1,05 | 0,88 | 15,45 |
| Permendur | 0,07 | 0,06 | 0,98 |
| Copper | 0,10 | 0,09 | 1,52 |
| Weight [kg] | | | |
| Steel | 8260 | 6974 | 122000 |
| Permendur | 537 | 454 | 7926 |
| Copper | 891 | 776 | 13336 |
| Tot Type | 9688 | 8203 | 143130 |
| Power [kW] | | | |
| | 78 | 68 | 1173 |

Permendur Cost
estimate: 950 k€
(120 €/kg)

Same Power
Supply of Dafne



Work to do

- Pole profile optimization on 2D in order to increase field quality
- 3D analysis