NED Status Report





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CARE General Meeting LNF 17 November 2006

CARE/NED JRA





- The NED Activity is articulated around four Work Packages and one Working Group
 - 1 Management & Communication (M&C),
 - 2 Thermal Studies and Quench Protection (TSQP),
 - 3 Conductor Development (CD),
 - 4 Insulation Development and Implementation (IDI),
 - 5 Magnet Design and Optimization (MDO) Working Group

(extension of scope).

• It involves 7 institutes (8 laboratories)



- Total budget: ~2 M€; EU grant: 979 k€.
- It was launched in January 2004 and was expected to last 3 years.

NED/TSQP Work Package





• The TSQ Work Package includes two main Tasks

 development and operation of a test facility to investigate and measure heat transfer to helium through conductor insulation (CEA and WUT; Task Leader: B. Baudouy, CEA),

quench protection computation

(INFN-Mi; Task Leader: G. Volpini; completed).

• Two complementary efforts, initiated by NED, are now gaining momentum and starting a life of their own

beam loss/energy deposition/temperature margin

computations

(INFN-MI and CERN; see F. Broggi's highlight talk),

- validation of CEA heat transfer measurements

(CERN; leader: D. Richter).

Heat Transfer Measurement Task

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- The He-II cryostat manufactured under WUT supervision was successfully commissioned at CEA last month (temperature stability of ~1 mK over 1 hour).
- Facility exploitation to measure heat transfer coefficient can now begin.



Validation of CEA HT Measurement (1/2)



- In parallel, D. Richter (CERN) has reanalyzed ramp-rate data from a series of short LHC dipole magnet models to extract an effective heat transfer coefficient from heated coil to superfluid helium.
- The results compare favorably with measurements performed at CEA more than 10 years ago (on samples relying on similar insulation scheme), providing that the heat transfer only occur on one coil side.



(Courtesy D. Richter, CERN)

Validation of CEA HT Measurement (2/2)





- D. Richter also performed *in situ* measurements on a coil section cut from an LHC dipole magnet coil taken out of production line.
- He relied on interstrand resistances to heat up the conductors and thermo couples to measure their temperatures.
- The measured heat transfer coefficient is 1.4 to 1.7 times higher than the one measured at CEA; more investigations are needed.



(Courtesy D. Richter, CERN)

NED Quench Computation Task

EARE



- Task was completed in early 2006 and a final report has been issued.
- Computations have been carried out for 1-m, 5-m, and 10-m long, 88-mm-aperture $\cos\theta$, layer design and 5-m-long, 160-mm-aperture, $\cos\theta$, slot design.



• Both designs can be protected, using active quench protection heaters.

NED/CD Work Package





- The CD Work Package includes two main Tasks
 - conductor development
 - (two industrial contracts under CERN supervision: Alstom/MSA,
 - France and SMI, The Netherlands; Task Leader: L. Oberli),
 - conductor characterization
 - (CEA, INFN-Ge, INFN-Mi, and TEU; Task Leader: A. den Ouden, TEU),
- It is the core of the Program and absorbs \sim 70% of the EU funding.
- It has been complemented by INFN-Ge and CERN through the development a FE wire model to simulate cabling effects *(see S. Farinon's highlight talk).*

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Conductor Development Task





• The two industrial subcontractors developing NED conductors have achieved significant milestones (see L. Oberli's highlight talk).



Alstom/NED (workability program milestone) 1.25 mm ; 78x85 µm sub-element 740 A (~1500 A/mm²) @4.2 K & 12T (measured at CERN & INFN-Mi)



SMI/NED (step II iteration) 1.26 mm ; 288 x 50 μm tube 1400 A (~2500 A/mm²) @4.2 K & 12T (measured at TEU & INFN-Mi)

FE Wire Model

EARE



- Stefania Farinon (INFN-Ge) has developed an (ANSYS[®]-based) mechanical model to compute (and, thereby, predict) the sensitivity of un-reacted, NED-type wires to transverse loading.
- This provides a unique tool to compare and optimize billet layouts with respect to cabling degradation.





Side-by-side comparisons of computed and observed deformations of un-reacted "internal tin" (left) and "PIT" (right) wires (Courtesy S. Farinon, INFN-Ge)

NED/IDI Work Package





- The IDI Work Package includes two main Tasks
 - studies on "conventional" insulation systems relying on
 ceramic or glass fiber tape and vacuum-impregnation by resin
 (CCLRC/RAL; Task Leader: S. Canfer),
 - studies on "innovative" insulation systems relying on preimpregnated fiber tapes and eliminating the need for a vacuum impregnation

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(CEA; Task Leader: F. Rondeaux).
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Conventional Insulation Task

EARE



• RAL has received 1 km of polyimide-sized S2 glass fiber tape from JPS, NC and is presently carrying out final qualification tests.



Polyimide-sized S2 glass fiber tape (Courtesy S. Canfer, CCLRC/RAL)

- It has started investigations on radiation-hard cyanate esters to replace epoxy resin for vacuum impregnation.
- It is developing an experimental set up to characterize turn-to-turn bonding in magnet coils.

Innovative Insulation Task





- CEA has launched a campaign to study the influence of the application of a pre-compression during heat treatment, so as to increase ceramic density and reduce insulation thickness.
- It should also help to eliminate large deformation measured on virgin conductor stack upon first loading and improve mechanical robustness.





Stress-strain curve measured on conductor stack (Courtesy F. Rondeaux & P. Fourcade, CEA)

NED/MDO Working Group





- The Magnet Design and Optimization (MDO) Working Group is made up of representatives from CCLRC, CEA, CERN and CIEMAT (Chairman: F. Toral, CIEMAT).
- The Working Group has completed its comparison of selected 2D magnetic configurations.
- In parallel, CERN has completed its optimization of 2D 88-mmaperture, cos0, layer magnetic design (Reference Design V2) and CCLRC/RAL has undertaken a 2D mechanical design.

2D Magnetic Design Comparison (1/2)







2D Magnetic Design Comparison (2/2)





• For a 88-mm aperture, the comparison supports the choice made earlier of the $\cos\theta$, layer design as a baseline.

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $			Layered		Slotted	Slotted	Common	Toroidal	
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$\begin{array}{c} \mbox{Current} & 25939 & 20243 & 23550 & 28950 & 27300 & 26700 & A \\ \mbox{Margin on load line} & 9.44 & 10 & 9.978 & 10.060 & 10.073 & 9.994 & \% \\ \mbox{Bore field} & 13.05 & 13.54 & 12.928 & 12.743 & 12.596 & 12.707 & T \\ \mbox{Peak field} & 13.46 & 13.974 & 13.394 & 13.266 & 13.414 & 13.465 & T \\ \mbox{Peak field} & 10.31 & 10.32 & 10.36 & 1.041 & 1.065 & 1.060 & T \\ \mbox{Peak field} for 0\% on load line & 15.01 & 15.49 & 14.879 & 14.749 & 14.917 & 14.960 & T \\ \mbox{Magnetic field quality} & 0.004 & 0.136 & -0.018 & -0.099 & 0.020 & -1.931 & 10^4 units \\ \mbox{b5} & -0.022 & 0.2635 & -0.012 & -0.009 & 0.020 & -1.931 & 10^4 units \\ \mbox{b7} & 0.024 & 0.661 & -0.007 & -0.378 & 8.895 & 0.072 & 10^4 units \\ \mbox{b7} & 0.024 & 0.661 & -0.007 & -0.378 & 8.895 & 0.072 & 10^4 units \\ \mbox{b7} & 0.024 & 0.661 & -0.007 & -0.378 & 8.895 & 0.072 & 10^4 units \\ \mbox{b7} & 0.024 & 0.661 & -0.007 & -0.378 & 8.895 & 0.072 & 10^4 units \\ \mbox{b9} - a2 (common coil) & 2.354 & -0.007 & -3.001 & -0.499 & 2.714 & -1.694 & 10^4 units \\ \mbox{Engineering current density} & 371.02 & 313.2 & 406.472 & 425.860 & 401.589 & 392.760 & A/mm ^2 \\ \mbox{Stored energy/aperture / unit length} & 1.471 & 2.19 & 1.628 & 1.304 & 2.111 & 2.987 & MJ/m \\ \mbox{Stray magnetic field} & -at 50 mm of the outer iron radius & 0.03 & 0.06 & 0.096 & 0.034 & 0.908 & 1.781 & T \\ - at 50 mm of the outer iron radius & 0.03 & 0.06 & 0.096 & 0.034 & 0.908 & 1.781 & T \\ - at 50 mm of the outer iron radius & 0.33 & 0.06 & 0.096 & 0.034 & 0.908 & 1.781 & T \\ - art 1 m away from the magnet center & 0.006 & 0.015 & 0.018 & 0.006 & 0.072 & 0.133 & T \\ - Fx per side of aperture & 13.37 & 19 & 13.894 & 12.072 & 13.049 & 11.199 & MN/m \\ - Fy per quadrant & -3.233 & -3.54 & -3.062 & -2.846 & -0.210 & -3.004 & MN/m \\ - Fx and xamum accumulated membrane stress & parallel & 10.62 & 65 & 126.390 & 111.984 & 110.281 & 115.231 & MPa \\ \mbox{Maximum accumulated membrane stress } parallel & 10.62 & 65 & 126.390 & 111.984 & 110.281 & 115.231 & MPa \\ Maximum accu$	Outer iron yoke radius		475	500	450	450	500/250	450	mm
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Magnetic field quality $b3$ 0.0040.136-0.018-0.0990.020-1.93110 4 units $b5$ -0.0220.2635-0.012-0.009-0.181-0.04510 4 units $b7$ 0.0240.661-0.007-0.3788.8950.07210 4 units $b9 - a2$ (common coil)0.8710.247-3.857-7.572-0.448-3.78510 4 units $b11 - a4$ (common coil)2.354-0.007-3.001-0.4992.714-1.69410 4 unitsEngineering current density371.02313.2406.472425.860401.589392.760A/mm 2 Stored energy /aperture / unit length1.4712.191.6281.3042.1112.987MJ/mStray magnetic field at 50 mm of the outer iron radius0.030.060.0960.0340.9081.781T- at 1 m away from the magnet center0.0060.0150.0180.0060.0720.133T- Fx per side of aperture13.371913.89412.07213.04911.198MN/m- Fy per quadrant-3.233-3.54-3.062-2.846-0.210-3.004MN/m- Maximum accumulated membrane stress125.2107118.69139.60671.76489.373MPa- Maximum accumulated membrane stressparallel101.6265126.390111.984110.281 <td>Peak field for 0% on load line</td> <td></td> <td>15.01</td> <td>15.49</td> <td>14.879</td> <td>14.749</td> <td>14.917</td> <td>14.960</td> <td>Т</td>	Peak field for 0% on load line		15.01	15.49	14.879	14.749	14.917	14.960	Т
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$b7$ 0.024 0.661 -0.007 -0.378 8.895 0.072 10^{-4} units $b9 - a2$ (common coil) 0.871 0.247 -3.857 -7.572 -0.448 -3.785 10^{-4} units $b11 - a4$ (common coil) 2.354 -0.007 -3.001 -0.499 2.714 -1.694 10^{-4} unitsEngineering current density 371.02 313.2 406.472 425.860 401.589 392.760 A/mm^2 Self inductance /aperture / unit length 4.373 10.71 5.869 3.112 5.662 8.380 mH/mStored energy/aperture / unit length 1.471 2.19 1.628 1.304 2.111 2.987 MJ/mStray magnetic field $-at 50$ mm of the outer iron radius 0.03 0.06 0.096 0.034 0.908 1.781 T- at 1 m away from the magnet center 0.006 0.015 0.018 0.006 0.072 0.133 TLorentz forces $-Fx$ per side of aperture 13.37 19 13.894 12.072 13.049 11.198 MN/m- Fx per side of aperture 125.2 107 118.691 39.606 71.764 89.373 MPa- Maximum accumulated membrane stressparallel 101.62 65 126.390 111.984 110.281 115.231 MPa	<i>b5</i>		-0.022	0.2635	-0.012	-0.009	-0.181	-0.045	10 ⁻⁴ units
$b9 - a2$ (common coil) 0.871 0.247 -3.857 -7.572 -0.448 -3.785 10^{-4} units $b11 - a4$ (common coil) 2.354 -0.007 -3.001 -0.499 2.714 -1.694 10^{-4} unitsEngineering current density 371.02 313.2 406.472 425.860 401.589 392.760 A/mm^2 Self inductance /aperture / unit length 4.373 10.71 5.869 3.112 5.662 8.380 mH/m Stored energy /aperture / unit length 1.471 2.19 1.628 1.304 2.111 2.987 MJ/m Stray magnetic field $ 0.03$ 0.06 0.096 0.034 0.908 1.781 T - at 1 m away from the magnet center 0.006 0.015 0.018 0.006 0.072 0.133 T Lorentz forces $ Fx$ per side of aperture 13.37 19 13.894 12.072 13.049 11.198 MN/m - Maximum accumulated membrane stress 125.2 107 118.691 39.606 71.764 89.373 MPa - Maximum accumulated membrane stressparallel 10.62 65 126.390 111.984 110.281 115.231 MPa	<i>b</i> 7		0.024	0.661	-0.007	-0.378	8.895	0.072	10 ⁻⁴ units
$b11 - a4$ (common coil) 2.354 -0.007 -3.001 -0.499 2.714 -1.694 10^{-4} unitsEngineering current density 371.02 313.2 406.472 425.860 401.589 392.760 A/mm^2 Self inductance /aperture / unit length 4.373 10.71 5.869 3.112 5.662 8.380 mH/mStored energy /aperture / unit length 1.471 2.19 1.628 1.304 2.111 2.987 MJ/mStray magnetic field at 50 mm of the outer iron radius 0.03 0.06 0.096 0.034 0.908 1.781 T- at 1 m away from the magnet center 0.006 0.015 0.018 0.006 0.072 0.133 TLorentz forces 13.37 19 13.894 12.072 13.049 11.198 MN/m- Fy per quadrant-3.233-3.54-3.062-2.846-0.210-3.004MN/m- Maximum accumulated membrane stress perp endicular to the broad side of the cable 125.2 107 118.691 39.606 71.764 89.373 MPato the broad side of the cable 101.62 65 126.390 111.984 110.281 115.231 MPa	b9 - a2 (common coil)		0.871	0.247	-3.857	-7.572	-0.448	-3.785	10 ⁻⁴ units
Engineering current density 371.02 313.2 406.472 425.860 401.589 392.760 A/mm^2 Self inductance /aperture / unit length 4.373 10.71 5.869 3.112 5.662 8.380 mH/mStored energy /aperture / unit length 1.471 2.19 1.628 1.304 2.111 2.987 MJ/mStray magnetic field- at 50 mm of the outer iron radius 0.03 0.06 0.096 0.034 0.908 1.781 T- at 1 m away from the magnet center 0.006 0.015 0.018 0.006 0.072 0.133 TLorentz forces 7.54 7.54 7.54 7.604 MN/m- Fx per side of aperture 13.37 19 13.894 12.072 13.049 11.198 MN/m- Maximum accumulated membrane stress perp endicular to the broad side of the cable 125.2 107 118.691 39.606 71.764 89.373 MPa- Maximum accumulated membrane stress parallel 101.62 65 126.390 111.984 110.281 115.231 MPa	<i>b11 a4</i> (common coil)		2.354	-0.007	-3.001	-0.499	2.714	-1.694	10 ⁻⁴ units
Self inductance /aperture / unit length 4.373 10.71 5.869 3.112 5.662 8.380 mH/mStored energy /aperture / unit length 1.471 2.19 1.628 1.304 2.111 2.987 MJ/mStray magnetic field- at 50 mm of the outer iron radius 0.03 0.06 0.096 0.034 0.908 1.781 T- at 1 m away from the magnet center 0.006 0.015 0.018 0.006 0.072 0.133 TLorentz forces Fx per side of aperture 13.37 19 13.894 12.072 13.049 11.198 MN/m- Fy per quadrant-3.233-3.54-3.062-2.846-0.210-3.004MN/m- Maximum accumulated membrane stress perp endicular to the broad side of the cable 125.2 107 118.691 39.606 71.764 89.373 MPa- Maximum accumulated membrane stress parallel 101.62 65 126.390 111.984 110.281 115.231 MPa	Engineering current density		371.02	313.2	406.472	425.860	401.589	392.760	A/mm ²
Stored energy /aperture / unit length 1.471 2.19 1.628 1.304 2.111 2.987 MJ/mStray magnetic field- at 50 mm of the outer iron radius 0.03 0.06 0.096 0.034 0.908 1.781 T- at 1 m away from the magnet center 0.006 0.015 0.018 0.006 0.072 0.133 TLorentz forces Fx per side of aperture13.371913.89412.07213.04911.198MN/m- Fy per quadrant-3.233-3.54-3.062-2.846-0.210-3.004MN/m- Maximum accumulated membrane stress perp endicular to the broad side of the cable125.2107118.69139.60671.76489.373MPa- Maximum accumulated membrane stress parallel101.6265126.390111.984110.281115.231MPa	Self inductance /aperture /unit length		4.373	10.71	5.869	3.112	5.662	8.380	mH/m
Stray magnetic field- at 50 mm of the outer iron radius 0.03 0.06 0.096 0.034 0.908 1.781 T- at 1 m away from the magnet center 0.006 0.015 0.018 0.006 0.072 0.133 TLorentz forces13.894 12.072 13.049 11.198 MN/m- Fy per quadrant-3.233-3.54-3.062-2.846-0.210-3.004MN/m- Maximum accumulated membrane stress perp endicular to the broad side of the cable125.2107118.69139.60671.76489.373MPa- Maximum accumulated membrane stress parallel101.6265126.390111.984110.281115.231MPa	Stored energy /aperture / unit length		1.471	2.19	1.628	1.304	2.111	2.987	MJ/m
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Stray magnetic field								
- at 1 m away from the magnet center 0.006 0.015 0.018 0.006 0.072 0.133 TLorentz forces-13.371913.89412.07213.04911.198MN/m- Fy per quadrant-3.233-3.54-3.062-2.846-0.210-3.004MN/m- Maximum accumulated membrane stress perp endicular to the broad side of the cable125.2107118.69139.60671.76489.373MPa- Maximum accumulated membrane stress perp endicular to the broad side of the cable101.6265126.390111.984110.281115.231MPa	- at 50 mm of the outer iron radius		0.03	0.06	0.096	0.034	0.908	1.781	Т
Lorentz forces - 13.37 19 13.894 12.072 13.049 11.198 MN/m - Fy per quadrant -3.233 -3.54 -3.062 -2.846 -0.210 -3.004 MN/m - Maximum accumulated membrane stress 125.2 107 118.691 39.606 71.764 89.373 MPa - Maximum accumulated membrane stress parallel 101.62 65 126.390 111.984 110.281 115.231 MPa	- at 1 m away from the magnet center		0.006	0.015	0.018	0.006	0.072	0.133	Т
- Fx per side of aperture13.371913.89412.07213.04911.198MN/m- Fy per quadrant-3.233-3.54-3.062-2.846-0.210-3.004MN/m- Maximum accumulated membrane stress perp endicular to the broad side of the cable - Maximum accumulated membrane stress to the broad side of the cable125.2107118.69139.60671.76489.373MPa- Maximum accumulated membrane stress to the broad side of the cable101.6265126.390111.984110.281115.231MPa	Lorentz forces								
- Fy per quadrant- 3.233- 3.54- 3.062- 2.846- 0.210- 3.004MN/m- Maximum accumulated membrane stress perp endicular to the broad side of the cable - Maximum accumulated membrane stress125.2107118.69139.60671.76489.373MPa- Maximum accumulated membrane stress to the broad side of the cable101.6265126.390111.984110.281115.231MPa	- <i>Fx</i> per side of aperture		13.37	19	13.894	12.072	13.049	11.198	MN/m
- Maximum accumulated membrane stress perp endicular to the broad side of the cable - Maximum accumulated membrane stress125.2107118.69139.60671.76489.373MPa- Maximum accumulated membrane stress to the broad side of the cable101.6265126.390111.984110.281115.231MPa	- Fy per quadrant		-3.233	-3.54	-3.062	-2.846	-0.210	-3.004	MN/m
perp endicular to the broad side of the cable123.2107116.09139.00071.70489.575MFa- Maximum accumulated membrane stressparallel101.6265126.390111.984110.281115.231MPa	- Maximum accumulated membrane stress		125.2	107	119 601	20,606	71 764	80 272	MDo
- Maximum accumulated membrane stress parallel 101.62 65 126.390 111.984 110.281 115.231 MPa to the broad side of the cable	perp endicular to the broad side of the cable		123.2	107	116.091	39.000	/1./04	69.575	NIFa
to the broad side of the cable	- Maximum accumulated membrane stress	parallel	101.62	65	126 200	111.084	110 281	115 221	MDo
	to the broad side of the cable		101.02	0.5	120.390	111.904	110.201	113.231	wira

(Courtesy F. Toral, CIEMAT)

Reference Design V2





- CERN has completed its 2D electromagnetic optimization of baseline, 88-mm-aperture, $\cos\theta$ layer design with respect to
 - conductor geometry,
 - iron shape (to reduce saturation effects),
 - ferromagnetic shims (to compensate magnetization effects).



2D Mechanical Design





CCLRC/RAL is pursuing its development of a comprehensive (ANSYS[®]-based) mechanical model of baseline, 88-mm-aperture, cosθ layer design throughout the various steps of manufacturing, cooldown and energization.





(Courtesy P. Loveridge, CCLRC/RAL)

Preparing for NED Phase II





- Most Tasks of the present NED Activity are expected to be completed during the first semester of 2007.
- By then (next Summer?), we should have: 4 Alstom/MSA and 2 SMI cable UL's, a conventional insulation system and a conceptual design.
- The next step would naturally be to build a couple of magnet models.
- Following the recommendation issued by ESGARD last May, the NED partners have investigated the possibility of maintaining the collaboration so as to carry out the detailed design, manufacture and test of NED magnets on internal funding.
- This led to the elaboration of a tentative Program and a preliminary cost estimate, that was reported to ESGARD in September.

Tentative NED Phase II Program





- The proposed NED Phase II Program is to build by 2009 one dipole magnet model with Alstom/MSA cable and one with SMI cable, relying on the $\cos\theta$, layer design and the conventional insulation system.
- The NED Phase II proposal is articulated around 3 main Work Packages
 - WP1: Design and Integration (01/07-12/09),
 - WP2: Supporting R&D and Demonstrators (01/07-06/08), WP3: Model Magnet Manufacturing and Test (07/07-12/09).
- WP1&2 call for paper studies and small-scale models that only requires limited investments; they need to be be launched right away.
- WP3 calls for significant material costs and human resources and its launching may be differed by 6 to 9 months.

NED Demonstrators





- The goal of WP2 is to build and test pairs of short Racetrack-type coils to validate, with a fast turnaround time, cable design, insulation choice and optimize various mechanical features.
- It is inspired from the successful "Short Model Coil" program carried out at LBNL and will be developed in collaboration with US-LARP.
- First results are expected by the end of 2007.





(Courtesy H. Félice, CEA)

NED Manufacturing and Test





- WP3 is articulated around 3 main Tasks
 - 3.1: Pole manufacturing
 - detailed design and manufacturing of 10 poles (4 dummy,
 - 4 Alstom/MSA, 2 SMI + possible extension to 4 Luvata)
 - 3.2 Collaring and cold mass assembly
 manufacture and test of 2 collaring and 1 yoking/shell welding
 model, collaring and yoking/shell welding of 2 NED magnets
 (1 Alstom and 1 SMI + possible extension to 1 Luvata)
 - 3.3: magnet test

adaptation of CERN FRESCA facility to high current (29 kA at 4.2 K, 32 ka at 1.9 K), large stored energy (2.3 MJ) and heavy load (7.5 t) operations and test of 2 to 3 NED magnets.

NED Phase II Budget & Schedule



NED

Work Package/Task	k€	Staff.month
WP1: Design and Integration	n/a	72
WP2: Supporting R&D and Demonstrators	350*	72
WP3.1: Pole manufacturing (x10)	550	164
WP3.2: Collaring & Cold Mass Assembly (x2)	450	72
WP3.3: Magnet Test (x2)	150	30
Total	1500	410

2007 2008 2009 2010 NED Phase II Qtr3 Qtr4 Qtr 1 Qtr2 Qtr3 Qtr 4 Qtr 1 Qtr2 Qtr3 Qtr4 Qtr 1 Qtr2 Qtr3 Qtr4 Qtr 1 1. Design and Integration 2 Supporting R&D and Demonstrators 3 Pole Manufacturing 4. Collaring and Cold Mass Assembly **5 Magnet Test**

Conclusion





- Significant progress have been achieved for most Tasks, and we can prepare the Activity landing.
- Foreseen end dates of various Tasks are
 - Task 2.2 (Heat Transfer Measurements): 31 September 2007
 - Task 2.3 (Quench Computation): completed
 - Task 3.2 (Preliminary Design): completed
 - Task 3.3 (Conductor Specifications): completed
 - Task 3.4&5 (Wire Development & Characterization): 30 June 2007
 - Task 3.6&7 (Cable Development & Characterization): 30 June 2007
 - Task 4.2 (Insulation Specifications): completed
 - Task 4.3 (Conventional Insulation): 31 December 2006
 - Task 4.4 (Innovative Insulation): 31 March 2007
- Preparation is ongoing for NED Phase II.