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# COMPARISON OF MAGNETIC AND MECHANICAL CENTER POSITIONS OF SMALL QUADRUPOLES AND SEXTUPOLES IN THE DAФNE MAIN RINGS 

B. Bolli, N. Ganlin, F. Iungo, F. Losciale, M. Paris, M. Preger, C. Sanelli, F. Sardone, F. Sgamma, M. Troiani

## 1. Introduction

The magnetic measurements on the 60 "small" quadrupoles and 14 "small" sextupoles of the DAФNE Main Rings are described in [1,2]. These measurements included also the position of the magnetic center of each magnet, while the determination of the mechanical center positions has been performed later, directly in the Main Rings Hall. We present here the methods and results of both kinds of measurements and the comparison between them.

## 2. Magnetic center position

The position of the magnetic center of each quadrupole is the result of the alignment procedure performed with the rotating coil system of the magnetic measurement laboratory [3].

An alignment table is precisely positioned on top of each magnet by means of three removable supporting cylinders leaning directly on the upper lamination stacks of the quadrupoles and on a machined reference surface of the sextupoles. The table is equipped with two micrometric slits, each holding a Taylor-Hobson sphere (A and B). The sphere centers are the reference of the magnet with respect to the laser beam of the rotating coil system, placed parallel to the rotating coil axis in a vertical plane at a distance of 350 mm from it. The accuracy of the system is discussed in [4].

The magnet is placed on the movable support of the rotating coil system, and the plane of the alignment table is accurately set horizontally by means of a levelling system. In this way we make sure that the mechanical azimuthal tilt (defined as the rotation around the longitudinal symmetry axis of the magnet) and the mechanical vertical tilt (defined as the rotation around an axis perpendicular to the longitudinal one and lying in the horizontal symmetry plane of the magnet) are negligible. However, there is no way of making the mechanical horizontal tilt (defined as the rotation around an axis perpendicular to the longitudinal one and lying in the vertical symmetry plane of the magnet) negligible as well, and therefore the magnet is placed on the support by placing the poles as parallel as possible to the rotation coil.

We recall that the rotating coil system cannot give any indication on the magnetic horizontal and vertical tilts, because it measures only the position of the average magnetic center. This information can only come from the mechanical measurements, as explained in the following. On the contrary, it is capable of measuring the azimuthal rotation $\Phi$ of the magnetic horizontal symmetry axis with respect to the mechanical position set by the levelling procedure of the alignment table. A positive $\Phi$ value means that the magnet, seen from the electrical and cooling connections side, must be rotated counterclockwise by the angle $\Phi$ to have the magnetic symmetry plane coincident with the ideal horizontal plane of the ring. Of course, the plane of the alignment table will then be tilted by the corresponding amount

After the initial positioning of the magnet on the rotating coil system support, the system indicates the horizontal and vertical displacements to be applied in order to bring the magnetic center of the magnet on the axis of the rotating coil. After a few iterations it is possible to reach a situation where these displacement are of the order of few microns. At this point the sphere centers are horizontally set on the laser beam by means of the micrometric movements and their readings (XAmag and XBmag) recorded. The laser system indicates the vertical displacement of the laser beam with respect to the center of each sphere, and these values are subtracted from 350 mm to give the vertical distances (YAmag and YBmag) between the center of the spheres and the magnetic axis. It is important to remark that the system also rotates the magnet by the angle $\Phi$ azimuthally to correct the magnet rotation before performing the field quality analysis. The vertical positions of the sphere centers are practically not affected by this rotation, while their horizontal positions change by 350 mm times the rotation angle. The final horizontal readings are therefore taken including the azimuthal correction.

These four positions have been measured on the 60 small quadrupoles of the DAФNE Main Rings using the alignment table Q3. The results of the measurements are given in Table I. The 14 sextupoles have been measured with the alignment table S 1 and the results are shown in Table II.

## 3. Mechanical center position

The position of the mechanical axis of the magnets has been measured in the DAФNE Main Rings Hall by means of a computer controlled equipment using two theodolites.

The mechanical axis of the magnet is simulated with an half-cylinder, leaning on the surfaces of the lower poles of magnets with two precision cylindrical ribs and having three optical targets, as shown in Figure 1. The two targets 1 and 2 are exactly on the axis of the cylinder defined by the two ribs.

The table is accurately levelled, acting on the adjustable supports of the magnets, to get a vanishing azimuthal angle; then the half-cylinder is rotated until the line parallel to the direction $2-->3$ is horizontal: in this way it is also parallel to the table.

The slits are positioned in an arbitrary but fixed position, so that the sphere centers are very near to the vertical plane passing through the cylinder axis. Then the positions of the five points (1, 2, 3 and sphere centers in A and B), referred to the reference system of the measuring equipment, are measured and recorded. These measures are later computed to obtain the positions of sphere centers A and B in the reference system defined in the figure.


Figure 1-Half-cylinder simulating the mechanical axis of the magnet
The readings of slits A and B , corresponding to a situation where the two sphere centers are on the vertical plane passing through the cylinder axis, are then computed and recorded as XAmec and XBmec. The distances of the sphere centers from the XY plane are recorded as YAmec and YBmec.

Each quadrupole and sextupole has been measured with three alignment tables, Q1, Q2 and Q3 for the quadrupoles, S1, S2 and S3 for the sextupoles. Table III reports the results for the quadrupoles with Q 1, Table IV the sextupoles with S 1 , Table V the quadrupoles with Q 2, Table VI the sextupoles with S2, Table VII the quadrupoles with Q3 and Table VIII the sextupoles with S3. Tables IV and VII are used for the comparison with the magnetic measurements described in the following section.

The accuracy of the measurements (maximum errors) is $\pm 0.10 \mathrm{~mm}$ in the horizontal plane, $\pm 0.05 \mathrm{~mm}$ in the vertical one.

## 4. Comparison between mechanical and magnetic center position

The magnetic measurements have been performed only with the alignment tables Q3 and S1. The results obtained for the other tables used for the mechanical measurements are useful anyway, since the tables have been calibrated against each other.

As mentioned in Section 1, the rotating coil system gives only the average position of the magnetic center along the longitudinal axis of the magnet, while the horizontal and vertical tilts are derived from the mechanical measurements.

Comparing the results in Tables I and VII for the quadrupoles, II and IV for the sextupoles, it is possible to find the average displacement of the magnetic axis from the mechanical one. Taking into account that the readings of the movable slits increase in opposite directions for the two slits, we can define two variables $\triangle \mathrm{XA}$ and $\triangle \mathrm{XB}$ representing the horizontal distance between the magnetic and mechanical readings of the two slits for each magnet:

$$
\begin{aligned}
& \Delta \mathrm{XA}=\mathrm{XAmag}-\mathrm{XAmec} \\
& \Delta \mathrm{XB}=\mathrm{XBmec}-\mathrm{XBmag}
\end{aligned}
$$

and the distance between the magnetic and mechanical axes is the average of $\triangle \mathrm{XA}$ and $\Delta \mathrm{XB}$ :

$$
\text { ShiftX }=\frac{\Delta X A+\Delta X B}{2}
$$

Let us discuss the meaning of the sign of the variables defined above. The small quadrupoles (and sextupoles) are positioned on the movable support of the measuring system in such a way that the electrical and cooling connections are on the encoder side of the rotating coil. The A slit is on the encoder side as well and its reading increases when the Taylor-Hobson sphere moves from left to right. The B slit, as mentioned before, increases its reading when the corresponding sphere moves from right to left. Let us assume that the magnet is initially positioned with its mechanical center exactly aligned on the axis of the rotating coil, and that its magnetic center is on the right. In order to bring the magnetic center on the coil axis, the system displaces the magnet towards the left; now, our procedure is such that the slit reading is taken with the sphere centers on the laser, which is in the same horizontal position as the coil axis, and to obtain this alignment the A sphere must be moved to the right, thus increasing its reading with respect to the initial value. With our definition, therefore, a positive value for $\triangle$ XA and ShiftX indicates that the magnetic center of the magnet is on the right with respect to the mechanical one, when the magnet is observed from the electrical and cooling connection side.

From $\triangle \mathrm{XA}$ and $\triangle \mathrm{XB}$ it is also possible to find the horizontal projection of the angle between the mechanical axis measured with the alignment optical system and the axis of the magnet positioned on the rotating coil system. We recall that the alignment of the magnet in the horizontal plane on the magnetic measurement system is rather rough, and therefore this angle can reach large and random values. This horizontal tilt is obtained as the difference between $\Delta \mathrm{XA}$ and $\Delta \mathrm{XB}$ divided by the longitudinal distance L between the centers of the spheres (170 mm for the quadrupoles, 100 mm for the sextupoles).

$$
\text { TiltX }=\frac{\Delta \mathrm{XA}-\Delta \mathrm{XB}}{\mathrm{~L}}
$$

The corresponding quantities for the vertical plane are defined in the same way, with the warning that the differences between the vertical positions of the two slits are taken in the same direction:

$$
\begin{aligned}
& \Delta \mathrm{YA}=\mathrm{YAmag}-\mathrm{YAmec} \\
& \Delta \mathrm{YB}=\mathrm{YBmag}-\mathrm{YBmec}
\end{aligned}
$$

In addition, the distribution for TiltY is now much narrower than in the horizontal case, due to the preliminary levelling of the alignment table in the horizontal plane during the magnetic measurements.

Table IX gives the values of ShiftX, ShiftY, TiltX and TiltY for the quadrupoles. The last column (ShiftXC) takes into account the effect of the azimuthal rotation performed by the rotating coil system to bring the magnetic horizontal plane of the magnet on the horizontal plane of the machine. This rotation, which is not applied during the mechanical measurement procedure, displaces the horizontal position of the sphere centers by the vertical distance between the sphere centers and the magnetic axis of the magnet times the rotation angle. The values of ShiftXC are therefore corrected by this amount to be better compared with the mechanical results. Table X shows the same quantities for the sextupoles.

We need to discuss again on the sign of the correction, as we did before for the displacement between the mechanical and magnetic centers. When the angle $\Phi$ in Tables I and II is positive, the system rotates the magnet in the counterclockwise direction, always looking from the electrical and cooling connection side, before performing the field quality measurement. When $\Phi$ is positive, therefore, the A sphere moves towards the left, and the slit must bring it again to the right in order to reach the position of the laser. In this case the reading of slit A is further increased and the corresponding value must be subtracted from ShiftX in order to have a correct comparison between the mechanical and magnetic center positions.

Figure 2 shows in an XY plane the uncorrected distance between the magnetic and mechanical axes of the quadrupoles. It can be noticed that there is systematic displacement in both planes: in the horizontal one the average shift and its standard deviation are +0.32 mm and 0.15 mm respectively. These values are smaller in the vertical plane $(-0.12 \mathrm{~mm}$ and 0.05 mm respectively). Figure 3 shows the same data corrected by the azimuthal rotation of the magnets: the distribution in the horizontal plane is now well centered around zero (its average is 0.05 mm ) and also its width is slightly smaller ( 0.12 mm ): the difference has been initially (see Section 5) explained by a systematic rotation of the magnetic symmetry plane with respect to the mechanical one ( 0.76 mrad on the average with 0.35 mrad r.m.s. width).


Figure 2 - Distance between magnetic and mechanical axes for the quadrupoles (not corrected for the azimuthal rotation)


Figure 3-Distance between magnetic and mechanical axes for the quadrupoles corrected for the azimuthal rotation

Figures 4 and 5 are the same plots for the sextupoles. Although the statistics is poorer than for the quadrupoles ( 14 magnets against 60 ), it is easy to notice that there is no vertical systematic displacement (the average is 0.01 mm , the standard deviation 0.04 mm ).


Figure 4-Distance between magnetic and mechanical axes for the sextupoles (not corrected for the azimuthal rotation)

After correction for the azimuthal rotation ( $\langle\Phi\rangle=0.42 \pm 0.23 \mathrm{mrad}$ ), the average horizontal shift is 0.04 mm , with an r.m.s. width of 0.18 mm .


Figure 5-Distance between magnetic and mechanical axes for the sextupoles corrected for the azimuthal rotation


Figure 6 - Horizontal and vertical angles between measured mechanical axis of the quadrupoles and magnet axis on the rotating coil system


Figure 7 - Horizontal and vertical angles between measured mechanical axis of the sextupoles and magnet axis on the rotating coil system

For sake of completeness, we show in Figures 6 and 7, for the quadrupoles and sextupoles respectively, the angles in the horizontal and vertical planes between the longitudinal axis position obtained from the mechanical measurements and the position of the magnet axis during the magnetic measurement, although, as remarked in Section 1, the latter is not the tilt of the magnetic axis, which cannot be obtained from the rotating coil system. As anticipated in that Section, the tilt distribution is much larger in the horizontal than in the vertical plane, and the vertical tilt spread is smaller for the quadrupoles, due to the larger longitudinal distance between the supporting cylinders.

## 5. Recalibration of the azimuthal rotating coil offset

As shown in Table I, the rotation $\Phi$ of the horizontal magnetic symmetry plane with respect to the mechanical one is positive for all the small quadrupoles of the DAФNE Main Rings. As already mentioned in Section 4, the average rotation is 0.76 mrad with an r.m.s. spread of 0.35 mrad . At the end of the measurements, we concluded that this small offset could be attributed to a systematic construction error of the quadrupoles. For the sextupoles, the average rotation is smaller ( $0.42 \pm 0.23 \mathrm{mrad}$ ), and its effect on the particle dynamics is negligible.

However, during the measurements on the "large" quadrupoles for the Main Ring achromats [5], the same behaviour was observed, In addition, due to the particular geometry of the electrical and cooling connections, half of the magnets were measured with the connections on the encoder side of the rotating coil and half of them on the opposite one. If the offset comes from a systematic construction error, the rotation of the magnet with respect to the measuring coil should change the sign of $\Phi$, but the measured values were again positive for all the quadrupoles. It was therefore decided to check the calibration of the coil (directly performed at the factory three years ago) by measuring the same quadrupoles once with the connections on the encoder side and once on the opposite one. In addition the calibration procedure followed by the builder, consisting in rotating the coil with respect to the quadrupole, was repeated. The two procedures were found to be in agreement with an offset variation $\Delta \Phi$ of $0.7 \pm 0.2 \mathrm{mrad}$. Applying this variation to the measurements performed on the quadrupoles, the average rotation is well within the accuracy of the measurement. Figure 8 shows the distribution of $\Phi$ among all the quadrupoles after applying the calibration correction. The corrected values are also given in Table XIII.


Figure 8-Distribution of the angle between the magnetic and mechanical horizontal symmetry planes among the 60 quadrupoles

## 6. Operating instructions for the alignment of the magnets on the rings

From the above described measurement we extract in this Section the essential information to align the small quadrupoles and sextupoles on the DAФNE Main Rings. We follow the general criterion, adopted throughout the whole project, of relying, as far as possible, on the results of magnetic measurements, integrating them, when necessary, with the mechanical ones. We take into account two possibilities:
a) alignment without compensation of the azimuthal rotation of the magnets
b) alignment with compensation of the azimuthal rotation to minimize the coupling between the betatron oscillations in the horizontal and vertical planes (it is a first order effect for the quadrupoles, a second order one for the sextupoles).

## 6a) Alignment without compensation

The average displacements in the horizontal direction between the magnetic and mechanical axes (after subtracting the effect of the rotation performed by the rotating coil system to compensate for the azimuthal rotation of the magnetic symmetry plane of the magnets) are given by ShiftXC in Tables IX (for the quadrupoles) and X (for the sextupoles), while the best estimate for the orientation of the axis is given by the mechanical measurements. Combining the two kinds of measurements, the final settings of the first slit (SlitA), corresponding to the horizontal alignment of the sphere centers on the ideal beam trajectory, are obtained by summing for each magnet the value of ShiftXC in Tables IX and X to the values of XAmec in Tables VII (for the quadrupoles) and II (for the sextupoles). For the second slit (SlitB), due to the opposite direction of the micrometric movements, ShiftXC must be subtracted from XBmec.

$$
\begin{array}{r}
\text { SlitA }=\text { XAmec }+ \text { ShiftXC } \\
\text { SlitB }=\text { XBmec }- \text { ShiftXC }
\end{array}
$$

For the vertical plane we indicate with HeightA and HeightB the vertical distances from the ideal beamline at which the centers of the spheres must be set to properly align the magnets. These values are obtained by summing for each magnet the values of ShiftY in Tables IX and X to the values of YAmec and YBmec in Tables VII and II. The results are summarized in Table XI for the quadrupoles and XII for the sextupoles.

$$
\begin{aligned}
& \text { HeightA }=\text { YAmec }+ \text { ShiftY } \\
& \text { HeightB }=\text { YBmec }+ \text { ShiftY }
\end{aligned}
$$

## 6b) Alignment with compensation of the magnet rotation

Obviously, a method of aligning the magnets taking into account the rotation of the magnets is to set them as described in 4a) and then perform an azimuthal rotation of the magnet by the angle $\Phi$ indicated in Tables XIII (after the coil recalibration) and XIV, keeping the position of the longitudinal axis fixed. However, this method may be rather unpractical in real life.

An alternative method is to perform, as a preliminary adjustment, an azimuthal rotation by the angle $\Phi$ with respect to the ideal horizontal plane of the ring, and then to adjust the positions of the sphere centers to the values indicated in Tables XIII (for the quadrupoles) and XIV (for the sextupoles). The values in this table must take into account the recalibration of the coil. We have therefore:

$$
\begin{aligned}
& \text { SlitA }=\text { XAmec }+ \text { ShiftX }-0.35 x \Delta \Phi \\
& \text { SlitB }=\text { XBmec }- \text { ShiftX }+0.35 x \Delta \Phi
\end{aligned}
$$

Of course, $\Delta \Phi$ is zero for the sextupoles. For the vertical plane, HeightA and HeightB are obtained exactly as described in 4 a ). When the sign of the rotation is positive the magnet, observed from the elctrical and cooling connections side, must be rotated counterclockwise.

## References

[1] B. Bolli, F. Iungo, F. Losciale, N. Ganlin, M. Preger, C. Sanelli, F. Sardone "Field quality of the small quadrupoles for the DAФNE Main Rings" - DAФNE Technical Note MM-10 (22/2/96).
[2] B. Bolli, F. Iungo, F. Losciale, N. Ganlin, M. Preger, C. Sanelli, F. Sardone "Field quality of the small sextupoles for the DAФNE Main Rings" - DAФNE Technical Note MM-11 (6/3/96).
[3] F. Iungo, M. Modena, Q. Qiao, C. Sanelli "DAФNE magnetic measurement systems" DAФNE Technical Note MM-1 (2/12/94).
[4] B. Bolli, F. Iungo, F. Losciale, M. Paris, M. Preger, C. Sanelli, F. Sardone, F. Sgamma, M. Troiani "Field quality and alignment of the DAФNE Accumulator quadrupoles" - DAФNE Technical Note MM-8 (21/8/95).
[5] DAФNE Technical Note, to be published.

Table I - Magnetic center position of the 60 quadrupoles (alignment table Q3)

| Serial \# | XA mag | XB mag | YA mag | YB mag | $\Phi$ (mrad) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 13.120 | 11.620 | 350.250 | 350.320 | 0.730 |
| 2 | 13.130 | 11.630 | 350.220 | 350.320 | 0.700 |
| 3 | 13.390 | 11.750 | 350.250 | 350.330 | 0.940 |
| 4 | 12.970 | 11.770 | 350.260 | 350.300 | 0.530 |
| 5 | 12.920 | 11.740 | 350.220 | 350.280 | 0.310 |
| 6 | 12.900 | 11.430 | 350.240 | 350.300 | 0.560 |
| 7 | 13.350 | 12.320 | 350.220 | 350.240 | 0.210 |
| 8 | 13.100 | 11.770 | 350.200 | 350.270 | 0.710 |
| 9 | 12.740 | 12.090 | 350.230 | 350.280 | 0.530 |
| 10 | 13.360 | 11.980 | 350.180 | 350.240 | 0.770 |
| 11 | 12.740 | 11.560 | 350.210 | 350.280 | 0.350 |
| 12 | 12.990 | 11.930 | 350.190 | 350.260 | 0.790 |
| 13 | 13.290 | 11.700 | 350.210 | 350.280 | 0.840 |
| 14 | 13.020 | 11.830 | 350.210 | 350.270 | 0.600 |
| 15 | 12.850 | 11.600 | 350.210 | 350.270 | 0.680 |
| 16 | 12.480 | 11.270 | 350.180 | 350.260 | 0.660 |
| 17 | 13.180 | 11.910 | 350.280 | 350.350 | 0.350 |
| 18 | 13.860 | 12.410 | 350.380 | 350.440 | 1.890 |
| 19 | 12.900 | 11.520 | 350.210 | 350.290 | 0.590 |
| 20 | 12.720 | 10.880 | 350.190 | 350.270 | 1.150 |
| 21 | 12.790 | 11.540 | 350.280 | 350.340 | 0.780 |
| 22 | 12.370 | 10.980 | 350.250 | 350.320 | 0.880 |
| 23 | 12.230 | 10.710 | 350.210 | 350.260 | 1.040 |
| 24 | 12.160 | 10.850 | 350.210 | 350.270 | 0.460 |
| 25 | 13.120 | 11.190 | 350.210 | 350.280 | 1.270 |
| 26 | 12.730 | 11.070 | 350.280 | 350.230 | 1.010 |
| 27 | 12.730 | 11.200 | 350.280 | 350.350 | 0.370 |
| 28 | 12.720 | 11.040 | 350.210 | 350.260 | 0.960 |
| 29 | 12.820 | 11.180 | 350.200 | 350.260 | 1.020 |
| 30 | 12.980 | 11.760 | 350.250 | 350.300 | 0.790 |
| 31 | 12.430 | 11.010 | 350.230 | 350.300 | 0.880 |
| 32 | 12.940 | 11.430 | 350.210 | 350.270 | 0.980 |
| 33 | 12.280 | 11.390 | 350.190 | 350.250 | 0.840 |
| 34 | 13.080 | 11.425 | 350.190 | 350.240 | 0.880 |
| 35 | 12.850 | 11.345 | 350.170 | 350.230 | 0.880 |
| 36 | 12.730 | 11.210 | 350.200 | 350.250 | 0.520 |
| 37 | 13.520 | 12.015 | 350.180 | 350.250 | 1.000 |
| 38 | 12.955 | 11.600 | 350.200 | 350.260 | 0.430 |
| 39 | 12.520 | 11.215 | 350.170 | 350.220 | 0.170 |
| 40 | 12.915 | 11.680 | 350.170 | 350.240 | 0.370 |

Table I (continued)

| Serial \# | XA mag | XB mag | YA mag | YB mag | $\Phi(\mathbf{m r a d})$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 41 | 13.080 | 11.705 | 350.170 | 350.230 | 0.650 |
| 42 | 12.715 | 11.690 | 350.200 | 350.260 | 0.350 |
| 43 | 12.495 | 11.125 | 350.190 | 350.220 | 0.830 |
| 44 | 12.935 | 11.335 | 350.420 | 350.480 | 2.060 |
| 45 | 12.380 | 10.955 | 350.200 | 350.260 | 0.690 |
| 46 | 12.825 | 11.430 | 350.170 | 350.260 | 0.850 |
| 47 | 12.665 | 11.525 | 350.220 | 350.290 | 0.440 |
| 48 | 12.695 | 11.480 | 350.220 | 350.280 | 0.790 |
| 49 | 13.065 | 11.595 | 350.190 | 350.260 | 0.810 |
| 50 | 13.020 | 11.510 | 350.200 | 350.270 | 0.890 |
| 51 | 13.925 | 12.260 | 350.210 | 350.280 | 0.890 |
| 52 | 13.485 | 11.955 | 350.250 | 350.330 | 0.740 |
| 53 | 12.900 | 11.395 | 350.240 | 350.300 | 0.850 |
| 54 | 12.910 | 11.310 | 350.200 | 350.260 | 0.480 |
| 55 | 12.560 | 10.960 | 350.290 | 350.350 | 1.530 |
| 56 | 12.375 | 10.865 | 350.170 | 350.240 | 0.710 |
| 57 | 12.760 | 11.565 | 350.310 | 350.380 | 0.150 |
| 58 | 12.765 | 11.545 | 350.180 | 350.240 | 0.780 |
| 59 | 12.925 | 11.470 | 350.210 | 350.290 | 0.780 |
| 60 | 13.040 | 11.470 | 350.250 | 350.330 | 1.010 |

Table II - Magnetic center position of the 14 sextupoles (alignment table S1)

| Serial \# | XA mag | XB mag | YA mag | YB mag | $\Phi(\mathbf{m r a d})$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 11.73 | 10.99 | 350.38 | 350.18 | 0.59 |
| 2 | 12.01 | 11.24 | 350.40 | 350.19 | 0.60 |
| 3 | 11.96 | 11.20 | 350.39 | 350.18 | 0.02 |
| 4 | 12.21 | 11.52 | 350.32 | 350.22 | 0.74 |
| 5 | 12.30 | 11.60 | 350.38 | 350.19 | 0.80 |
| 6 | 11.86 | 11.39 | 350.46 | 350.16 | 0.09 |
| 7 | 12.01 | 11.57 | 350.36 | 350.18 | 0.22 |
| 8 | 12.05 | 11.48 | 350.36 | 350.18 | 0.37 |
| 9 | 12.23 | 11.75 | 350.41 | 350.19 | 0.24 |
| 10 | 12.12 | 11.65 | 350.36 | 350.22 | 0.33 |
| 11 | 12.25 | 11.62 | 350.38 | 350.15 | 0.58 |
| 12 | 11.91 | 11.53 | 350.36 | 350.31 | 0.33 |
| 13 | 12.06 | 11.44 | 350.37 | 350.14 | 0.47 |
| 14 | 12.42 | 11.72 | 350.52 | 350.00 | 0.48 |

Table III- Mechanical center position of the 60 quadrupoles (alignment table Q1)

| Serial \# | XA mec | XB mec | YA mec | YB mec |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 12.40 | 12.75 | 350.49 | 350.52 |
| 2 | 12.44 | 12.68 | 350.46 | 350.49 |
| 3 | 12.42 | 12.62 | 350.44 | 350.41 |
| 4 | 12.55 | 12.79 | 350.46 | 350.44 |
| 5 | 12.42 | 12.78 | 350.48 | 350.43 |
| 6 | 12.35 | 12.77 | 350.50 | 350.43 |
| 7 | 12.25 | 12.81 | 350.46 | 350.36 |
| 8 | 12.33 | 12.77 | 350.47 | 350.41 |
| 9 | 12.10 | 12.96 | 350.47 | 350.38 |
| 10 | 12.42 | 12.62 | 350.43 | 350.35 |
| 11 | 12.00 | 12.98 | 350.53 | 350.58 |
| 12 | 12.07 | 13.05 | 350.47 | 350.40 |
| 13 | 12.49 | 12.61 | 350.37 | 350.46 |
| 14 | 12.35 | 12.81 | 350.49 | 350.39 |
| 15 | 12.39 | 12.79 | 350.39 | 350.34 |
| 16 | 12.32 | 12.87 | 350.39 | 350.34 |
| 17 | 12.51 | 12.76 | 350.68 | 350.38 |
| 18 | 11.80 | 13.40 | 350.58 | 350.63 |
| 19 | 12.37 | 12.63 | 350.44 | 350.34 |
| 20 | 12.33 | 12.66 | 350.41 | 350.39 |
| 21 | 12.22 | 12.83 | 350.43 | 350.41 |
| 22 | 12.16 | 12.87 | 350.48 | 350.42 |
| 23 | 12.24 | 12.83 | 350.43 | 350.36 |
| 24 | 12.29 | 12.70 | 350.47 | 350.34 |
| 25 | 12.33 | 12.74 | 350.46 | 350.40 |
| 26 | 12.31 | 12.79 | 350.44 | 350.44 |
| 27 | 12.31 | 12.79 | 350.50 | 350.46 |
| 28 | 12.48 | 12.63 | 350.47 | 350.42 |
| 29 | 12.35 | 12.70 | 350.46 | 350.38 |
| 30 | 12.37 | 12.83 | 350.46 | 350.38 |
| 31 | 12.33 | 12.79 | 350.44 | 350.38 |
| 32 | 12.24 | 12.74 | 350.46 | 350.34 |
| 33 | 12.21 | 12.80 | 350.46 | 350.37 |
| 34 | 12.38 | 12.93 | 350.48 | 350.42 |
| 35 | 12.26 | 12.79 | 350.46 | 350.41 |
| 36 | 12.37 | 12.78 | 350.43 | 350.37 |
| 37 | 12.13 | 12.88 | 350.52 | 350.46 |
| 38 | 12.39 | 12.70 | 350.42 | 350.38 |
| 39 | 12.34 | 12.71 | 350.45 | 350.38 |
| 40 | 12.23 | 12.85 | 350.43 | 350.36 |

Table III (continued)

| Serial \# | XA mec | XB mec | YA mec | YB mec |
| :---: | :---: | :---: | :---: | :---: |
| 41 | 12.42 | 12.82 | 350.44 | 350.41 |
| 42 | 12.06 | 13.00 | 350.50 | 350.43 |
| 43 | 12.14 | 12.98 | 350.46 | 350.37 |
| 44 | 12.27 | 13.08 | 350.66 | 350.57 |
| 45 | 12.42 | 12.69 | 350.40 | 350.32 |
| 46 | 12.16 | 12.92 | 350.49 | 350.40 |
| 47 | 12.17 | 12.86 | 350.54 | 350.47 |
| 48 | 12.17 | 12.95 | 350.54 | 350.51 |
| 49 | 12.41 | 12.70 | 350.40 | 350.37 |
| 50 | 12.43 | 12.69 | 350.39 | 350.34 |
| 51 | 12.01 | 13.15 | 350.57 | 350.54 |
| 52 | 12.32 | 12.62 | 350.52 | 350.35 |
| 53 | 12.37 | 12.79 | 350.39 | 350.38 |
| 54 | 12.46 | 12.83 | 350.42 | 350.36 |
| 55 | 11.80 | 12.87 | 350.60 | 350.53 |
| 56 | 12.36 | 12.77 | 350.43 | 350.34 |
| 57 | 12.28 | 13.02 | 350.55 | 350.48 |
| 58 | 12.26 | 12.85 | 350.42 | 350.39 |
| 59 | 12.42 | 12.88 | 350.45 | 350.33 |
| 60 | 12.35 | 12.62 | 350.42 | 350.40 |

Table IV - Mechanical center position of the 14 sextupoles (alignment table S1)

| Serial \# | XA mec | XB mec | YA mec | YB mec |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 12.13 | 12.23 | 350.30 | 350.32 |
| 2 | 12.30 | 11.65 | 350.38 | 350.18 |
| 3 | 12.24 | 11.97 | 350.32 | 350.22 |
| 4 | 12.04 | 12.09 | 350.33 | 350.31 |
| 5 | 12.47 | 11.67 | 350.29 | 350.22 |
| 6 | 12.08 | 12.08 | 350.34 | 350.24 |
| 7 | 12.11 | 11.87 | 350.37 | 350.19 |
| 8 | 12.03 | 11.99 | 350.31 | 350.19 |
| 9 | 12.05 | 11.91 | 350.35 | 350.27 |
| 10 | 11.90 | 12.11 | 350.36 | 350.21 |
| 11 | 12.00 | 12.19 | 350.38 | 350.26 |
| 12 | 12.29 | 11.91 | 350.29 | 350.17 |
| 13 | 12.35 | 11.93 | 350.29 | 350.20 |
| 14 | 12.43 | 11.73 | 350.29 | 350.21 |

Table V- Mechanical center position of the 60 quadrupoles (alignment table Q2)

| Serial \# | XA mec | XB mec | Y ${ }^{\text {mec }}$ | YB mec |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 12.27 | 11.97 | 350.52 | 350.57 |
| 2 | 12.31 | 11.90 | 350.49 | 350.54 |
| 3 | 12.29 | 11.84 | 350.47 | 350.46 |
| 4 | 12.42 | 12.01 | 350.49 | 350.49 |
| 5 | 12.29 | 12.00 | 350.51 | 350.48 |
| 6 | 12.22 | 11.99 | 350.53 | 350.48 |
| 7 | 12.12 | 12.03 | 350.49 | 350.41 |
| 8 | 12.20 | 11.99 | 350.50 | 350.46 |
| 9 | 11.97 | 12.18 | 350.50 | 350.43 |
| 10 | 12.29 | 11.84 | 350.46 | 350.40 |
| 11 | 11.87 | 12.20 | 350.56 | 350.63 |
| 12 | 11.94 | 12.27 | 350.50 | 350.45 |
| 13 | 12.36 | 11.83 | 350.40 | 350.51 |
| 14 | 12.22 | 12.03 | 350.52 | 350.44 |
| 15 | 12.26 | 12.01 | 350.42 | 350.39 |
| 16 | 12.19 | 12.09 | 350.42 | 350.39 |
| 17 | 12.38 | 11.98 | 350.71 | 350.43 |
| 18 | 11.67 | 12.62 | 350.61 | 350.68 |
| 19 | 12.24 | 11.85 | 350.47 | 350.39 |
| 20 | 12.20 | 11.88 | 350.44 | 350.44 |
| 21 | 12.09 | 12.05 | 350.46 | 350.46 |
| 22 | 12.03 | 12.09 | 350.51 | 350.47 |
| 23 | 12.11 | 12.05 | 350.46 | 350.41 |
| 24 | 12.16 | 11.92 | 350.50 | 350.39 |
| 25 | 12.20 | 11.96 | 350.49 | 350.45 |
| 26 | 12.18 | 12.01 | 350.47 | 350.49 |
| 27 | 12.18 | 12.01 | 350.53 | 350.51 |
| 28 | 12.35 | 11.85 | 350.50 | 350.47 |
| 29 | 12.22 | 11.92 | 350.49 | 350.43 |
| 30 | 12.24 | 12.05 | 350.49 | 350.43 |
| 31 | 12.20 | 12.01 | 350.46 | 350.40 |
| 32 | 12.11 | 11.96 | 350.48 | 350.36 |
| 33 | 12.08 | 12.02 | 350.48 | 350.39 |
| 34 | 12.25 | 12.15 | 350.50 | 350.44 |
| 35 | 12.13 | 12.01 | 350.48 | 350.43 |
| 36 | 12.24 | 12.00 | 350.45 | 350.39 |
| 37 | 12.00 | 12.10 | 350.54 | 350.48 |
| 38 | 12.26 | 11.92 | 350.44 | 350.40 |
| 39 | 12.21 | 11.93 | 350.47 | 350.40 |
| 40 | 12.10 | 12.07 | 350.45 | 350.38 |

Table V (continued)

| Serial \# | XA mec | XB mec | YA mec | YB mec |
| :---: | :---: | :---: | :---: | :---: |
| 41 | 12.29 | 12.04 | 350.46 | 350.43 |
| 42 | 11.93 | 12.22 | 350.52 | 350.45 |
| 43 | 12.01 | 12.20 | 350.48 | 350.39 |
| 44 | 12.14 | 12.30 | 350.68 | 350.59 |
| 45 | 12.29 | 11.91 | 350.42 | 350.34 |
| 46 | 12.03 | 12.14 | 350.51 | 350.42 |
| 47 | 12.04 | 12.08 | 350.56 | 350.49 |
| 48 | 12.04 | 12.17 | 350.56 | 350.53 |
| 49 | 12.28 | 11.92 | 350.42 | 350.39 |
| 50 | 12.30 | 11.91 | 350.41 | 350.36 |
| 51 | 11.88 | 12.37 | 350.59 | 350.56 |
| 52 | 12.19 | 11.84 | 350.54 | 350.37 |
| 53 | 12.24 | 12.01 | 350.41 | 350.40 |
| 54 | 12.33 | 12.05 | 350.44 | 350.38 |
| 55 | 11.67 | 12.09 | 350.62 | 350.55 |
| 56 | 12.23 | 11.99 | 350.45 | 350.36 |
| 57 | 12.15 | 12.24 | 350.57 | 350.50 |
| 58 | 12.13 | 12.07 | 350.44 | 350.41 |
| 59 | 12.29 | 12.10 | 350.47 | 350.35 |
| 60 | 12.22 | 11.84 | 350.44 | 350.42 |

Table VI - Mechanical center position of the 14 sextupoles (alignment table S2)

| Serial \# | XA mec | XB mec | YA mec | YB mec |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 11.80 | 11.92 | 350.40 | 350.30 |
| 2 | 11.97 | 11.34 | 350.48 | 350.16 |
| 3 | 11.91 | 11.66 | 350.42 | 350.20 |
| 4 | 11.71 | 11.78 | 350.43 | 350.29 |
| 5 | 12.14 | 11.36 | 350.39 | 350.20 |
| 6 | 11.75 | 11.77 | 350.44 | 350.22 |
| 7 | 11.78 | 11.56 | 350.47 | 350.17 |
| 8 | 11.70 | 11.68 | 350.41 | 350.70 |
| 9 | 11.72 | 11.60 | 350.45 | 350.25 |
| 10 | 11.57 | 11.80 | 350.46 | 350.19 |
| 11 | 11.67 | 11.88 | 350.48 | 350.24 |
| 12 | 11.96 | 11.60 | 350.39 | 350.15 |
| 13 | 12.02 | 11.62 | 350.39 | 350.18 |
| 14 | 12.10 | 11.42 | 350.39 | 350.19 |

Table VII- Mechanical center position of the 60 quadrupoles (alignment table Q3)

| Serial \# | XA mec | XB mec | YA mec | YB mec |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 12.82 | 11.89 | 350.38 | 350.50 |
| 2 | 12.86 | 11.82 | 350.35 | 350.47 |
| 3 | 12.84 | 11.76 | 350.33 | 350.39 |
| 4 | 12.97 | 11.93 | 350.35 | 350.42 |
| 5 | 12.84 | 11.92 | 350.37 | 350.41 |
| 6 | 12.77 | 11.91 | 350.39 | 350.41 |
| 7 | 12.67 | 11.95 | 350.35 | 350.34 |
| 8 | 12.75 | 11.91 | 350.36 | 350.39 |
| 9 | 12.52 | 12.10 | 350.36 | 350.36 |
| 10 | 12.84 | 11.76 | 350.32 | 350.33 |
| 11 | 12.42 | 12.12 | 350.42 | 350.56 |
| 12 | 12.49 | 12.19 | 350.36 | 350.38 |
| 13 | 12.91 | 11.75 | 350.26 | 350.44 |
| 14 | 12.77 | 11.95 | 350.38 | 350.37 |
| 15 | 12.81 | 11.93 | 350.28 | 350.32 |
| 16 | 12.74 | 12.01 | 350.28 | 350.32 |
| 17 | 12.93 | 11.90 | 350.57 | 350.36 |
| 18 | 12.22 | 12.54 | 350.47 | 350.61 |
| 19 | 12.79 | 11.77 | 350.33 | 350.32 |
| 20 | 12.75 | 11.80 | 350.30 | 350.37 |
| 21 | 12.64 | 11.97 | 350.32 | 350.39 |
| 22 | 12.58 | 12.01 | 350.37 | 350.40 |
| 23 | 12.66 | 11.97 | 350.32 | 350.34 |
| 24 | 12.71 | 11.84 | 350.36 | 350.32 |
| 25 | 12.75 | 11.88 | 350.35 | 350.38 |
| 26 | 12.73 | 11.93 | 350.33 | 350.42 |
| 27 | 12.73 | 11.93 | 350.39 | 350.44 |
| 28 | 12.90 | 11.77 | 350.36 | 350.40 |
| 29 | 12.77 | 11.84 | 350.35 | 350.36 |
| 30 | 12.79 | 11.97 | 350.35 | 350.36 |
| 31 | 12.75 | 11.93 | 350.33 | 350.36 |
| 32 | 12.66 | 11.88 | 350.35 | 350.32 |
| 33 | 12.63 | 11.94 | 350.35 | 350.35 |
| 34 | 12.80 | 12.07 | 350.37 | 350.40 |
| 35 | 12.68 | 11.93 | 350.35 | 350.39 |
| 36 | 12.79 | 11.92 | 350.32 | 350.35 |
| 37 | 12.55 | 12.02 | 350.41 | 350.44 |
| 38 | 12.81 | 11.84 | 350.31 | 350.36 |
| 39 | 12.76 | 11.85 | 350.34 | 350.36 |
| 40 | 12.65 | 11.99 | 350.32 | 350.34 |

Table VII (continued)

| Serial \# | XA mec | XB mec | YA mec | YB mec |
| :---: | :---: | :---: | :---: | :---: |
| 41 | 12.84 | 11.96 | 350.33 | 350.39 |
| 42 | 12.48 | 12.14 | 350.39 | 350.41 |
| 43 | 12.56 | 12.12 | 350.35 | 350.35 |
| 44 | 12.69 | 12.22 | 350.55 | 350.55 |
| 45 | 12.84 | 11.83 | 350.29 | 350.30 |
| 46 | 12.58 | 12.06 | 350.38 | 350.38 |
| 47 | 12.59 | 12.00 | 350.43 | 350.45 |
| 48 | 12.59 | 12.09 | 350.43 | 350.49 |
| 49 | 12.83 | 11.84 | 350.29 | 350.35 |
| 50 | 12.85 | 11.83 | 350.28 | 350.32 |
| 51 | 12.43 | 12.29 | 350.46 | 350.52 |
| 52 | 12.74 | 11.76 | 350.41 | 350.33 |
| 53 | 12.79 | 11.93 | 350.28 | 350.36 |
| 54 | 12.88 | 11.97 | 350.31 | 350.34 |
| 55 | 12.22 | 12.01 | 350.49 | 350.51 |
| 56 | 12.78 | 11.91 | 350.32 | 350.32 |
| 57 | 12.70 | 12.16 | 350.44 | 350.46 |
| 58 | 12.68 | 11.99 | 350.31 | 350.37 |
| 59 | 12.84 | 12.02 | 350.34 | 350.31 |
| 60 | 12.77 | 11.76 | 350.31 | 350.38 |

Table VIII - Mechanical center position of the 14 sextupoles (alignment table S3)

| Serial \# | XA mec | XB mec | YA mec | YB mec |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 12.74 | 12.48 | 350.31 | 350.40 |
| 2 | 12.91 | 11.90 | 350.39 | 350.26 |
| 3 | 12.85 | 12.22 | 350.33 | 350.30 |
| 4 | 12.65 | 12.34 | 350.34 | 350.39 |
| 5 | 13.08 | 11.92 | 350.30 | 350.30 |
| 6 | 12.69 | 12.33 | 350.35 | 350.32 |
| 7 | 12.72 | 12.12 | 350.38 | 350.27 |
| 8 | 12.64 | 12.24 | 350.32 | 350.27 |
| 9 | 12.66 | 12.16 | 350.36 | 350.35 |
| 10 | 12.51 | 12.36 | 350.37 | 350.29 |
| 11 | 12.61 | 12.44 | 350.39 | 350.34 |
| 12 | 12.90 | 12.16 | 350.30 | 350.25 |
| 13 | 12.96 | 12.18 | 350.30 | 350.28 |
| 14 | 13.04 | 11.98 | 350.30 | 350.29 |

Table IX - Distance (mm) and tilt (mrad) between magnetic and mechanical axes for the quadrupoles

| Serial \# | Shift X | Shift Y | Tilt X | Tilt Y | Shift XC |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.29 | -0.15 | 0.18 | 0.29 | 0.03 |
| 2 | 0.23 | -0.14 | 0.47 | 0.12 | -0.01 |
| 3 | 0.28 | -0.07 | 3.18 | -0.12 | -0.05 |
| 4 | 0.08 | -0.11 | -0.94 | 0.18 | -0.11 |
| 5 | 0.13 | -0.14 | -0.59 | -0.12 | 0.02 |
| 6 | 0.30 | -0.13 | -2.06 | -0.24 | 0.11 |
| 7 | 0.16 | -0.12 | 6.18 | -0.18 | 0.08 |
| 8 | 0.24 | -0.14 | 1.24 | -0.23 | -0.00 |
| 9 | 0.11 | -0.10 | 1.24 | -0.29 | -0.07 |
| 10 | 0.15 | -0.12 | 4.35 | -0.29 | -0.12 |
| 11 | 0.44 | -0.25 | -1.41 | 0.41 | 0.32 |
| 12 | 0.38 | -0.14 | 1.41 | -0.29 | 0.10 |
| 13 | 0.22 | -0.11 | 1.94 | 0.65 | -0.08 |
| 14 | 0.18 | -0.14 | 0.76 | -0.41 | -0.03 |
| 15 | 0.18 | -0.06 | -1.71 | -0.12 | -0.05 |
| 16 | 0.24 | -0.08 | -5.88 | -0.24 | 0.01 |
| 17 | 0.12 | -0.15 | 1.53 | -1.65 | -0.00 |
| 18 | 0.88 | -0.13 | 8.88 | 0.47 | 0.22 |
| 19 | 0.18 | -0.07 | -0.82 | -0.53 | -0.03 |
| 20 | 0.45 | -0.10 | -5.59 | -0.06 | 0.04 |
| 21 | 0.29 | -0.05 | -1.65 | 0.06 | 0.02 |
| 22 | 0.41 | -0.10 | -7.29 | -0.24 | 0.10 |
| 23 | 0.41 | -0.10 | -9.94 | -0.18 | 0.05 |
| 24 | 0.22 | -0.10 | -9.06 | -0.59 | 0.06 |
| 25 | 0.53 | -0.12 | -1.88 | -0.24 | 0.09 |
| 26 | 0.43 | -0.12 | -5.06 | 0.82 | 0.08 |
| 27 | 0.37 | -0.10 | -4.29 | -0.12 | 0.24 |
| 28 | 0.28 | -0.14 | -5.35 | -0.06 | -0.06 |
| 29 | 0.35 | -0.12 | -3.59 | -0.29 | -0.00 |
| 30 | 0.20 | -0.08 | -0.12 | -0.24 | -0.08 |
| 31 | 0.30 | -0.08 | -7.29 | -0.24 | -0.01 |
| 32 | 0.36 | -0.10 | -1.00 | -0.53 | 0.02 |
| 33 | 0.10 | -0.13 | -5.29 | -0.35 | -0.19 |
| 34 | 0.46 | -0.17 | -2.15 | -0.12 | 0.15 |
| 35 | 0.38 | -0.17 | -2.44 | -0.12 | 0.07 |
| 36 | 0.32 | -0.11 | -4.53 | -0.12 | 0.14 |
| 37 | 0.49 | -0.21 | 5.68 | -0.24 | 0.14 |
| 38 | 0.19 | -0.10 | -0.56 | -0.06 | 0.04 |
| 39 | 0.20 | -0.15 | -5.15 | -0.18 | 0.14 |
| 40 | 0.29 | -0.13 | -0.26 | -0.29 | 0.16 |

Table IX (continued)

| Serial \# | Shift X | Shift Y | Tilt X | Tilt Y | Shift XC |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 41 | 0.25 | -0.16 | -0.09 | 0.00 | 0.02 |
| 42 | 0.34 | -0.17 | -1.26 | -0.24 | 0.22 |
| 43 | 0.46 | -0.15 | -6.24 | -0.18 | 0.17 |
| 44 | 0.57 | -0.10 | -3.76 | -0.35 | -0.16 |
| 45 | 0.21 | -0.06 | -7.85 | -0.29 | -0.03 |
| 46 | 0.44 | -0.16 | -2.26 | -0.53 | 0.14 |
| 47 | 0.28 | -0.18 | -2.35 | -0.29 | 0.12 |
| 48 | 0.36 | -0.21 | -2.97 | 0.00 | 0.08 |
| 49 | 0.24 | -0.10 | -0.06 | -0.06 | -0.04 |
| 50 | 0.24 | -0.07 | -0.88 | -0.18 | -0.07 |
| 51 | 0.76 | -0.24 | 8.62 | -0.06 | 0.45 |
| 52 | 0.28 | -0.08 | 5.53 | -0.94 | 0.02 |
| 53 | 0.32 | -0.05 | -2.50 | 0.12 | 0.02 |
| 54 | 0.34 | -0.09 | -3.71 | -0.18 | 0.18 |
| 55 | 0.70 | -0.18 | -4.18 | -0.24 | 0.16 |
| 56 | 0.32 | -0.12 | -8.53 | -0.41 | 0.07 |
| 57 | 0.33 | -0.10 | -3.15 | -0.29 | 0.28 |
| 58 | 0.26 | -0.13 | -2.12 | 0.00 | -0.01 |
| 59 | 0.32 | -0.07 | -2.74 | -0.65 | 0.04 |
| 60 | 0.28 | -0.06 | -0.12 | -0.06 | -0.07 |

Table X - Distance (mm) and tilt (mrad) between magnetic and mechanical axes for the sextupoles

| Serial \# | Shift X | Shift Y | Tilt X | Tilt Y | Shift XC |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.42 | -0.03 | -16.40 | 2.20 | 0.21 |
| 2 | 0.06 | 0.01 | -7.00 | 0.10 | -0.15 |
| 3 | 0.25 | 0.01 | -10.50 | 1.10 | 0.24 |
| 4 | 0.37 | -0.05 | -4.00 | 0.80 | 0.11 |
| 5 | -0.05 | 0.03 | -2.40 | 1.20 | -0.33 |
| 6 | 0.23 | 0.02 | -9.10 | 2.00 | 0.20 |
| 7 | 0.10 | -0.01 | -4.00 | 0.00 | 0.02 |
| 8 | 0.27 | 0.02 | -4.90 | 0.60 | 0.14 |
| 9 | 0.17 | -0.01 | 0.20 | 1.40 | 0.09 |
| 10 | 0.34 | 0.01 | -2.40 | -0.10 | 0.22 |
| 11 | 0.41 | -0.06 | -3.20 | 1.10 | 0.21 |
| 12 | 0.00 | 0.10 | -7.60 | -0.70 | -0.12 |
| 13 | 0.10 | 0.01 | -7.80 | 1.40 | -0.06 |
| 14 | -0.00 | 0.01 | -0.20 | 4.36 | -0.17 |

Table XI - Alignment values without compensation of azimuthal rotation for the 60 quadrupoles of the DAФNE Main Rings (Method 4a)

| Serial\# | Slit A | Slit B | Height A | Height B |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 12.85 | 11.86 | 350.23 | 350.35 |
| 2 | 12.84 | 11.84 | 350.21 | 350.33 |
| 3 | 12.79 | 11.81 | 350.26 | 350.32 |
| 4 | 12.86 | 12.04 | 350.24 | 350.32 |
| 5 | 12.86 | 11.90 | 350.23 | 350.27 |
| 6 | 12.88 | 11.80 | 350.26 | 350.28 |
| 7 | 12.75 | 11.87 | 350.23 | 350.22 |
| 8 | 12.75 | 11.91 | 350.22 | 350.25 |
| 9 | 12.45 | 12.17 | 350.26 | 350.26 |
| 10 | 12.72 | 11.88 | 350.21 | 350.21 |
| 11 | 12.74 | 11.80 | 350.17 | 350.32 |
| 12 | 12.59 | 12.09 | 350.21 | 350.24 |
| 13 | 12.83 | 11.83 | 350.15 | 350.33 |
| 14 | 12.75 | 11.97 | 350.24 | 350.23 |
| 15 | 12.76 | 11.98 | 350.22 | 350.26 |
| 16 | 12.75 | 12.00 | 350.20 | 350.24 |
| 17 | 12.93 | 11.90 | 350.42 | 350.21 |
| 18 | 12.44 | 12.32 | 350.34 | 350.48 |
| 19 | 12.76 | 11.80 | 350.26 | 350.24 |
| 20 | 12.79 | 11.76 | 350.20 | 350.27 |
| 21 | 12.66 | 11.95 | 350.27 | 350.35 |
| 22 | 12.68 | 11.91 | 350.27 | 350.30 |
| 23 | 12.71 | 11.92 | 350.23 | 350.24 |
| 24 | 12.77 | 11.78 | 350.26 | 350.22 |
| 25 | 12.84 | 11.79 | 350.23 | 350.26 |
| 26 | 12.81 | 11.85 | 350.21 | 350.30 |
| 27 | 12.97 | 11.69 | 350.29 | 350.34 |
| 28 | 12.84 | 11.83 | 350.21 | 350.26 |
| 29 | 12.77 | 11.84 | 350.23 | 350.23 |
| 30 | 12.71 | 12.05 | 350.27 | 350.28 |
| 31 | 12.74 | 11.94 | 350.25 | 350.28 |
| 32 | 12.68 | 11.86 | 350.26 | 350.22 |
| 33 | 12.44 | 12.13 | 350.22 | 350.22 |
| 34 | 12.95 | 11.92 | 350.20 | 350.23 |
| 35 | 12.75 | 11.86 | 350.18 | 350.22 |
| 36 | 12.93 | 11.78 | 350.21 | 350.24 |
| 37 | 12.69 | 11.88 | 350.20 | 350.23 |
| 38 | 12.85 | 11.80 | 350.21 | 350.26 |
| 39 | 12.90 | 11.71 | 350.18 | 350.21 |
| 40 | 12.81 | 11.83 | 350.20 | 350.21 |

Table XI (continued)

| Serial \# | Slit A | Slit B | Height A | Height B |
| :---: | :---: | :---: | :---: | :---: |
| 41 | 12.86 | 11.94 | 350.17 | 350.23 |
| 42 | 12.70 | 11.92 | 350.22 | 350.24 |
| 43 | 12.73 | 11.95 | 350.21 | 350.21 |
| 44 | 12.53 | 12.38 | 350.45 | 350.45 |
| 45 | 12.81 | 11.86 | 350.23 | 350.23 |
| 46 | 12.72 | 11.92 | 350.22 | 350.22 |
| 47 | 12.71 | 11.88 | 350.24 | 350.27 |
| 48 | 12.67 | 12.01 | 350.22 | 350.28 |
| 49 | 12.79 | 11.88 | 350.20 | 350.26 |
| 50 | 12.78 | 11.90 | 350.21 | 350.26 |
| 51 | 12.88 | 11.84 | 350.21 | 350.27 |
| 52 | 12.76 | 11.74 | 350.33 | 350.25 |
| 53 | 12.81 | 11.91 | 350.23 | 350.31 |
| 54 | 13.06 | 11.79 | 350.22 | 350.24 |
| 55 | 12.38 | 11.85 | 350.31 | 350.33 |
| 56 | 12.85 | 11.84 | 350.21 | 350.21 |
| 57 | 12.98 | 11.88 | 350.34 | 350.35 |
| 58 | 12.67 | 12.00 | 350.18 | 350.24 |
| 59 | 12.88 | 11.98 | 350.27 | 350.23 |
| 60 | 12.70 | 11.83 | 350.26 | 350.33 |

Table XII - Alignment values without compensation of azimuthal rotation for the 14 sextupoles of the DAФNE Main Rings (Method 4a)

| Serial \# | Slit A | Slit B | Height A | Height B |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 12.34 | 12.02 | 350.27 | 350.29 |
| 2 | 12.15 | 11.80 | 350.40 | 350.20 |
| 3 | 12.48 | 11.73 | 350.34 | 350.23 |
| 4 | 12.15 | 11.98 | 350.28 | 350.26 |
| 5 | 12.14 | 12.00 | 350.32 | 350.25 |
| 6 | 12.28 | 11.88 | 350.36 | 350.26 |
| 7 | 12.13 | 11.85 | 350.36 | 350.18 |
| 8 | 12.17 | 11.85 | 350.33 | 350.21 |
| 9 | 12.14 | 11.82 | 350.34 | 350.26 |
| 10 | 12.12 | 11.89 | 350.36 | 350.21 |
| 11 | 12.21 | 11.98 | 350.33 | 350.21 |
| 12 | 12.17 | 12.03 | 350.39 | 350.27 |
| 13 | 12.29 | 11.99 | 350.30 | 350.21 |
| 14 | 12.26 | 11.90 | 350.30 | 350.22 |

Table XIII - Alignment values with compensation of azimuthal rotation for the 60 quadrupoles of the DAФNE Main Rings (Method 4b)

| Serial \# | $\Phi$ (mrad) | Slit A | Slit B | Height A | Height B |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.030 | 12.86 | 11.85 | 350.23 | 350.35 |
| 2 | -0.000 | 12.84 | 11.84 | 350.21 | 350.33 |
| 3 | 0.240 | 12.88 | 11.73 | 350.26 | 350.32 |
| 4 | -0.170 | 12.81 | 12.10 | 350.24 | 350.32 |
| 5 | -0.390 | 12.73 | 12.03 | 350.23 | 350.27 |
| 6 | -0.140 | 12.83 | 11.85 | 350.26 | 350.28 |
| 7 | -0.490 | 12.58 | 12.04 | 350.23 | 350.22 |
| 8 | 0.010 | 12.75 | 11.91 | 350.22 | 350.25 |
| 9 | -0.170 | 12.39 | 12.23 | 350.26 | 350.26 |
| 10 | 0.070 | 12.74 | 11.86 | 350.21 | 350.21 |
| 11 | -0.350 | 12.61 | 11.93 | 350.17 | 350.32 |
| 12 | 0.090 | 12.62 | 12.06 | 350.21 | 350.24 |
| 13 | 0.140 | 12.88 | 11.78 | 350.15 | 350.33 |
| 14 | -0.100 | 12.71 | 12.01 | 350.24 | 350.23 |
| 15 | -0.020 | 12.75 | 11.99 | 350.22 | 350.26 |
| 16 | -0.040 | 12.73 | 12.02 | 350.20 | 350.24 |
| 17 | -0.350 | 12.81 | 12.02 | 350.42 | 350.21 |
| 18 | 1.190 | 12.86 | 11.90 | 350.34 | 350.48 |
| 19 | -0.110 | 12.72 | 11.84 | 350.26 | 350.24 |
| 20 | 0.450 | 12.95 | 11.60 | 350.20 | 350.27 |
| 21 | 0.080 | 12.69 | 11.93 | 350.27 | 350.35 |
| 22 | 0.180 | 12.74 | 11.85 | 350.27 | 350.30 |
| 23 | 0.340 | 12.83 | 11.80 | 350.23 | 350.24 |
| 24 | -0.240 | 12.68 | 11.87 | 350.26 | 350.22 |
| 25 | 0.570 | 13.03 | 11.60 | 350.23 | 350.26 |
| 26 | 0.310 | 12.91 | 11.74 | 350.21 | 350.30 |
| 27 | -0.330 | 12.85 | 11.81 | 350.29 | 350.34 |
| 28 | 0.260 | 12.93 | 11.74 | 350.21 | 350.26 |
| 29 | 0.320 | 12.88 | 11.73 | 350.23 | 350.23 |
| 30 | 0.090 | 12.74 | 12.02 | 350.27 | 350.28 |
| 31 | 0.180 | 12.81 | 11.87 | 350.25 | 350.28 |
| 32 | 0.280 | 12.78 | 11.76 | 350.26 | 350.22 |
| 33 | 0.140 | 12.48 | 12.09 | 350.22 | 350.22 |
| 34 | 0.180 | 13.02 | 11.85 | 350.20 | 350.23 |
| 35 | 0.180 | 12.81 | 11.80 | 350.18 | 350.22 |
| 36 | -0.180 | 12.87 | 11.84 | 350.21 | 350.24 |
| 37 | 0.300 | 12.79 | 11.78 | 350.20 | 350.23 |
| 38 | -0.270 | 12.76 | 11.89 | 350.21 | 350.26 |
| 39 | -0.530 | 12.71 | 11.90 | 350.18 | 350.21 |
| 40 | -0.330 | 12.69 | 11.95 | 350.20 | 350.21 |

Table XIII (continued)

| Serial \# | $\Phi$ (mrad) | Slit A | Slit B | Height A | Height B |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 41 | -0.050 | 12.84 | 11.96 | 350.17 | 350.23 |
| 42 | -0.350 | 12.58 | 12.04 | 350.22 | 350.24 |
| 43 | 0.130 | 12.78 | 11.90 | 350.21 | 350.21 |
| 44 | 1.360 | 13.01 | 11.90 | 350.45 | 350.45 |
| 45 | -0.010 | 12.80 | 11.87 | 350.23 | 350.23 |
| 46 | 0.150 | 12.77 | 11.87 | 350.22 | 350.22 |
| 47 | -0.260 | 12.62 | 11.97 | 350.24 | 350.27 |
| 48 | 0.090 | 12.70 | 11.98 | 350.22 | 350.28 |
| 49 | 0.110 | 12.82 | 11.85 | 350.20 | 350.26 |
| 50 | 0.190 | 12.85 | 11.83 | 350.21 | 350.26 |
| 51 | 0.190 | 12.95 | 11.77 | 350.21 | 350.27 |
| 52 | 0.040 | 12.77 | 11.73 | 350.33 | 350.25 |
| 53 | 0.150 | 12.87 | 11.85 | 350.23 | 350.31 |
| 54 | -0.220 | 12.98 | 11.87 | 350.22 | 350.24 |
| 55 | 0.830 | 12.67 | 11.56 | 350.31 | 350.33 |
| 56 | 0.010 | 12.85 | 11.84 | 350.21 | 350.21 |
| 57 | -0.550 | 12.78 | 12.08 | 350.34 | 350.35 |
| 58 | 0.080 | 12.70 | 11.97 | 350.18 | 350.24 |
| 59 | 0.080 | 12.91 | 11.95 | 350.27 | 350.23 |
| 60 | 0.310 | 12.81 | 11.73 | 350.26 | 350.33 |

Table XIV - Alignment values with compensation of azimuthal rotation for the 14 sextupoles of the DAФNE Main Rings (Method 4b)

| Serial \# | $\Phi(\mathbf{m r a d})$ | Slit A | Slit B | Height A | Height B |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.59 | 12.55 | 11.81 | 350.27 | 350.29 |
| 2 | 0.60 | 12.36 | 11.59 | 350.40 | 350.20 |
| 3 | 0.02 | 12.49 | 11.73 | 350.34 | 350.23 |
| 4 | 0.74 | 12.41 | 11.72 | 350.28 | 350.26 |
| 5 | 0.80 | 12.42 | 11.72 | 350.32 | 350.25 |
| 6 | 0.09 | 12.31 | 11.85 | 350.36 | 350.26 |
| 7 | 0.22 | 12.21 | 11.77 | 350.36 | 350.18 |
| 8 | 0.37 | 12.30 | 11.72 | 350.33 | 350.21 |
| 9 | 0.24 | 12.22 | 11.74 | 350.34 | 350.26 |
| 10 | 0.33 | 12.24 | 11.77 | 350.36 | 350.21 |
| 11 | 0.58 | 12.41 | 11.78 | 350.33 | 350.21 |
| 12 | 0.33 | 12.29 | 11.91 | 350.39 | 350.27 |
| 13 | 0.47 | 12.45 | 11.83 | 350.30 | 350.21 |
| 14 | 0.48 | 12.43 | 11.73 | 350.30 | 350.22 |

